

17 Dec 2019

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27/02/2020

BUILDING CONSENT NUMBER

2019/1381

**GUIDANCE NOTES FOR ACHIEVING A CODE  
COMPLIANCE CERTIFICATE FOR FIRE SAFETY SYSTEMS  
HWCP ZONE 1 ANCHOR TENANT AND CHILDCARE CENTRE, INVERCARGILL**

The sprinkler system installer is to provide a fully completed certificate of completion on satisfactory completion of the installation and commissioning tests. The certificate is to be in a form meeting the requirements of the NZ building Code and associated Standard NZS 4541:2013, and to be signed by suitably qualified personnel such as FPIS Ltd, AON, or similar. The sprinkler system in conjunction with the manual call point system is to be Type 6 in accordance with the Building Consent. *(Note this work will only be fully completed when the subsequent Zone 2 is in construction and the Class A water supply and sprinkler valve set installed. Notwithstanding this, as an interim, the associated statements for the Building Consent works is required).*

The fire alarm installer shall supply a fully completed certificate of completion on satisfactory completion of the installation and commissioning tests. The certificate is to be in a form meeting the requirements of the NZ building Code and associated Standard NZS 4512:2010, and to be signed by suitably qualified personnel such as FPIS Ltd, AON, or similar. The alarm system in conjunction with the sprinkler system is to be Type 6 with supplementary smoke detection to the extent required in accordance with the Building Consent including that all fire alarm interfaces are functioning. *(Note this work may only be completed when the subsequent Zone 2 is completed and the Fireman's control room installed).*

The installer of the Type 18 hydrant system on completion is to provide a fully completed certificate of completion on satisfactory completion of the installation and commissioning tests. The certificate is to be in a form meeting the requirements of the NZ building Code and associated Standard NZS 4510:2008 and to be signed by suitably qualified personnel such as FPIS Ltd, AON, or similar. *(Note this work may only be completed when the subsequent Zone 2 are completed and the Fire control room with subsequent inlets installed).*

The installer of the smoke extract system within the anchor tenant shall undertake a physical test confirming operation of the extract fan and make up air supply operate as per the Cosgroves consented mechanical design (Type 11), including all other required commissioning requirements of the standard. A PS3 is to be provided on completion for the system installer stating that the smoke extraction system complies with AS 1668:Part 1.

Cosgroves as the designer responsible for the smoke extraction system design is to provide a PS4 construction review stating compliance with AS 1668:Part 1.

The emergency lighting installer shall provide a producer statement (PS3) confirming that the emergency lighting meets minimum illumination levels to the required areas and the minimum duration time as required by NZBC F6/AS1 and the Building Consent. Also required is the test and commissioning certificates for the emergency lighting, including test results. *(Note this work may only be completed when the subsequent Zones 1 and 2 are completed when the subsequent Zone 2 works when the connection to the development main is achieved. Notwithstanding this, as an interim, the associated statements for the Building Consent works is required).*

Cosgroves as the owner's consultant responsible for the emergency lighting design shall provide a producer statement for construction review (PS4) to confirm that the appropriate

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Inspections have been carried out and the building works have been completed in accordance with the consented documentation. *(Note this work may only be completed when the subsequent Zone 2 works is completed when the connection to the development main is achieved).*

Penetrations through smoke and fire separations to be sealed in accordance with AS:1530 Part 4 and AS4071:Part 1. A PS3 to C3 of the NZBC is to be provided from relevant trade that is sealing penetrations. A schedule of penetrations sealed is to be provided, noting that the treatment is to be in accordance for the solutions provided in the building consent documentation.

The applicator of the intumescent paint system shall on completion provide a PS3 stating compliance with C6 of the NZBC and the Building Consent. Also to be included is a record of the independent thickness tests.

Holmes Fire LP as the owner's consultant responsible for the fire design shall provide a producer statement for construction review (PS4) to confirm that the appropriate observations have been carried out and the building works have been completed in accordance with the consented fire strategy documentation. The level of construction monitoring is to be CM2. It is the applicant's responsibility to arrange the appropriate observations directly with the Fire Engineer or their representative.

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# **HWCP Invercargill Central Invercargill**

**HWCP Management Group**

**Zone 1 (Anchor) Fire Engineering Brief**

**Issue Authorisation**

Project: HWCP Invercargill Central, Invercargill  
Project No. 136249

Version	Date	Status	Prepared	Reviewed
A	24 June 2019	For Review	ACC	DXM

Version	Extent of Revision

This report caters specifically for the requirements for this project and this client. No warranty is intended or implied for use by any third party and no responsibility is undertaken to any third party for any material contained herein. This report is produced and signed solely on behalf of Holmes Fire and no liability whatsoever accrues to the authors.

The building owner must be aware that the fire safety solutions described in this report may be alternative solutions to those given by the MBIE Acceptable Solutions or Verification Methods. Consideration of protection of the building owner's property is not included unless this has been specifically requested.

**Written By:**



AMY CHAO  
Fire Engineer

**Reviewed By:**



DARIN MILLAR  
Principal

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## 1 PURPOSE

### 1.1 Purpose of this Document

The purpose of this Fire Engineering Brief (FEB) is to establish and agree the fire safety design and acceptance criteria with the relevant stakeholders of the HWCP Invercargill CBD Development **Zone 1** project. The FEB will describe the additional methodologies, input data, and acceptance criteria required to supplement those prescribed within the Verification Method C/VM2, that is used to justify compliance with the Building Code and the project design brief.

The development of the Zone 1 FEB is to address the technical aspects of design scenarios and calculation methods for this particular zone. This document is to be considered in conjunction with the Master Fire Engineering Brief.

### 1.2 Related Documents

This Fire Engineering Brief should be read in conjunction with the various briefing reports prepared for other consultants during this phase of the project, including any future fire reports prepared for this project by Holmes Fire. The following documents are prepared by the fire engineer for the project:

- Master Fire Engineering Brief (FEB), ref: 136249FEB01(Master)
- Zone 1 Fire Engineering Brief (FEB), ref: 136249FEB03(Anchor).
- Zone 1 Fire Engineering Strategy's (FES), ref: 136249FES01 (Anchor).
- Zone 1 Fire Engineering Sketches (FS), ref: 136249FS01 (Anchor).
- Zone 1 Fire Engineering Verification's (FEV), ref: 136249FEV01 (Anchor).

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## 2 DESCRIPTION OF THE PROJECT

The project covered in this C/VM2 design is the construction of the HWCP Invercargill CBD development Zone 1 (Anchor).

Zone 1 is a three-storey structure that consists of a two-storey anchor retail building with a childcare centre above and will be connected to a shopping centre (Zone 2) on the west side. Entrance into the ground floor anchor retail space is located on the north side via Esk Street with direct access to the shopping centre on the west side of building. Direct access to the first-floor anchor retail space will be available on the west side via the Level 1 carpark (Zone 3). Level 2 childcare centre can be accessed via the Level 2 carpark.

The anchor building has two exits that leads occupants directly to a safe place outside on the north side and the SE side. Occupants can also egress via the shopping centre on the west side. Level 1 has two stairwells located on the SE and NE side that leads directly to a safe place outside with a connection to the Level 1 carpark on the west side. Level 2 childcare has two means of egress via the east side stairwell that leads directly to a safe place outside or the west side walkway that leads to the carpark stairwell on the west side.

The ground floor and level 1 anchor building are interconnected via the escalator void in the centre of the building. Level 2 childcare centre is fire separated from the anchor space. Smoke extract system is proposed in the escalator ceiling void with make up air provided from the ground floor main entrance, west side opening to the shopping centre (Zone 2) and first floor opening to the Level 1 carpark on the west side.

Following the meeting on 20 June 2019 with FENZ and the peer reviewer, the design philosophy is developed as such –

- C/VM2 is silent on children having a slower travel speed. The proposed design will consider the children having slower evacuation speed of 0.7 m/s for horizontal travel and 0.5 m/s for vertical travel.
- C/VM2 requires the children to be evacuated to a “place of safety” on the same level first, which would require the sprinkler system to be fully compliant with NZS 4541 without modification. The building does not have a place of safety and the proposed design is to rely on having a buffer area (outdoor play area) on the roof top away from the childcare centre instead of a place of safety. All occupants of the building are on all out evacuation.
- Based on the departures identified above, the design may need to be considered as Alternative Solution.

Refer to Master FEV (ref:136249.FEB01) for overall principles.



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### 3 EGRESS DESIGN PHILOSOPHY

#### 3.1 Fire Emergency Procedures

The evacuation strategy adopted for this building forms an important part of the building design. An 'all-out' evacuation strategy applies to this building. All egress routes are assumed to be used by all occupants upon activation of the fire alarm.

There are two cases to consider regarding the evacuation of the childcare centre – which are fire inside the childcare centre, and fire in other areas. Note that only a single fire is to be considered happening in the building at any one time.

##### 3.1.1 Fire inside Childcare Centre

In case of fire inside the childcare centre, the teachers and staff members are to either lead the children to the buffer area on the roof top, or into the carpark and then when all the children are accounted for, they are then led downstairs by the teachers and staff members.

The pre-movement time is 60 seconds for staff to respond to alarm and then 60 seconds per child per staff to the buffer area. The pre-movement times for other occupants in the other locations are not changed and not affected by the childcare centre. Due to the long pre-movement time, the egress time from the childcare centre will be isolated from the remainder of the building and RSET time will be calculated utilising hand calculation.

This concept is the same as the philosophy used in C/VM2. However, instead of having a place of safety, the area away from the childcare centre is considered as a "buffer area" as the building is unlikely to have a full NZS 4541 compliant sprinkler system. It should however be noted that if the sprinkler system is modified by appendix B of C/AS2-7, the level of safety at the open air buffer area when there is a fire inside the childcare centre is at least the same if not better as for a fire within the building.

##### 3.1.2 Fire in Other Areas

In case of fire in other areas, the pre-movement time for the childcare centre would be 120 seconds in accordance with C/VM2 and then 60 seconds per child per staff. The pre-movement times for other occupants in the other locations are not changed and not affected by the childcare centre. Due to the long pre-movement time, the egress time from the childcare centre will be isolated from the remainder of the building and RSET time will be calculated utilising hand calculation.

C/VM2 does not distinguish the evacuation speeds between adults and children. Our proposed design will adopt the travel speed for childcare centre based on Kholshchevnikov et al.<sup>1</sup>, with travel speed of 0.7 m/s for horizontal travel, and 0.5 m/s for vertical travel.

Once the occupants reach the safe path stairs they can travel all the out to the external safe place.

#### 3.2 Management and Use

The staff members and teachers of the childcare centre will be the first to respond in the childcare centre

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<sup>1</sup>2 Kholshchevnikov, V.V. et al., Study of children evacuation from pre-school education institutions, Fire & Materials, Vol 36, pp. 349-366, 2012.

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area to a fire emergency in this building. Suitable training of building staff and management is obligatory to ensure that the evacuation procedures put in place are carried out effectively.

For the purposes of meeting the requirements of the Fire Service Act, it is recommended that a Fire Safety Management Plan is prepared for the building after approval of the Fire Engineering Strategy, incorporating documentation the staff emergency response plan.

## 4 FIRE SYSTEMS OVERVIEW

### 4.1 Sprinkler System

A new Type 6 automatic sprinkler system is to be installed throughout the Zone 1 building in accordance with NZS4541, as an Appendix B (C/ASX) system. This may increase to being a Class A system to Appendix B but this will be established at the end of the verification.

### 4.2 Fire Alarm System

Supplementary smoke detection system is to be installed on Level 2 childcare centre in accordance with NZS 4512. The supplementary smoke detection system will not trigger building wide alarm and will not be connect to the FENZ. The manual call points and the sprinkler system will trigger the building wide alarm and evacuation and contact the FENZ.

A new Type 2 fire alarm system is to be installed throughout the Zone 1 building in accordance with NZS4512.

The extent of a smoke detection system on ground and level 1 will be determined as part of the detailed assessment. Certain coverage is expected to facilitate the smoke control system and any EMHOD but this does not necessarily mean a full Type 4 system in this Zone.

The use or otherwise of a double knock system for smoke detectors prior to initiating evacuation is yet to be determined and will be considered as part of a detailed assessment.

### 4.3 Storage Requirements

The Fire Engineering design is based on a capable storage height of no more than 3 m. It is noted that as we have not yet received a written confirmation from the Anchor tenant, that this could potentially change. Should the storage height exceed 3 m at a later stage, the design will be revisited.

### 4.4 Indicative Fire Separations and Means of Escape

The indicative locations of fire and smoke separations are detailed on the attached sketch FS101. Also shown on these plans are the proposed means of escape for the building. These drawings are indicative only and provided for the purpose of informing the stakeholders of the intended Fire Engineering design at this early stage of the design.

### 4.5 Other Proposed Key Fire Engineering Design Features

It is expected that the following Fire Engineering design features will be included in the final design:

- Mechanical smoke extract system that extracts smoke at high level of the escalator void in the centre of the anchor building.

Make up air is expected to be provided via

- powered opening of the automatic sliding doors on the ground floor, and
- powered opening of the automatic sliding doors first floor, and
- the ground floor opening that connects the anchor to the shopping centre on the west side (it is expected to be open during opening hours with meshed security roller doors afterhours that permits make up air).

The specific performance requirements of these features is currently under development and will be detailed in the Fire Engineering Strategy.

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#### 4.6 “Do Not Exit” Exit signage

The “Do Not Exit” signage is proposed on the Childcare Centre west exit. This “Do Not Exit” signage shall be activated when the sprinkler activated on either L1 or L2 carpark. This is to prevent egress from the Childcare Centre into the carpark when there is a fire that could potentially affect occupant egress.

## 5 C/VM2 DESIGN SCENARIO APPLICABILITY

The following identifies the design scenarios that require analysis.

Table 1 - C/VM2 Design Scenario Applicability

Design Scenario	Description	Further review required	Justification
BE	Blocked Exit	No	All areas with occupant load greater than 50 people have no less than two exits available. Any space with excessive (as defined by the BE scenario) travel distances will have additional escape routes added.
UT	Unoccupied room	No	Fire suppression is provided by way of sprinkler protection throughout building
CS	Concealed Space fire	No	All areas in building provided with automatic detection.
SF	Smouldering Fire	No	Smoke detection in sleeping areas, designed and installed to a recognised national or international standard.
HS	Horizontal fire Spread	No	Clause 3.6: On the basis that the sprinkler system is provided with a Class A sprinkler system and the spaces to which this applies do not have storage in excess of 3m height. For a space to not apply with storage in excess of 3m height - it must be in a separate firecell - this is to be confirmed in the detailed design. Clause 3.7 To be achieved by compliance with Table 4.1 of C/VM2.
VS	Vertical fire Spread	No	Part A: Either by Table 4.2 of C/VM2 or use of non-combustible material. Part B & Part C: The building is provided with automatic sprinkler system.
IS	Internal Surface fire spread	No	Compliance with NZBC C3.4 is required. Proposed to comply with internal surface finish requirements in accordance with C/VM2 and appropriate C/AS4 and C/AS5.

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Design Scenario	Description	Further review required	Justification
FO	Firefighting Operations	Yes	The proposed firefighting facilities for the building, e.g. the fire alarm panel, sprinkler inlets and internal hydrant inlets and outlets, are being addressed directly with FENZ. Input from the NZFS Operational representative is requested to confirm that the proposed locations are appropriate.  The agreement with FENZ will be consolidated and included in the respective FEV documentation.
CF	Challenging Fire	Yes	Refer Section 5.1
RC	Robustness Check	Yes	Refer Section 5.2

### 5.1 Design Scenario CF: Challenging Fire

Challenging Fire Scenarios are described in the table below and the sketches FS301 and FS302.

Table 2 - Challenging Fire Descriptions

Challenging Fire Scenario	Location	Description
CF1	GF Anchor	Fire in middle of atrium (escalator void). "Fast" t-squared fire growth rate, i.e. $Q=0.0469t^2$ . Maximum fire size = 20 MW or fire size at which sprinklers activate.
CF2	GF Anchor	Fire on the ground floor retail space under L1 (intermediate floor). We will adopt the ceiling height as being the highest expected for the tenancy for the sprinkler activation time, "Fast" t-squared fire growth rate, i.e. $Q=0.0469t^2$ . Maximum fire size = 20 MW or fire size at which sprinklers activate.
CF3	2L Childcare Centre	"Fast" t-squared fire growth rate, i.e. $Q=0.0469t^2$ . Maximum fire size = 20 MW or fire size at which sprinklers activate.

Input and acceptance criteria specified by the Verification Method C/VM2 are used for the fire design as detailed below, including consideration of the additional design parameters previously discussed, and other relevant data and assumptions as referenced.

#### 5.1.1 Challenging Fire 1

Challenging Fire 1 is located to simulate a plume scenario at the bottom of the high-ceiling space. This reflects the anticipated worst case for largest fire and affect the tenability on the Level 1 retail space resulting in less available safe egress time for occupants from the Level 1 retail space.

The internal, non-fire rated partition between Zone 1 (Anchor) and Zone 2 (Mall) is expected to remain in place for the duration of egress, as the upper layer temperature is not expected to exceed 200°C. The above expectations will be confirmed in the analysis to be undertaken.

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Both the GF and L1 of the Zone 1 (Anchor) will be included as part of the assessment with automatic sliding doors open upon fire alarm activation. A delay of 15 s will be applied after the operation of the fire alarm system before the doors are taken as open. The connection between GF Zone 1 (Anchor) and Zone 2 (Mall) will be considered as constantly open. The smoke exhaust system will start at the activation of the fire alarm system with a 30 s ramp up time.

This fire represents the worst-case scenario for Level 1 retail space, therefore no challenging fire is proposed on Level 1 as a separate scenario.

### 5.1.2 Challenging Fire 2

Challenging Fire 2 is located to simulate a balcony spill plume fire which reflect the worst case for smoke production and affect tenability on Level 1 retail space resulting in less available safe egress time for occupants.

The internal, non-fire rated partition between Zone 1 (Anchor) and Zone 2 (Mall) is expected to remain in place for the duration of egress, as the upper layer temperature is not expected to exceed 200°C. The above expectations will be confirmed in the analysis to be undertaken.

Both the GF and L1 of the Zone 1 (Anchor) will be included as part of the assessment with automatic sliding doors open upon fire alarm activation. A delay of 15s will be applied after the operation of the fire alarm system before the doors are taken as open. The connection between GF Zone 1 (Anchor) and Zone 2 (Mall) will be considered as constantly open. The smoke exhaust system will start at the activation of the fire alarm system with a 30 s ramp up time.

As the ceiling height is not the same throughout the ground floor, it is proposed that for this challenging fire, B-Risk model will be used to find the sprinkler activation time for the higher ceiling (GF) and this number will be used as the sprinkler activation time in the FDS model. The FDS model for smoke movement will use the lower ceiling height (GF).

### 5.1.3 Challenging Fire 3

Challenging Fire 3 threatens the occupants within the childcare centre area, for whom tenability will be assessed. The fire within the childcare centre is not expected to threaten the occupants in the remainder of the building due to the inherent separations expected. Note that the building is still under an “all out” evacuation.

CF3 will be modelled in B-RISK with a room for fire origin in the kitchen and a supplementary room to be equivalent to 50% of the floor area (given the partitions will be non rated).

## 5.2 Design Scenario RC: Robustness Check

### 5.2.1 Smoke exhaust

Robustness Check Scenario (RC1) will utilise CF1 with the failure of the smoke exhaust system. A fire in the atrium is considered a worst-case scenario with the largest fire due to the high-ceiling space. For this scenario, only FEDco will be assessed. The doors are still expected to power open.

Table 3 - Robustness Check Scenario Descriptions

Robustness Check Scenario	Location	Description
RC1 (utilising CF1)	GF Fire	Smoke Exhaust System failure. Fire in middle of atrium (escalator void). "Fast" t-squared fire growth rate, i.e. $Q=0.0469t^2$ . Maximum fire size = 20 MW or fire size at which sprinklers activate.

### 5.2.2 Fire and smoke control doors without hold-open devices.

The building has two independent fire separated stairs. The Robustness Check scenario requires fire safety features to be failed only one at a time. Therefore, this scenario is considered addressed by provision of a second stair (that would not simultaneously be affected by failure of a fire/smoke door), and no further analysis is proposed.

### 5.2.3 Smoke curtain

Potentially a smoke curtain located in the Ground level west connection to the mall (This may not be required due to the beam height and will be confirmed at design stage). The proposed curtain may only descend to 2.5 m above FFL as a smoke barrier/reservoir. Therefore, for the purpose of the Robustness Check design scenario in this means of escape assessment, a failure of the curtain will not adversely impact occupant egress and no further analysis is proposed.



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## 6 OCCUPANT CHARACTERISTICS

Occupant characteristics in the anchor building, which may affect occupant response to a fire emergency include:

1. Occupants are generally unfamiliar with the layout of the building.
2. Occupants are generally alert, ambulant, cognitive and able to understand and act on instructions to evacuate.

There will be no sleeping occupants in the anchor building at any time (except the childcare centre).

For the childcare centre, the staff members and the teachers are awake, familiar with the layout of the centre and the escape route.

The children are not expected to initiate the evacuation by themselves and will rely on the staff members to instruct them.

The pre-movement time proposed for the childcare centre is as described in the Egress Design Philosophy.

### 6.1 Fire Design Occupant Loads

The general assumptions to be used in the fire engineering assessment of the proposed design are provided below. Any alterations to the design that result in the assumptions becoming invalid will be checked as part of the detailed verification and updated loads will be presented at that time.

The following is a summary of the fire design occupant load within the Zone 1 anchor building from C/VM2 Table 3.1. The occupant loads detailed in Table 4 are the maximum number of occupants for the spaces listed (as calculated using the C/VM2 densities).

Table 4 - Summary of Occupant Loads

Level	Description	Area [m <sup>2</sup> ]	Occupant Density [m <sup>2</sup> /person]	Occupant Load
Ground	Anchor	2091	3.33 <sup>1</sup>	628
Ground	Esk St tenancy A	119	3.5	34
Ground	Esk St tenancy B	121	3.5	35
Ground	Esk St tenancy C	120	3.5	34
Ground	Esk St tenancy D	115	3.5	33
Ground	B.O.H (Reserve)	110	100	1
L1	Anchor	2310	3.33 <sup>1</sup>	694
L1	B.O.H (Reserve)	313	100	3
L1	Offices	217	10	22
	<b>Anchor space</b>			<b>1484</b>
L2	Childcare Centre	-		88 children + staff
	<b>Total (Zone 1)</b>			<b>1572</b>

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### Explanatory Notes

1. Anchor tenant seeks to have their occupant density to be 3.33p/m<sup>2</sup> as opposed to 3.5p/m<sup>2</sup>.
2. The exact occupant load for the Childcare Centre is yet to be confirmed. However, due to the restriction to external play area, a maximum of 88 children is permitted in the Childcare Centre. This is to be confirmed in the detailed design.

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## 7 FIRE RESISTANCE RATING TO WITHSTAND BURNOUT

The time equivalence formula shall be used to determine the required fire resistance rating to withstand burnout, as per C/VM2 Equation 2.1.

### 7.1 Fire Load Energy Density

The time-equivalent formula, as described in C/VM2 2.4.4, shall be used to model the full burnout design fire. The parameters to be used in the calculation are outlined below.

#### 7.1.1 Fire Load Energy Density, $e_f$

The following is a summary of the fuel load energy density (FLED),  $e_f$ , within the building from C/VM2 Table 2.2.

Table 5 - Summary of Fuel Load Energy Density

Level	Activity	Example	FLED [MJ/m <sup>2</sup> ]
G	Spaces for display of goods for sale and B.O.H	96% retail (800 MJ/m <sup>2</sup> ) + 4% B.O.H (1200 MJ/m <sup>2</sup> ). Exact split will depend on updated Architectural plans	816
L1	Spaces for display of goods for sale, office and B.O.H	81% retail (800 MJ/m <sup>2</sup> ) + 8% Office (800 MJ/m <sup>2</sup> ) + 11% B.O.H (1200 MJ/m <sup>2</sup> ) Exact split will depend on updated Architectural plans	844
L2	Childcare	Early childhood centre	800

#### 7.1.2 Thermal Properties Conversion Factor, $k_b$

Refer to Master Fire Engineering Brief (ref:136249FEB01) for details.

#### 7.1.3 Modification Factor, $F_m$

Refer to Master Fire Engineering Brief (ref:136249FEB01) for details.

#### 7.1.4 Ventilation Factor, $w_f$

The ventilation factor,  $w_f$ , shall be determined as described in accordance with C/VM2 Equation 2.2.

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## 8 ANALYSIS TOOLS

### 8.1 Fire modelling

Due to the complexity of the geometry, the computational fluid dynamics modelling Fire Dynamics Simulator (FDS) Version 6.7.1 will be used for this project. Refer to Appendix B for FDS modelling information.

Further to the Master FEB, the following assumptions and simplifications are made for purposes of fire modelling:

- Fire and smoke separations (including those around lifts) are assumed to have no leakage areas.
- The GF connection to Zone 2 will be modelled as a connection to outside for the purposes of this FEB. When Zone 2 FEB is undertaken, we will allow for Zone 1 scenario (worst case) to interact with the Zone 2.
- The Level 1 connection to Zone 3 will be modelled as an opening to the exterior. Given the Zone 3 is a carpark and alternative means of escape options exist for a relatively small occupant load, this simplification will occur. This opening will not be modelled at any other time.

### 8.2 Movement of people

The methodology is as described in the Master Fire Engineering Brief. Further to that content, we offer the following supplementary information:

1. A base case Zone 1 consideration will be based on the distribution as per the Master FEB for Zone 1 only i.e no blocking of a route.
2. Non base case that will consider egress for all of Zone 1, 2 and 3 occupants with no exits being considered unavailable. Distribution as per the Master FEB.
3. To facilitate evacuation of a childcare facility, "Do not enter" signs were proposed in the vicinity of access into the Zone 3 carpark. These were intended to inform staff that it would be wiser to use the other exit. We propose that this signage be active when any alarm is initiated from Zone 3 Level 1 or Level 2. Given the methodology used to evacuate the childcare facility, and the inherent delays we need to accommodate, we do not intend on simulating their impact on the Zone 1 RSET. This assumption of the delay being longer than it will take for the remainder of Zone 1 occupants to enter a safe place will be verified as part of the assessment.

## 9 SCENARIOS AND PERFORMANCE CRITERIA FOR ASET VS RSET

The available safe environment time (ASET) is the earliest time period from fire ignition to the time at which one of acceptance criteria reaches a limit state where occupants are egressing the building.

The ASET calculation is to be based on the following acceptance criteria depending on the specific location of the occupants:

- $FED_{CO}$  of  $<0.3$ ,
- $FED_{thermal}$  of  $<0.3$ , and
- Visibility  $> 10$  m

ASET will be taken when the above acceptance criteria (measured at 2.0 m above floor level) is exceeded depending on the specific location of CF and the occupants.

The challenging fires, occupant scenarios and ASET tenability are summaries in the table below.

Table 6 - Design Scenario Summary Matrix

Challenging Fire Scenario	Occupant load <sup>1</sup> /Egress distribution	ASET Tenability
CF1 & CF2 (FDS model)	Base case: <ul style="list-style-type: none"> <li>• Zone 1 occupants only</li> <li>• All exits available (no blocked exit)</li> </ul>	<ul style="list-style-type: none"> <li>• <math>FED_{CO}</math> only on Zone 1 GF and L1 retail areas (on the basis that adjacent tenancies egress directly to the outside).</li> <li>• Visibility and <math>FED_{thermal}</math> on Zone 1 L1 Retail space.</li> <li>• <math>FED_{CO}</math> only in Zone 1 Stairwell will; be based on the <math>FED_{CO}</math> of the retail floor.</li> <li>• Visibility and <math>FED_{thermal}</math> in Zone 2 GF will only be established in Zone 2 assessment.</li> <li>• No tenability assessed in Zone 3 Carpark.</li> </ul>
	Non-Base case RSET (occupants from other Zones interact): <ul style="list-style-type: none"> <li>• Zone 1, 2 &amp; 3 occupants (Zone 3 L5 - community event).</li> <li>• All exits available (no blocked exit)</li> </ul>	
CF3 (B-Risk model)	Base case: <ul style="list-style-type: none"> <li>• L2 Childcare occupants only.</li> <li>• All exits available (no blocked exit)</li> </ul>	<ul style="list-style-type: none"> <li>• <math>FED_{CO}</math> only on Zone 1 L2 (Childcare Centre).</li> <li>• <math>FED_{CO}</math> will not be measured anywhere else as the occupants will be in appropriate "buffer zones" once they depart the L2 enclosure.</li> </ul>
	Non-Base case RSET (occupants from other Zones interact). Due to the long pre-movement time, the egress time from the Childcare centre will be isolated from the remainder of the building therefore no non-base case RSET will be presented - this will need to be verified by one example.	

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Challenging Fire Scenario	Occupant load <sup>1</sup> /Egress distribution	ASET Tenability
RC 1 (FDS model)	Base case: <ul style="list-style-type: none"> <li>Zone 1 occupants only.</li> <li>All exits available (no blocked exit)</li> </ul>	<ul style="list-style-type: none"> <li>FEDco only on Zone 1 GF and L1 retail areas (on the basis that adjacent tenancies egress directly to the outside).</li> <li>FEDco only in Zone 1 Stairwell will; be based on the FEDco of the retail floor.</li> </ul> <p>FEDco only in Zone 2 GF will only be established in Zone 2 assessment.</p>
	Non-Base case RSET (occupants from other Zones interact): <ul style="list-style-type: none"> <li>Zone 1, 2 &amp; 3 occupants (Zone 3 L5 - community event).</li> <li>All exits available (no blocked exit)</li> </ul>	

<sup>1</sup> Refer to the occupant load table and functional modes for a description of the numbers of persons being considered in a space for the calculation of RSET.

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## 10 SUMMARY

The stake holders in the fire safety design for this project are expected to participate in the development of this FEB. The members of this team, including the Authorities Having Jurisdiction, are expected to record their general agreement with the content. The content is then regarded as the official accepted brief for Fire Engineering design.

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## Appendix A Preliminary Fire Engineering Sketches



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# Legends for the drawing sets

## Drawing title references:

Block - **Fire Strategy(FS)** - Drawing number Rev

These drawings represent the Fire Strategy outcomes and are therefore the overall identification of Fire Ratings and Means of Escape intent.

- Sm** ■ ■ ■ Smoke separation
  - 15** <<<< (15)/15/15 Sm
  - 30** ■ ■ ■ (30)/30/30 Sm
  - 45** ■ ■ ■ (45)/45/45 Sm
  - 60** <<<<< (60)/60/60 Sm
  - 90** <<<<<< (90)/90/90 Sm
  - 120** <<<<<< (120)/120/120 Sm
  - 180** ■ ■ ■ (180)/180/180 Sm
  - SB** - - - Smoke baffle
- 
- XXXXmm** Minimum clear egress width
  - VP** Vision Panel
  - PBDH** Panic-bar door hardware, or non-latching door readily pushed open
  - EXIT** Exit Sign (indicative)
  - Egress route (no requirement for direction of door swing) [minimum 760mm door clear unless noted otherwise]
  - Egress route (door to swing in direction of egress) [minimum 760mm door clear unless noted otherwise]
  - Egress route (both leaves required for egress) [minimum 1520 door clear unless noted otherwise]
  - Exitway
  - Final Exit** "Safe place"
  - NO EXIT** No Exit sign
  - Electromagnetic Hold Open Device
  - Fire Service vehicle access
  - Vehicle Attendance Point
  - Fire Service Access
  - Smoke Detector
  - Heat detector

- Design action or note.
- Design question relating to items outside the scope of NZBC compliance.
- Design question for discussion or further assessment.

## Drawing title references:

Block - **Fire Protection(FP)** - Drawing number Rev

These drawings represent the Fire Protection outcomes and are therefore the overall identification of infrastructure considerations for the Performance Specification.

- Fire Service vehicle access
- Vehicle Attendance Point
- Fire Service Access
- FAP** Fire Alarm Panel
- FIP** Fire Indicator Panel
- RDU** Remote Display Unit (text display)
- Electromagnetic Hold Open Device
- Manual Call Point
- FH** Fire Hydrant
- FHI** Fire Hydrant Inlets
- Hydrant Outlet
- FSI** Fire Sprinkler Inlets
- SVS** Sprinkler Valve Set
- BFP** Backflow preventer

## Drawing title references:

Block - Verification(V) - (no numbering as they are calculations/verification documents)

These sketches represent information used to verify the design complies with the Building Code. They support calculations and are used by the Peer Reviewer, NZFS and Council.

- Design action or note.
- Design question relating to items outside the scope of NZBC compliance.
- Design question for discussion or further assessment.
- Challenging Fire location
- Travel distance
- End of dead end travel

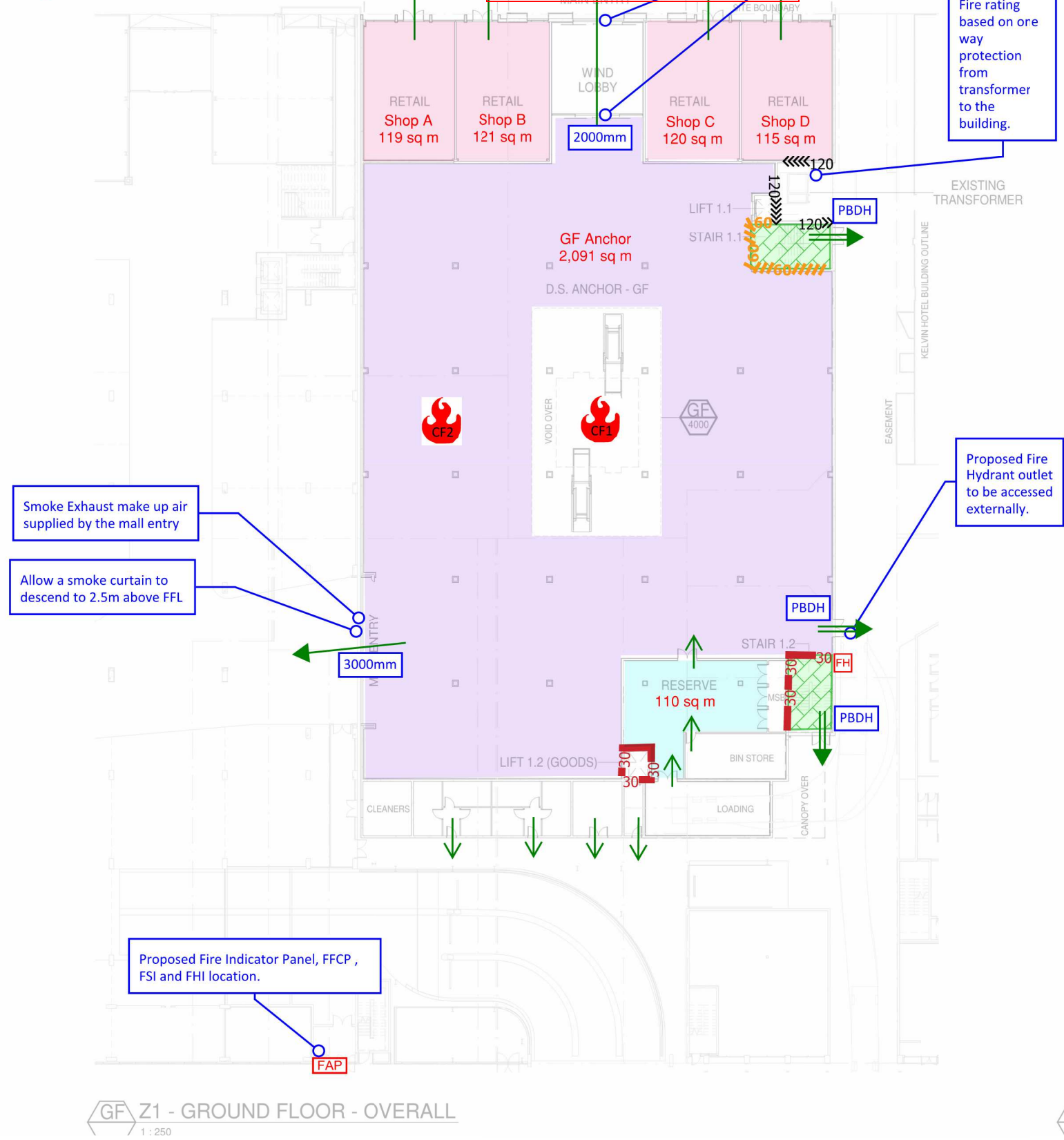
<b>BUILDING CONSENT NUMBER</b> fire engineering design or detail. Detailed construction drawings are provided by other parties. Fire engineering drawings are shown.		
<b>2019/1381</b>		
Drawn: DXM	Date: 03/05/2019	
Project No.	Sheet No.	Rev
<b>136249</b>	<b>Z1FEB FS 100</b>	<b>A</b>
		Holmes Fire LP L2, 254 Montreal St Christchurch New Zealand T: +64 3 365 8855 holmesfire.com
Sketch Title		
Legend Page		

# HWCP Development Zone 1 Anchor and Childcare Centre

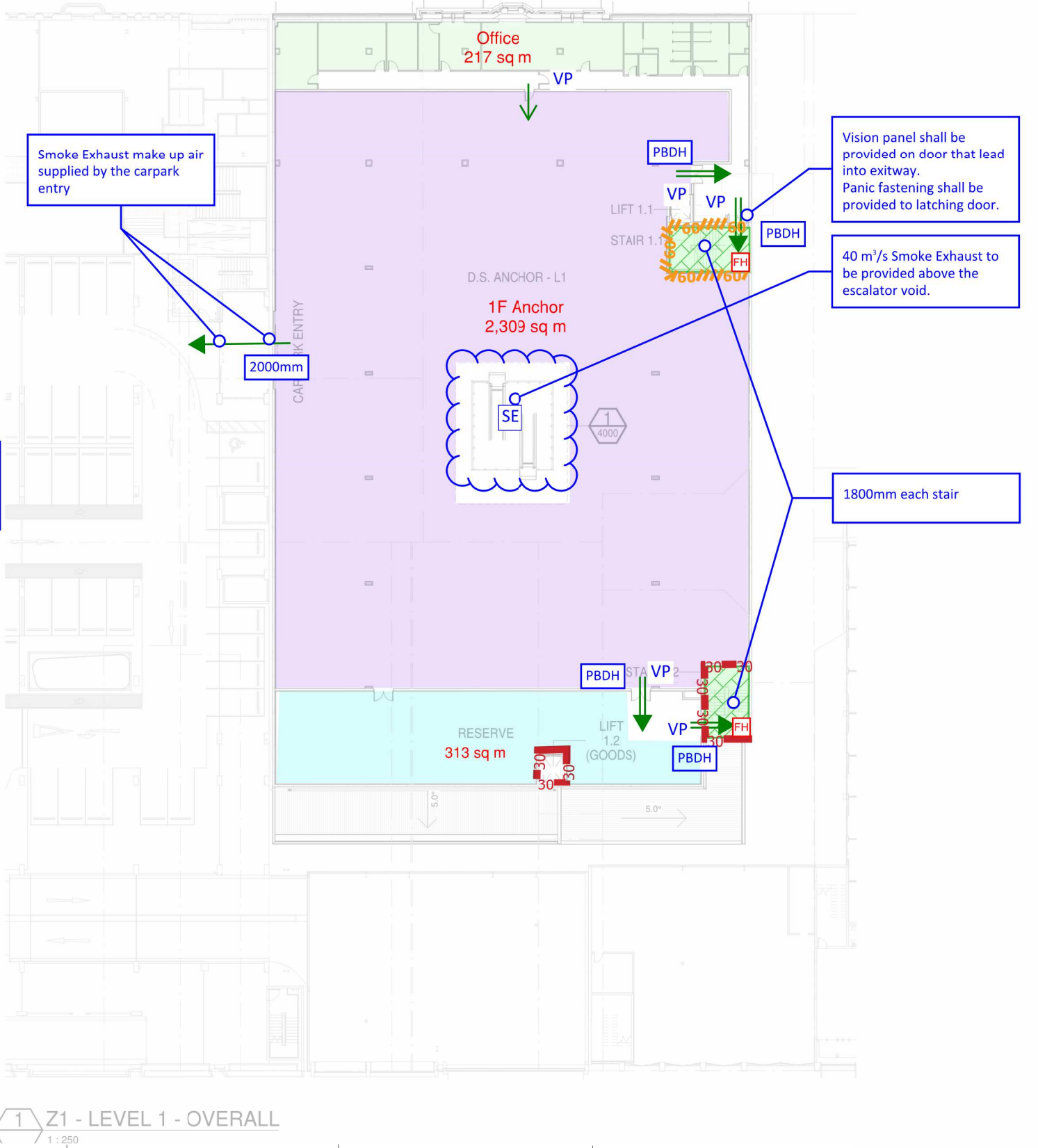
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Z1 - GROUND FLOOR - OVERALL  
 1 : 250



Z1 - LEVEL 1 - OVERALL  
 1 : 250

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Project Title  
**HWCP - Invercargill Central**

Sketch Title  
**Zone 1 GF & L1  
 Fire / Smoke Separations  
 & Means of Escape**

Drawn: ACC Date: 02 / 05 / 2019

Project No. **136249** Sheet No. **Z1FEB FS 101** Rev **A**

Rev.	Date	Description	Iss.	Appr.
A	27.11.19	FOR COMMENT	BH	JB
B	10.01.19	PRELIMINARY DESIGN	BH	JB
C	21.03.19	PRELIMINARY DESIGN	BH	DA
D	17.04.19	FOR INFORMATION	JT	DA



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**HWCP**

Project  
**INVERCARGILL CENTRAL - ZONE 1**  
 TAY STREET & DEE STREET CORNER  
 INVERCARGILL  
 Project Number  
 917077

Status  
**PRELIMINARY DESIGN**  
 Date Plotted 17/04/2019 2:44:26 PM  
 Date Issued 21.03.19  
 Scale 1 : 250 @A1

Drawing Title  
**ZONE 1  
 OVERALL FLOOR PLANS**  
 Drawing Number  
**Z1-PD-A-1100**

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WALL CODE	DESCRIPTION
WT.E01	PRECAST CONCRETE PANELS
WT.E02	POWDER COATED ALUMINIUM EXTRUSION SHOPFRONT SYSTEM
WT.E03	300mm CONCRETE SKIN BEHIND EXISTING RETAINED FACADE, REFER TO STRUCTURAL ENGINEERS DETAILS
WT.E04	SWISSPEAR

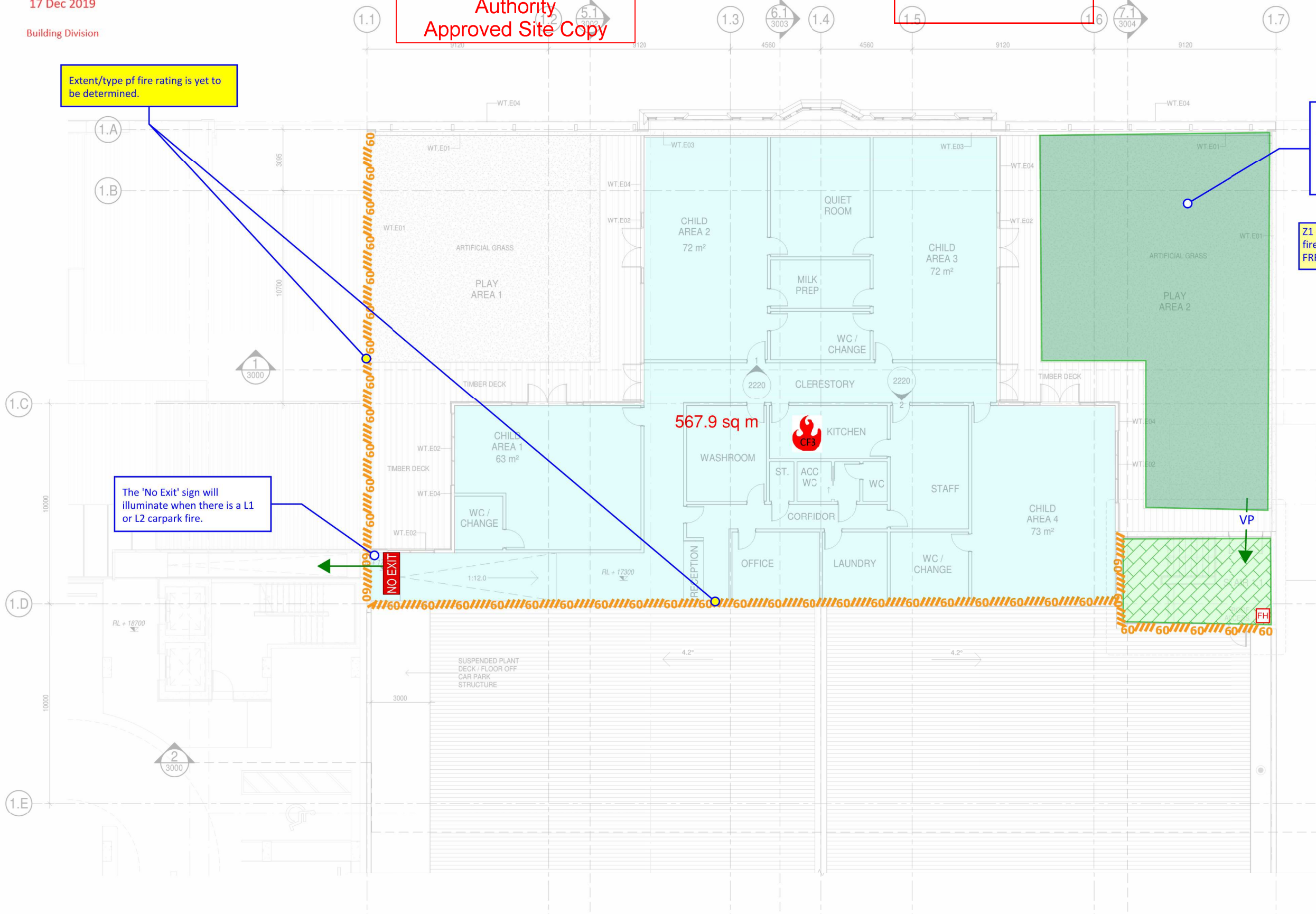
Extent/type of fire rating is yet to be determined.

Buffer Area, expect to include some play equipment

Z1 - Level 2 is considered as a separate firecell and shall be provided with an FRR of (60)/60/60.

The 'No Exit' sign will illuminate when there is a L1 or L2 carpark fire.

NOTE:  
EXTERNAL PLAY AREA = 440m<sup>2</sup>  
5m<sup>2</sup> PER CHILD REQUIRED = MAX. 88 CHILDREN  
CHILD AREA CALCULATED AT 2.5m<sup>2</sup> PER CHILD (+ 10% ALLOWANCE FOR FFE)



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Sketch Title  
Zone 1 L2  
Fire / Smoke Separations  
& Means of Escape

Drawn: ACC	Date: 02 / 05 / 2019
Project No. 136249	Sheet No. Z1FEB FS 103
Rev. A	

CHILD CARE FACILITY IS A PRELIMINARY CONCEPT AND IS SUBJECT TO CONFIRMATION. OUTS WILL BE THESE CONFIRMED.

Rev.	Date	Description	Iss.	Appr.
A	27.11.18	FOR COMMENT	BH	JB
B	10.01.19	PRELIMINARY DESIGN	BH	JB
C	05.02.19	FOR PRELIMINARY COSTING	TH	JB
D	14.03.19	FOR INFORMATION	BH	RM
E	21.03.19	PRELIMINARY DESIGN	BH	DA



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TAY STREET & DEE STREET CORNER  
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ZONE 1  
LEVEL 2 FLOOR PLAN  
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Z1-PD-A-1105

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## Appendix B Fire Modelling (FDS)

The following FDS model parameters applies to CF1, CF2 and RC1. CF3 will utilise B-Risk model.

### B.1 FDS Input parameters are used:

- Reaction based on the following fuel:  $C_{4.14}H_{9.11}O_{2.58}$ .
- The input yield quantities for CO, CO<sub>2</sub> and H<sub>2</sub>O are those described in C/VM2.

*The calculated yields using the fuel described above align with those required by C/VM2, as follows:*

$$y_{CO} = 0.04\text{kg/kg}$$

$$y_{CO_2} = 1.5\text{kg/kg}$$

$$y_{H_2O} = 0.82\text{kg/kg}$$

$$y_{soot} = 0.07\text{kg/kg (assuming } y_{soot} = y_C).$$

- The heat of combustion for the reaction is also specifically input as 20MJ/kg

The fire is modelled as a growing-area square burner, with heat release rate (HRR) input to grow as a 'fast' t<sup>2</sup> fire. In this manner, the overall HRRPUA of the burner is held virtually constant over time; the fire size grows as the physical size of the burner grows.

The maximum HRRPUA is expected to be within a range of 500 – 1000 kW/m<sup>2</sup> as per C/VM2.

Initially the model will be run with a fire that grows up to 20MW in order to determine sprinkler activation time. The time at which sprinkler activation occurs will be used to establish the peak HRR for subsequent models for this fire growth rate.

### B.2 FDS Output

Refer to Master Fire Engineering Brief (ref:136249FEB01) for details.

### B.3 FDS Grid Size

No grid sensitivity study will be performed on the FDS model for the 'fast' t<sup>2</sup> fire. It is assumed the grid sensitivity study carried out for the 'fast' t<sup>2</sup> fire in Zone 3 Carpark Fire Engineering Brief (ref:136249FEB02) is sufficient.

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# **Zone 1 – D.S. Anchor & Childcare Centre HWCP Invercargill CBD Development**

HWCP Management Ltd

**Fire Engineering Verification**

### Issue Authorisation

Project: Zone 1 – D.S. Anchor & Childcare Centre, HWCP Invercargill CBD Development

Project No. 136249

Version	Date	Status	Prepared	Reviewed
A	28 August 2019	For Approval	ACC	DXM
B	14 October 2019	For Approval	ACC	DXM

Version	Extent of Revision
B	Update in response to peer reviewer comments <ul style="list-style-type: none"><li>BE Scenario – Table 2</li><li>RSET for L1 Anchor</li></ul>

This report caters specifically for the requirements for this project and this client. No warranty is intended or implied for use by any third party and no responsibility is undertaken to any third party for any material contained herein. This report is produced and signed solely on behalf of Holmes Fire and no liability whatsoever accrues to the authors.

The building owner must be aware that the fire safety solutions described in this report may be alternative solutions to those given by the MBIE Acceptable Solutions or Verification Methods. Consideration of protection of the building owner's property is not included unless this has been specifically requested.

#### Written By:

#### Reviewed By:



AMY CHAO  
Fire Engineer  
BE(Hons), MEngSt (Fire)



DARIN MILLAR  
Principle  
BE(Hons), MEFireE, CMEngNZ, CPEng, IntPE(NZ)

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## 1 PURPOSE

The purpose of this document is to demonstrate that the proposed minimum fire safety precautions that are to be installed within the Zone 1 Anchor, HWCP Invercargill CBD Development at Invercargill, achieve compliance with Section 17 of the New Zealand Building Act 2004 with respect to the fire regulations, due to the proposed works.

This document is one of a number of documents prepared by the fire engineer:

- Master Fire Engineering Brief (FEB), ref: 136249FEB01(Master).
- Zone 3 Fire Engineering Brief (FEB), ref: 136249FEB03(D.S. Anchor & Childcare Centre).
- Zone 3 Fire Engineering Strategy (FES), ref: 136249FES01 (D.S. Anchor & Childcare Centre).
- Zone 3 Fire Engineering Sketches (FS).
- Zone 3 Fire Engineering Verification (FEV), ref: 136249FEV01 (D.S. Anchor & Childcare Centre).

The Fire Engineering Verification document is provided for regulatory approval and contains the calculations and engineering background to the fire safety design – the verification showing how the design solution meets the acceptance criteria.

## 2 FIRE SAFETY EVALUATION AND ANALYSIS METHODS

### 2.1 Evaluation Methods

Compliance with the Building Code for this project is achieved in accordance with the Verification Method: Framework for Fire Safety Design (C/VM2, July 2014) for New Zealand Building Code Clauses C1 – C6 (2012).

The fire engineering design has been evaluated by following the methodology of the Verification Method, and the analysis of Design Scenarios and associated calculations are detailed within this report.

The challenging fire scenarios have been completed including an ASET/RSET analysis; the fire modelling has been completed using the latest version of FDS (at the time modelling is commenced, version 6.7.1) for the Anchor space and B-Risk 2019.03 for the Childcare space, while the movement times of the occupants (traversal walking and flow times) has been carried out utilising the computer model EvacuationNZ for the Anchor space and hand calculations (by spreadsheet) for the Childcare space.

## 3 INTRODUCTION

Zone 1 is a three-storey structure consisting of a large anchor tenancy occupying the ground and level 1 space. In the centre of the ground floor are two elevators that leads from the ground floor to level one which creates an open void. Level one is therefore considered as an intermediate floor rather than fully fire separated first floor. Ground floor has three direction of egress; to the north (Esk St), south-east (Tay St) and south-west (mall) side of the building. Level one has three direction of egress via the north-east stair, south-east stair and the West side carpark. Small retail tenancies unrelated to the Anchor, are accessed directly from Esk St.

Level two is proposed to be a childcare centre that is accessed via the adjacent Zone 3 Carpark or the north-east stair.

For a full description of the different zones and their interrelationship, please refer to the Fire Engineering Briefs.

### 3.1 Correspondence post FEB

Refer to Appendices for Q&A log. There is no content in the Q&A log that alters the FEB content.

### 3.2 Building Use and Fire Design Occupant Loads

The following is a summary of the activities and fire design occupant loads within the building, determined in accordance with C/VM2 Table 3.1.

Table 1 - Occupant Load summary

Location	Activity	Area (m <sup>2</sup> )	Occ Density (m <sup>2</sup> /person)	Occ Load (ppl)
G	Anchor	2091	3.33 <sup>1</sup>	628
G	Esk St tenancy A	119	3.5	34
G	Esk St tenancy B	121	3.5	35
G	Esk St tenancy C	120	3.5	34
G	Esk St tenancy D	115	3.5	33
G	B.O.H (Reserve)	110	100	1
	<b>GF Anchor</b>			<b>765</b>
L1	Anchor	2310	3.33 <sup>1</sup>	694
L1	B.O.H (Reserve)	313	100	3
L1	Offices	217	10	22
	<b>L1 Anchor</b>			<b>719</b>
	<b>ANCHOR SPACE</b>			<b>1484</b>
L2	Childcare Centre	-		88 children + 12 staff
<b>ZONE 1 BUILDING TOTAL</b>				<b>1572</b>

#### Explanatory Notes

1. Anchor tenant seeks to have their occupant density to be 3.33p/m<sup>2</sup> as opposed to 3.5p/m<sup>2</sup>.
2. The exact occupant load for the Childcare Centre is yet to be confirmed. However, due to the restriction to external play area, a maximum of 88 children is permitted in the Childcare Centre.

#### 4 SUMMARY OF DESIGN SCENARIO COMPLIANCE

Table 2 below identifies C/VM2 fire scenarios in relation to the building assessment. Reference should be made to the FEB and stakeholder agreement correspondence (Appendix F) for the stakeholder agreed fire design methodology.

Table 2 - Design Scenario Applicability: Summary

Design Scenario	Description	Further Verification Required?	Comment / Reference
BE	Blocked Exit	No	All areas with occupant load greater than 50 people have no less than two exits available and have a dead-end travel distance less than 40 m for occupants not familiar with the building. Both the GF and 1L anchor spaces have occupant load > 250 people. Each level has three designated egresses > 8.0 m apart. 1L anchor space have two stairwells more than 8.0 m apart with the third egress via the carpark. The carpark also has two stairwells more than 20 m apart, each serving more than 250 people.
UT	Unoccupied room, Threatening other rooms	No	Fire suppression is provided by way of sprinkler protection throughout building.
CS	Concealed Space Fire	No	All areas in building provided with automatic detection (sprinklers).
SF	Smouldering Fire	No	Smoke detection in sleeping areas, designed and installed to a recognised national or international standard.
HS	Horizontal Fire Spread	No	Refer to Section 4.1 below.
VS	Vertical Fire Spread	No	Part A: Either by Table 4.2 of C/VM2 or use of non-combustible material. Part B & Part C: The building is provided with automatic sprinkler system.
IS	Internal Surfaces Fire Spread	No	Compliance with NZBC C3.4 is required. Proposed to comply with internal surface finish requirements in accordance with C/VM2 and appropriate C/AS.
FO	Firefighting Operations	Yes	The proposed firefighting facilities for the building, e.g. the fire alarm panel, sprinkler inlets and internal hydrant inlets and outlets, are being addressed directly with FENZ with the agreement with FENZ consolidated in a separate document.  Burnout calculation has been assessed and presented in the summary table below in Section 4.2 and in Appendix A.

Rev B

Design Scenario	Description	Further Verification Required?	Comment / Reference
CF	Challenging Fire	Yes	Three challenging fires has been assessed. Refer to Section 4.3 for a summary of results. Refer to Appendix B for RSET assessment. Refer to Appendix C for ASET assessment. Refer to Appendix D for Smoke Barrier Assessment.
RC	Robustness Check	Yes	Refer to section 4.5 below for a summary of results. Refer to Appendix C for ASET assessment.

#### 4.1 Horizontal Fire Spread

The Anchor building is 40 m from the south relevant boundary across Tay Street and is 19 m from the north relevant boundary across Esk Street. The east side is 6 m from the relevant boundary and the west side faces the Carpark building. Based on the location of relevant boundary and provision of the sprinkler system with independent water supply, 100% unprotected opening on all levels of Zone 1 is acceptable. Refer to Appendix A for overall site plan that showed the relevant boundaries.

The building is provided with automatic sprinkler system with two independent water supplies, one of which is not dependent on town mains and the building shall not be used for storage above 3.0 m.

#### 4.2 Fire Resistance Ratings Summary

The burnout fire resistance rating calculation for the relevant firecells within the building is summarised below, with calculations included in Appendix A.

Table 3 - Firecell Burnout Summary

Firecell	Calculated FRR (min)	FRR Applied to Building (min)
Anchor Building	60	60
L2 Childcare	60	60
L1 Anchor (Intermediate Floor) <sup>1</sup>	30	30

Explanatory Notes:

- Level 1 Anchor is considered as intermediate floor due to the escalator atrium opening that connects ground floor and Level 1. In accordance with C/VM2 section 4.8, for buildings with an escape height is less than 10 m, intermediate floor and supporting structure shall be provided with an FRR of (30)/30/30. The total intermediate floor area is more than 40% of the firecell area, thus integrity and insulation ratings need to apply to the intermediate floor.

### 4.3 Challenging Fire ASET vs RSET Summary

Table 4 - ASET v RSET Summary

Scenario	Location <sup>1</sup>	ASET (s)	RSET (s)		ASET > RSET
			Base-Case	Non-Base Case	
CF1 (Atrium)	GF Anchor	>1700	209	199	Yes
	L1 Anchor	328	282	284	Yes
	L0 Stair 3 Landing <sup>2</sup>	>1700	295	287	Yes
	L0 Stair 4 Landing <sup>3</sup>	>1700	267	273	Yes
	N Circulation <sup>4</sup>	>1700	-	348	Yes
	Corridor <sup>5</sup>	>1700	-	1537	Yes
	Childcare	>1700	783		Yes
CF2 (Spill plume)	GF Anchor	>1700	193	183	Yes
	L1 Anchor	362	266	268	Yes
	L0 Stair 3 Landing <sup>2</sup>	>1700	279	271	Yes
	L0 Stair 4 Landing <sup>3</sup>	>1700	251	332	Yes
	N Circulation <sup>4</sup>	>1700	-	515	Yes
	Corridor <sup>5</sup>	>1700	-	1521	Yes
	Childcare	>1700	767		Yes
CF3 (Childcare)	GF Anchor	>1700	227	217	Yes
	L1 Anchor	>1700	270	272	Yes
	L0 Stair 3 Landing <sup>2</sup>	>1700	283	275	Yes
	L0 Stair 4 Landing <sup>3</sup>	>1700	255	261	Yes
	N Circulation <sup>4</sup>	>1700	-	350	Yes
	Corridor <sup>5</sup>	>1700	-	1521	Yes
	Childcare	917	711		Yes

Explanatory Notes:

- 1) Location is the space represented as nodes in EvacuationNZ.
- 2) 'L0 Stair3 Landing' is the node that corresponds to the space precede the final exit from Stair 3 (L1 Anchor north stairwell) which is shared by the occupants from L2 Childcare space.
- 3) 'L0 Stair4 Landing' is the node that corresponds to the space precede the final exit from Stair 4 (i.e. time to clear L1 Anchor south stairwell).
- 4) 'N Circulation' is the node that corresponds to the space preceding the final exit from the Zone 2 mall area.

- 5) 'Corridor' is the node that corresponds to the space preceding the final exit from the north stairwell from the Zone 3 Carpark area.

As per the above table, ASET > RSET for all locations.

#### 4.4 Grid Resolution Study Summary

Grid resolution study has been assessed in Zone 3 Carpark Fire Engineering Verification Report (136249FEV02) for both a 0.0117t<sup>2</sup> 'medium' fire and 0.0469t<sup>2</sup> 'fast' fire. The results showed minimal difference between the results produced from the 0.1 m and the 0.2 m mesh grid sizes which supports the justification that a 0.2 m grid cell size in the near field mesh is adequate for the purpose of life safety assessment. Therefore, no further assessment has been carried out for Zone 1.

#### 4.5 Robustness Check

Robustness Check Scenario (RC1) has utilised CF1 with the failure of the smoke exhaust system. A fire in the atrium is considered a worst-case scenario with the largest fire due to the high-ceiling space. For this scenario, only FEDco has been assessed. The doors are still expected to power open.

Table 5 - RC1 ASET v RSET Summary

Scenario	Location <sup>1</sup>	ASET (s)	RSET (s)		ASET > RSET
			Base-Case	Non-Base Case	
CF1 (Atrium)	GF Anchor	>1700	212	202	Yes
	L1 Anchor	1610	285	287	Yes
	L0 Stair 3 Landing <sup>2</sup>	1610	298	290	Yes
	L0 Stair 4 Landing <sup>3</sup>	1644	270	276	Yes
	N Circulation <sup>4</sup>	>1700	-	351	Yes
	Corridor <sup>5</sup>	>1700	-	1540	Yes
	Childcare	>1700	786		Yes

Rev B

Explanatory Notes:

- 1) Location is the space represented as nodes in EvacuationNZ.
- 2) 'L0 Stair3 Landing' is the node that corresponds to the space precede the final exit from Stair 3 (L1 Anchor north stairwell) which is shared by the occupants from L2 Childcare space.
- 3) 'L0 Stair4 Landing' is the node that corresponds to the space precede the final exit from Stair 4 (i.e. time to clear L1 Anchor south stairwell).
- 4) 'N Circulation' is the node that corresponds to the space preceding the final exit from the Zone 2 mall area.
- 5) 'Corridor' is the node that corresponds to the space preceding the final exit from the north stairwell from the Zone 3 Carpark area.

As per the above table, ASET > RSET for all locations.

#### 4.6 Smoke Barrier (ULT) Summary

The wall between the Level 1 Anchor and Level 1 carpark is intended to perform as a smoke barrier including the glazed partition. The Smoke Barrier assessment is not applicable for Zone 1 assessment on its own but have been provided as requested in Q&A log from stakeholders for future reference.

Temperature slice file has been placed in front of the wall between Anchor and carpark/mall.

As per Appendix D, the average upper layer temperature on the Anchor side did not exceed 200°C for the duration of fire model from both ground floor and first floor, hence any “smoke barrier” is considered to achieve smoke control performance for the duration of RSET.

Table 6 - Smoke Barrier Summary

Scenario	Location	Temperature (°C)
CF1	GF (between Anchor and Mall)	<50
	L1 (between Anchor and Carpark)	<50
CF2	GF (between Anchor and Mall)	<117
	L1 (between Anchor and Carpark)	<30
RC1	GF (between Anchor and Mall)	<40
	L1 (between Anchor and Carpark)	<80



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## Appendix A Design Scenario FO

To achieve C/VM2 Design Scenario FO, refer to the FENZ fire fighting facilities correspondence in a separate document.

Further to the correspondence with FENZ, for the purposes of NZBC C5.5:

- Internal hydrants are located in the north-east and south-east stairwell.

For the purposes of NZBC C6.3, burnout calculation has been carried out as per Section A.1 below. The south-east and north-east stairwell have been designed as exitways with the following fire resistance rating:

- The south-east stairwell that leads to Tay Street is provided with an FRR of (60)/60/60.
- The north-east stairwell that leads to Esk Street is provided with an FRR of (60)/60/60.

Master fire control room, FAP, mimic, FSI and HI locations are as per the FENZ firefighting facilities correspondence provided separately.

### A.1 Burnout Calculation

Fire resistance rating to withstand full burnout is calculated using the Eurocode method (refer comment to paragraph 2.4 of C/VM2):

Both the ground floor and Level 1 of the anchor space is considered as the same firecell due to the escalator atrium that connects both floors. The burnout fire resistance rating calculation for the Anchor firecell and the childcare firecell is summarised below, with calculations included in Appendix A.1.

Table 7 - Firecell Burnout Summary

Firecell	FHC	Floor Area (A <sub>f</sub> ) (m <sup>2</sup> )	Openings (m <sup>2</sup> )		Rating to withstand burnout (min.)	Proposed FRR (min.)
			Vertical A <sub>v</sub> (A <sub>v</sub> /A <sub>f</sub> )	Horizontal A <sub>h</sub> (A <sub>h</sub> /A <sub>f</sub> )		
Anchor (GF & L1)	2	3549	224.6	n/a	41	60
Anchor (GF only)	2	3510	191	144.4	43	60
Anchor (L1 - concrete roof)	2	3330	33.6	n/a	79	-
Anchor (L1 - thin sheet steel roof)	2	3330	33.6	n/a	49	-
			Weighted average		58	60
Childcare	2	569	69	n/a	40	60

Level 1 Anchor is considered as intermediate floor due to the escalator atrium opening that connects ground floor and Level 1 and are provided with an FRR of (30)/30/30. The total intermediate floor area is more than 40% of the firecell area, thus integrity and insulation ratings need to apply to the intermediate floor.

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- Anchor Burnout Calculation
- L2 Childcare Burnout Calculation
- FSKA.1.01 - FSKA.1.03

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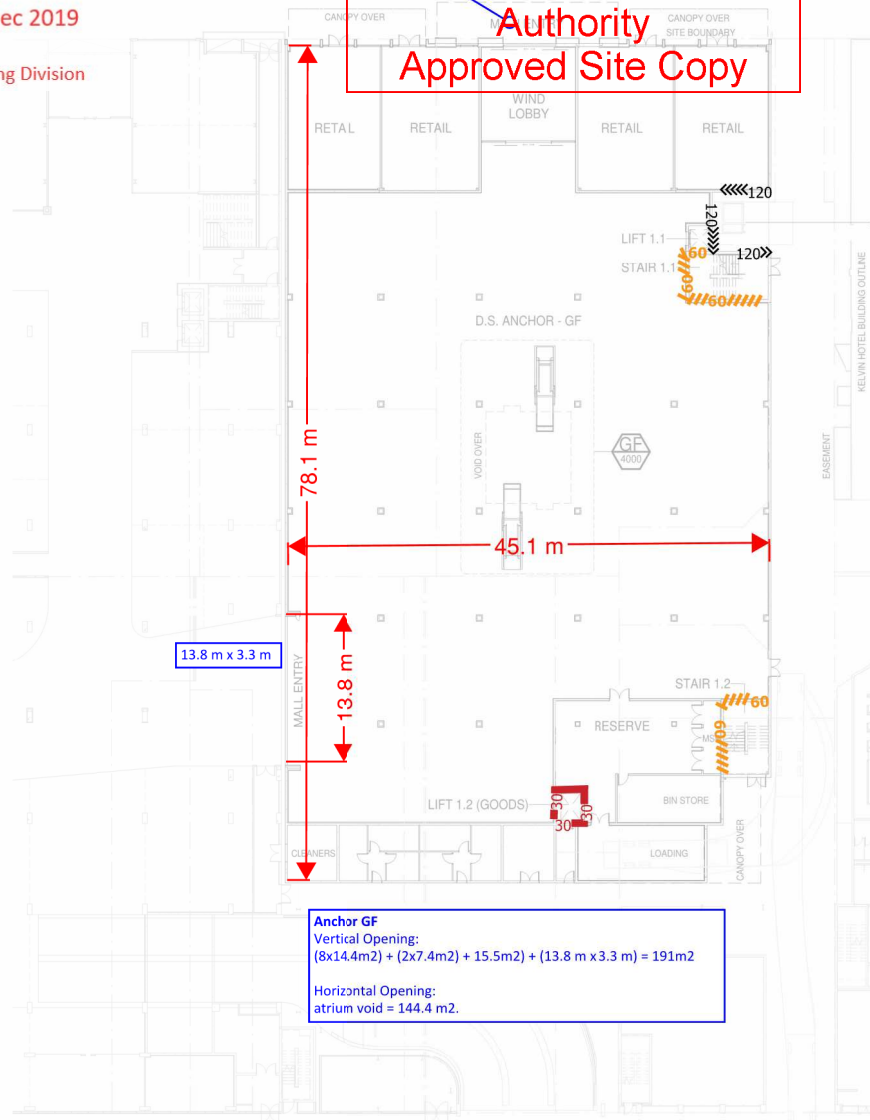
**Appendix A.1 - Burnout Calculation**

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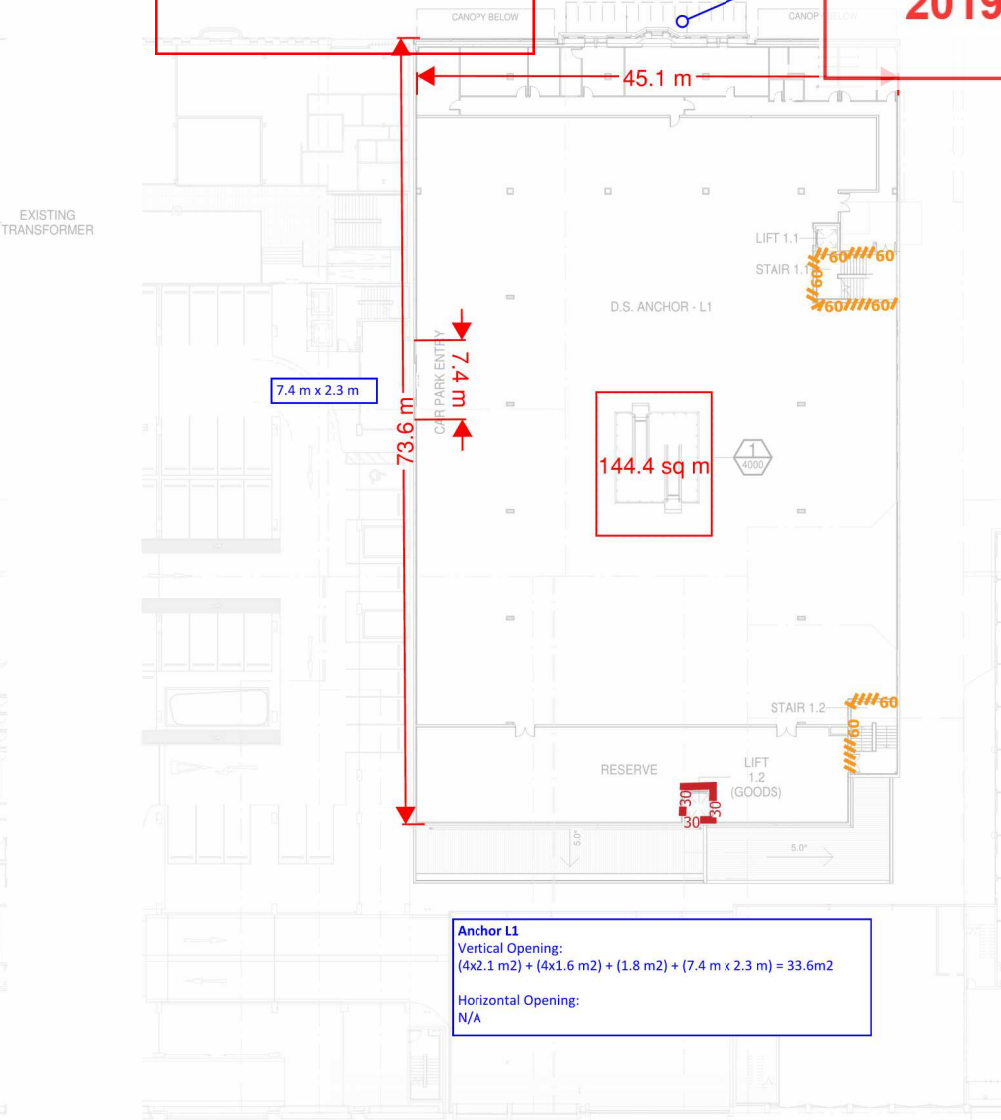
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GF North Elevation Vertical Opening  
(8x14.4m<sup>2</sup>) + (2x7.4m<sup>2</sup>) + 15.5m<sup>2</sup>

L1 North Elevation  
(4x2.1 m<sup>2</sup>) + (4x1.6 m<sup>2</sup>) + (1.8 m<sup>2</sup>)



**Anchor GF**  
Vertical Opening:  
(8x14.4m<sup>2</sup>) + (2x7.4m<sup>2</sup>) + 15.5m<sup>2</sup> + (13.8 m x 3.3 m) = 191m<sup>2</sup>  
Horizontal Opening:  
atrium void = 144.4 m<sup>2</sup>.



**Anchor L1**  
Vertical Opening:  
(4x2.1 m<sup>2</sup>) + (4x1.6 m<sup>2</sup>) + (1.8 m<sup>2</sup>) + (7.4 m x 2.3 m) = 33.6m<sup>2</sup>  
Horizontal Opening:  
N/A

**GF Z1 - GROUND FLOOR - OVERALL**  
1:250

**1 Z1 - LEVEL 1 - OVERALL**  
1:250

	Holmes Fire LP L2, 254 Montreal St Christchurch New Zealand T: +64 3 365 8855 holmesfire.com	Project Title	Sketch Title	Drawn: ACC	Date: 31 / 07 / 2019
		HWCP - Invercargill Central	Zone 1 Anchor Burnout Calculation Measurement	Project No. <b>136249</b>	Sheet No. <b>FSK A.1.01</b>

Rev.	Date	Description	Iss. Appr.	By	Project
A	07/11/19	FOR COMMENT	SH	JB	
B	10/01/19	PRELIMINARY DESIGN	SH	JB	
C	21/03/19	PRELIMINARY DESIGN	SH	DA	
D	17/04/19	FOR INFORMATION	JT	DA	

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**INVERCARGILL CENTRAL - ZONE 1**  
TAY STREET & DEE STREET CORNER  
INVERCARGILL

Project Number  
917077

Status  
PRELIMINARY DESIGN

Issue Period  
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Issue Number  
21/03/19

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Drawing Title  
**ZONE 1 OVERALL FLOOR PLANS**

Drawing Number  
**Z1-PD-A-1100**

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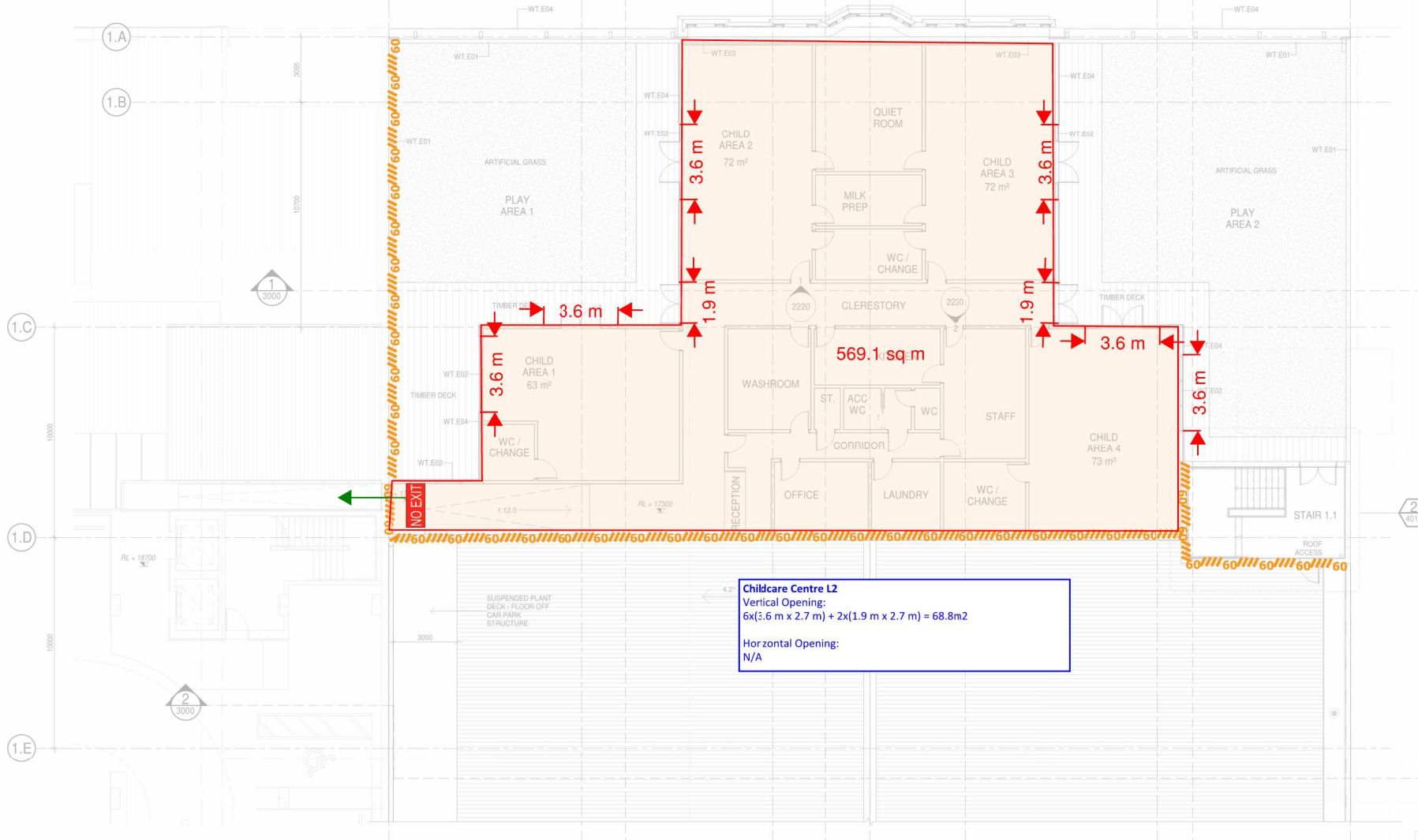
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Appendix A.1 - Burnout Calculation

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NOTE:  
 EXTERNAL PLAY AREA = 440m²  
 5m² PER CHILD REQUIRED = MAX. 88 CHILDREN  
 CHILD AREA CALCULATED AT 2.5m² PER CHILD  
 (+ 10% ALLOWANCE FOR FFE)

<p>Holmes Fire LP                  L2, 254 Montreal St                  Christchurch                  New Zealand                  T: +64 3 365 8855                  holmesfire.com</p>	Project Title <b>HWCP - Invercargill Central</b>	Sketch Title <b>Zone 1 L2 Childcare                  Burnout Calculation                  Measurement</b>	Drawn: ACC Date: 31 / 07 / 2019
	Project No. <b>136249</b>	Sheet No. <b>FSK A.1.02</b>	Rev <b>A</b>

CHILD CARE FACILITY IS A  
 PRELIMINARY CONCEPT AND IS  
 PENDING OPERATORS  
 REQUIREMENTS. LAYOUTS WILL  
 LIKELY CHANGE ONCE THESE  
 REQUIREMENTS ARE CONFIRMED.

Rev.	Date	Description	Iss. Appr.	Keyplan
A	07.11.19	FOR COMMENT	BH JB	
B	19.01.19	PRELIMINARY DESIGN	BH JB	
C	05.02.19	FOR PRELIMINARY COSTING	TH JB	
D	14.02.19	FOR INFORMATION	BH JB	
E	21.03.19	PRELIMINARY DESIGN	BH JB	

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Drawing Title  
**ZONE 1  
 LEVEL 2 FLOOR PLAN**

Drawing Number  
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Appendix A.1 - Burnout Calculation

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			Project No.      Sheet No.      Rev <b>136249</b> <b>FSK A.1.03</b> <b>A</b>

Rev.	Date	Description	Rev.	Appr.
A	15.02.19	PRELIMINARY DESIGN	MR	DR
B	05.02.19	FOR PRELIMINARY COSTING	MR	DR
C	15.02.19	FOR INFORMATION	DR	DA

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Project Number  
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 Date Revised: 10.01.19  
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Drawing Title  
**ZONE 1  
 PROPOSED ELEVATIONS**

Drawing Number  
**Z1-DD-A-2000**

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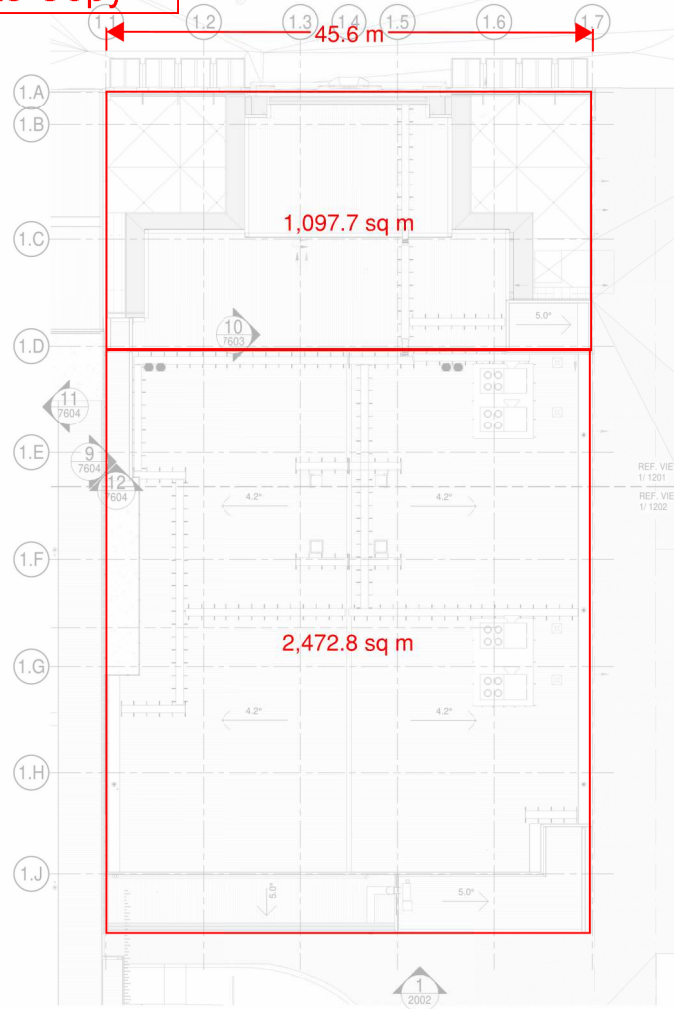
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Appendix A.1 - Burnout Calculation

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			Project No.      Sheet No.      Rev	136249      FSK A.1.04      A	

Rev	Date	Description	By	Appr.
A	27.11.19	FOR COMMENT	BH	JD
B	19.01.19	PRELIMINARY DESIGN	BH	JD
C	21.03.19	PRELIMINARY DESIGN	BH	DA
D	16.06.19	FOR INFORMATION	DR	DA

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**HWCP**

Project  
**INVERCARGILL CENTRAL - ZONE 1**  
 TAY STREET & DEE STREET CORNER  
 INVERCARGILL

Project Number  
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Status  
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Date Plotted: 7/08/2019 9:38:10 AM  
 Date Issued: 21.03.19  
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**ZONE 1  
 OVERALL ROOF PLAN**

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 Z1-DD-A-1200

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 D

Document Received

17 Dec 2019

Building Division

WT.EI	PRECAST CONCRETE PANELS TO STRUCTURAL ENGINEERS DETAILS
WT.EI	13mm GIB PLASTERBOARD LINING OVER TIMBER STRAPPING STOPS 100mm ABOVE CEILING LEVEL LINING STEPS BACK AT BASE. REFER TO SPECIFICATION FOR DETAILS.
WT.I0	190x45 H1.2 TIMBER STUDS @ 400cs & DWANGS @ 800cs. 13 GIB PLASTERBOARD TO BOTH SIDES OF WALL, STOPPED TO LEVEL 4, PAINT FINISH
WT.I03	13mm PLASTERBOARD LINING OVER TIMBER STRAPPING STOPS 100mm ABOVE CEILING LEVEL LINING STEPS BACK AT BASE. REFER TO SPECIFICATION FOR DETAILS.
WT.I07	190x45 H1.2 TIMBER STUDS @ 400cs & DWANGS @ 800cs. 13 GIB PLASTERBOARD TO BOTH SIDES OF WALL, STOPPED TO LEVEL 4, PAINT FINISH

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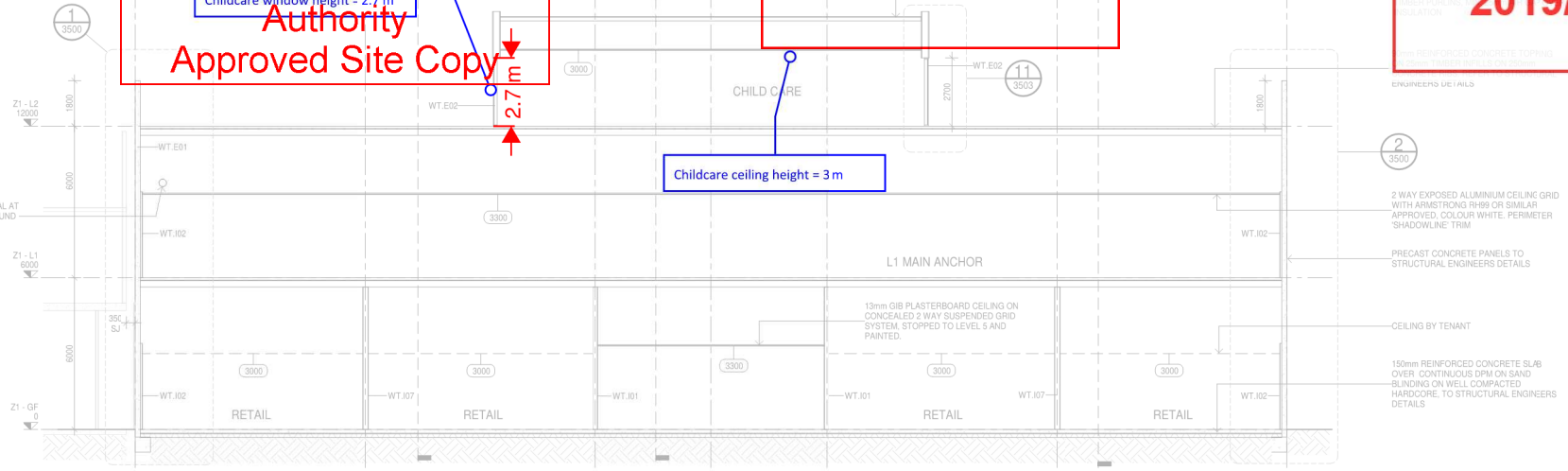
Appendix A.1 - Burnout Calculation

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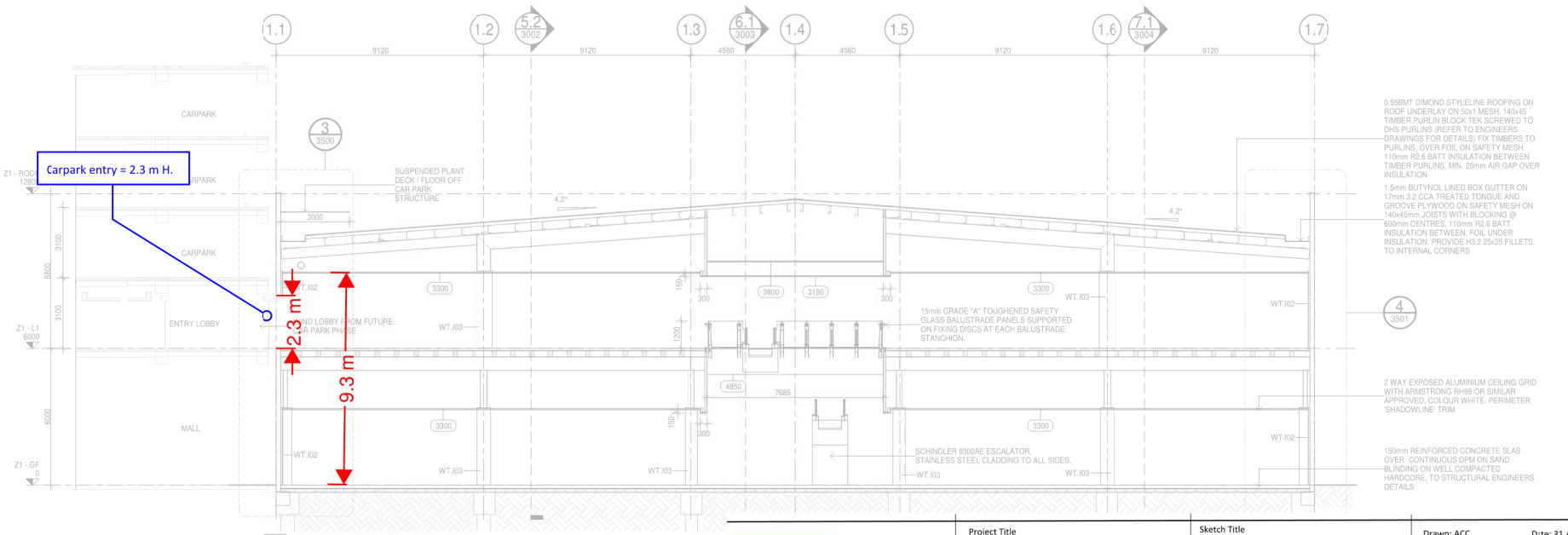
Childcare window height = 2.7 m

Childcare ceiling height = 3 m

**BUILDING CONSENT NUMBER**  
**2019/1381**



1 Z1 - MAIN SECTION 1  
1:100



2 Z1 - MAIN SECTION 2  
1:100



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Project Title  
**HWCP - Invercargill Central**

Sketch Title  
**Zone 1 Burnout Calculation Measurement - Sections**

Drawn: ACC	Date: 31 / 07 / 2019	
Project No. 136249	Sheet No. FSK A.1.05	Rev A

Rev	Date	Description	Iss. Appr.	Rev	Appr.
1	27/11/18	FDM COMMENT			

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**HWCP**

PROJECT  
**INVERCARGILL**  
TAY STREET & DEE STREET CORNER  
INVERCARGILL

Issue/Rev: 1/30 Dec 19 2:32:27 PM  
Date Issued: 27/11/18  
Scale: 1:100 @A

MAIN SECTION 1 & 2  
Drawing Number  
Z1-PD-3000

Revision  
**A**

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PRELIMINARY

**BUCHAN**

17 Dec 2019

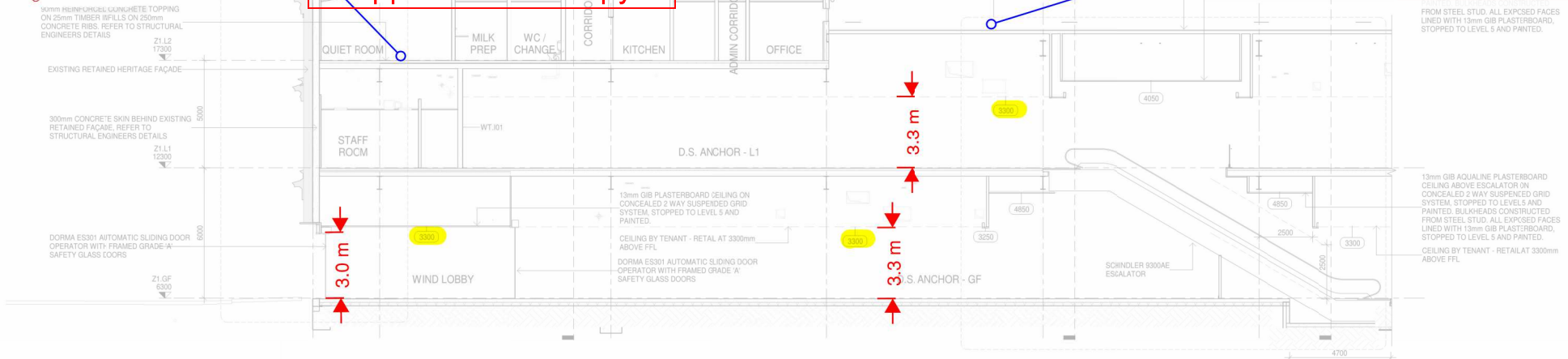
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Authority  
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Appendix A.1 - Burnout Calculation

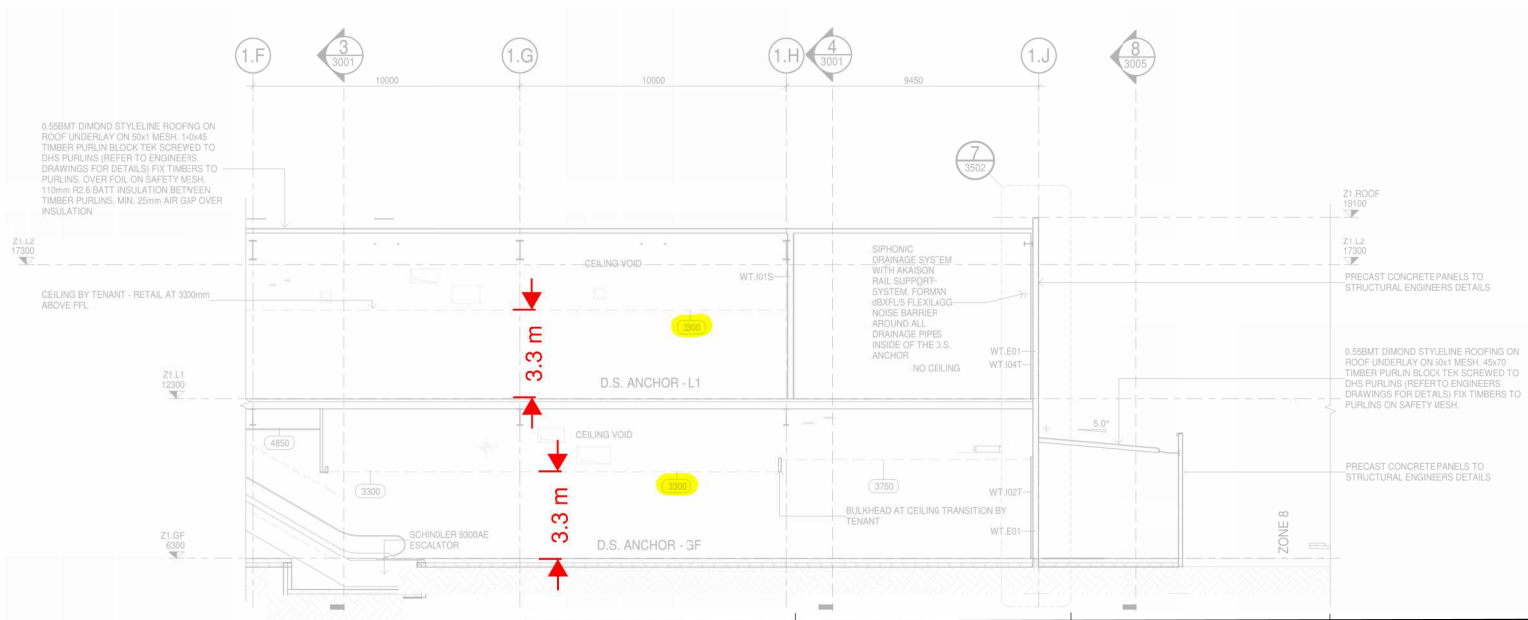
Approved For Issue  
27/02/2020

**BUILDING CONSENT NUMBER**  
**2019/1381**



6.1 Z1 - MAIN SECTION 6 - PART 1  
1:100

WALL TYPES	
WALL CODE	DESCRIPTION
WT.E01	PRECAST CONCRETE PANELS TO STRUCTURAL ENGINEERS DETAILS
WT.E03	300mm CONCRETE SKIN BEHIND EXISTING RETAINED FACADE, REFER TO STRUCTURAL ENGINEERS DETAILS
WT.I01	190x45 H1.2 TIMBER STUDS @ 400cs & DWANGS @ 800cs. 13mm GIB PLASTERBOARD TO BOTH SIDES OF WALL, STOPPED TO LEVEL 4. PAINT FINISH. 17mm FULL HEIGHT PLYWOOD BETWEEN PLASTERBOARD AND FRAMING TO DS ANCHOR SIDE. FULL HEIGHT WALL TO U/S OF SLAB
WT.I01S	190x45 H1.2 TIMBER STUDS @ 400cs & DWANGS @ 800cs. 13mm GIB PLASTERBOARD TO BOTH SIDES OF WALL, STOPPED TO LEVEL 4. PAINT FINISH. 17mm FULL HEIGHT PLYWOOD BETWEEN PLASTERBOARD AND FRAMING TO DS ANCHOR SIDE. SMOKE SEPARATION REQUIRED. R2.2 BATTS TO ACHIEVE GIB SYSTEM GST132 FOR ACUSTICS. FULL HEIGHT WALL TO U/S OF SLAB
WT.I02T	70mm H1.2 TIMBER STRAPPING @ 600cs. ON DPC WITH 13mm PLASTERBOARD TAKEN 100mm ABOVE CEILING LEVEL ONE SIDE. 70mm LDF 120 TO 70mm SEGMENTS BETWEEN STRAPPING UP TO UNDERSIDE OF CONCRETE SLAB, R2.2 BATTS
WT.I04T	70mm H1.2 TIMBER STRAPPING ON DPC WITH 12mm MDF ONE SIDE, ONE COAT OF CLEAR POLYURETHANE. 70mm LDF TO 70mm SEGMENTS BETWEEN STRAPPING UP TO UNDERSIDE OF CONCRETE SLAB, MINIMUM VALUE OF R2.2 BULKHEAD AT CEILING TRANSITION BY TENANT
WT.I32	BULKHEAD AT CEILING TRANSITION BY TENANT



6.2 Z1 - MAIN SECTION 6 - PART 2  
1:100

No.	Date	Description	Rev.	Appr.	Region
A	27.11.19	FOR COMMENT	001	AS	ZONE 1
B	03.02.19	PRELIMINARY DESIGN	001	AS	ZONE 1
C	03.02.19	FOR PRELIMINARY COSTING	001	AS	ZONE 1
D	14.02.19	FOR INFORMATION	001	AS	ZONE 1
E	21.03.19	PRELIMINARY DESIGN	001	DA	ZONE 1
F	15.02.19	FOR INFORMATION	001	DA	ZONE 1

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Project  
**INVERCARGILL CENTRAL - ZONE 1**  
TAY STREET & DEE STREET CORNER  
INVERCARGILL

Project Number  
917077



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Project Title  
**HWCP - Invercargill Central**

Sketch Title  
**Zone 1  
Burnout Calculation  
Measurement - Sections**

Drawn: ACC	Date: 31 / 07 / 2019
Project No. 136249	Sheet No. FSK A.1.06
	Rev A

Status  
DEVELOPED DESIGN

Date Posted 7/08/2019 9:30:31 AM

Date Issued 21.03.19

Scale 1:100 @ A1

Drawing Title  
**ZONE 1  
MAIN SECTION 6**

Drawing Number  
Z1-DD-A-3003

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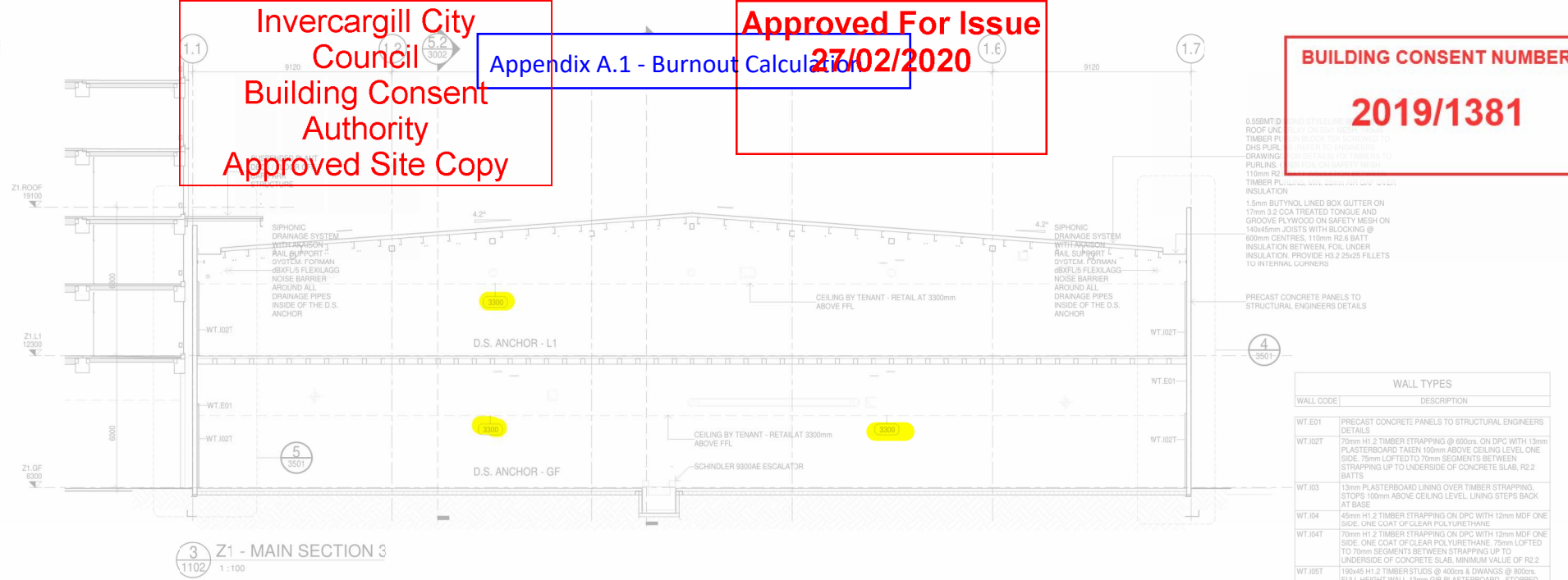


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Appendix A.1 - Burnout Calculation

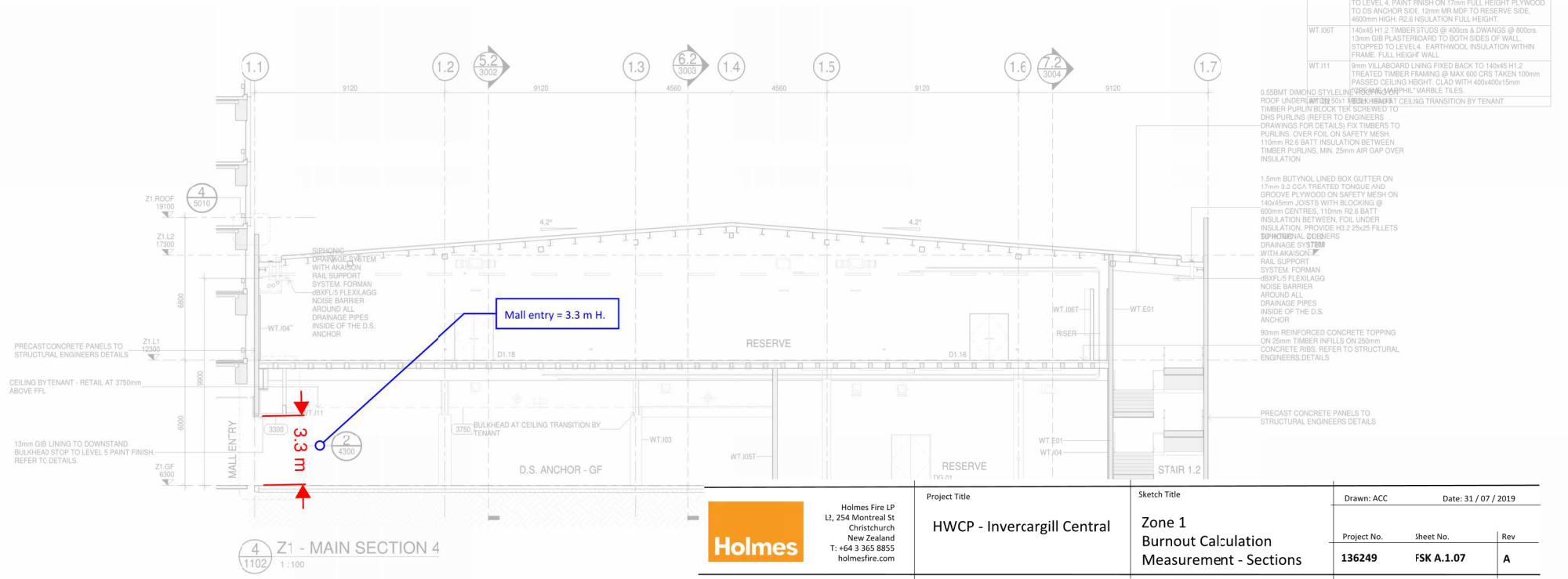
Approved For Issue  
27/02/2020

BUILDING CONSENT NUMBER  
2019/1381



WALL TYPES	
WALL CODE	DESCRIPTION
WT.E01	PRECAST CONCRETE PANELS TO STRUCTURAL ENGINEERS DETAILS
WT.I02T	70mm H1 2 TIMBER STRAPPING @ 600cs. ON DPC WITH 13mm PLASTERBOARD TAKEN 100mm ABOVE CEILING LEVEL ONE SIDE. 75mm LOFTED TO 70mm SEGMENTS BETWEEN STRAPPING UP TO UNDERSIDE OF CONCRETE SLAB, R2.2 BATTS
WT.I03	13mm PLASTERBOARD LINING OVER TIMBER STRAPPING, STOPS 100mm ABOVE CEILING LEVEL. LINING STEPS BACK AT BASE
WT.I04	45mm H1 2 TIMBER STRAPPING ON DPC WITH 12mm MDF ONE SIDE. ONE COAT OF CLEAR POLYURETHANE
WT.I04T	70mm H1 2 TIMBER STRAPPING ON DPC WITH 12mm MDF ONE SIDE. ONE COAT OF CLEAR POLYURETHANE. 75mm LOFTED TO 70mm SEGMENTS BETWEEN STRAPPING UP TO UNDERSIDE OF CONCRETE SLAB, MINIMUM VALUE OF R2.2
WT.I05T	190x45 H1 2 TIMBER STUDS @ 400cs & DWANGS @ 800cs FULL HEIGHT WALL. 13mm GIB PLASTERBOARD, STOPPED TO LEVEL 4. PAINT FINISH ON 17mm FULL HEIGHT PLYWOOD TO DS ANCHOR SIDE. 120mm MDF TO RESERVE SIDE. 4600mm HIGH. R2.6 INSULATION FULL HEIGHT.
WT.I06T	140x45 H1 2 TIMBER STUDS @ 400cs & DWANGS @ 800cs. 13mm GIB PLASTERBOARD TO BOTH SIDES OF WALL, STOPPED TO LEVEL 4. EARTHWOOL INSULATION WITHIN FRAME. FULL HEIGHT WALL.
WT.I11	9mm VILLABARD LINING FIXED BACK TO 140x45 H1 2 TREATED TIMBER FRAMING @ MAX 600 CRS TAKEN 100mm PASSED CEILING HIGHT. CLAD WITH 400x400x15mm 0.55BMT DIAMOND STYLELINE 'PERMAMARPHIL' MARBLE TILES.

3 Z1 - MAIN SECTION 3  
1102 1:100



4 Z1 - MAIN SECTION 4  
1102 1:100



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Project Title  
HWCP - Invercargill Central

Sketch Title  
Zone 1  
Burnout Calculation  
Measurement - Sections

Drawn: ACC	Date: 31 / 07 / 2019
Project No. 136249	Sheet No. FSK A.1.07
	Rev A

Rev.	Date	Description	Rev.	Appr.	Region
A	27.11.18	FOR COMMENT	SH	JD	CDW
B	28.01.19	PRELIMINARY DESIGN	SH	JD	CDW
C	21.03.19	PRELIMINARY DESIGN	SH	DA	CDW
D	06.06.19	FOR INFORMATION	SH	DA	CDW
E	15.09.19	FOR INFORMATION	SH	DA	CDW



Project  
INVERCARGILL CENTRAL - ZONE 1  
TAY STREET & DEE STREET CORNER  
INVERCARGILL  
Project Number  
917077

Status  
DEVELOPED DESIGN  
Date Posted 7/08/2019 9:40:19 AM  
Date Issued 21.03.19  
Scale 1:100 @ A1

Drawing Title  
ZONE 1  
MAIN SECTION 3 & 4  
Drawing Number  
Z1-DD-A-3001

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Building Division Fire Severity Calculation

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Burnout

BUILDING CONSENT NUMBER

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Ref 1: Spearpoint, M.J., Fire Engineering Design Guide - Third Edition,  
Centre for Advanced Engineering, University of Canterbury, 2008. Ch. 6.4  
Ref 2: C/VM2 Verification Method: Framework for Fire Safety Design (July 2014)  
For New Zealand Building Code Clauses C1-6 Protection from Fire

Job No.	136249
Project Name:	HWCP Zone 1 Anchor
By:	ACC
Space:	Anchor - GF & L1

Whole building - including  
both ground floor and level 1

$t_e = e_f k_b k_m w_f$  (minutes)  
where:

- $t_e$  = Time equivalence fire severity
- $e_f$  = Design fire load energy density
- $k_b$  = Thermal properties conversion factor
- $w_f$  = Ventilation factor
- $k_m$  = Modification factor for load-bearing structure material

<p>Firecell lining materials = Normal weight concrete ceiling and floors</p> <p>Fire cell width, W = 45.5 m</p> <p>Fire cell length, L = 78 m</p> <p>Fire cell height, H = 9.3 m</p> <p>Floor area, <math>A_f</math> = 3549.0 m<sup>2</sup></p> <p>Vertical openings, <math>A_v</math> = 224.6 m<sup>2</sup></p> <p>Horizontal openings, <math>A_h</math> = m<sup>2</sup></p> <p>Fire Load Energy Density = 800 MJ/m<sup>2</sup></p> <p><math>F_m</math> factor for FLED = Sprinklered: structural elements C/VM2 Table 2.2</p> <p><b>Burnout Rating for firecell, <math>t_e</math> = 41 minutes</b></p>	<p><math>k_b = 0.065</math></p> <p><math>w_f = (6/H)^{0.3} \cdot [0.62 + 90 \cdot (0.4 + H \cdot 27)^{0.4} / (1 + (b_v \cdot H \cdot 28))]</math></p> <p>Calculated <math>w_f = 1.56</math></p> <p>Use <math>w_f = 1.56</math></p> <p>Calculated <math>\alpha_v = A_v/A_f = 0.063</math></p> <p>Use <math>\alpha_v = A_v/A_f = 0.063</math></p> <p><math>\alpha_h = A_h/A_f = 0.00</math></p> <p><math>b_v = 20</math></p> <p>FLED = 812 MJ</p> <p><math>F_m = 0.50</math></p> <p><math>e_f = 406</math> MJ</p>	<p><math>w_f &gt;= 0.50</math> (C/VM2)</p> <p><math>0.025 &lt;= \alpha_v &lt;= 0.25</math> (C/VM2)</p> <p><math>b_v &gt;= 10</math></p>
<p>Rating for structural material = Unprotected steel members</p> <p><math>A_v</math> Height of Openings, <math>h_{eq} = 2.3</math> m (relevant to unprotected steel, only)</p> <p>Time equivalence value, <math>t_e = 41</math> minutes</p>	<p><math>k_m = 1.00</math></p> <p><math>A_v(h_{eq})0.5/At = 0.036</math></p>	<p><math>k_m &gt;= 1</math> (C/VM2)</p> <p><math>0.02 &lt;= t_e &lt;= 0.20</math></p>

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Ref 1: Spearpoint, M.J., Fire Engineering Design Guide - Third Edition,  
Centre for Advanced Engineering, University of Canterbury, 2008. Ch. 6.4  
Ref 2: C/VM2 Verification Method: Framework for Fire Safety Design (July 2014)  
For New Zealand Building Code Clauses C1-6 Protection from Fire

Job No.	136249
Project Name:	HWCP Zone 1 Anchor
By:	ACC
Space:	Ground Floor Anchor

Ground floor only.

$$t_e = e_f k_b k_m w_f \text{ (minutes)}$$

where:

- $t_e$  = Time equivalence fire severity
- $e_f$  = Design fire load energy density
- $k_b$  = Thermal properties conversion factor
- $w_f$  = Ventilation factor
- $k_m$  = Modification factor for load-bearing structure material

Firecell lining materials = Normal weight concrete ceiling and floors  Fire cell width, W = 45 m Fire cell length, L = 78 m Fire cell height, H = 3.3 m Floor area, $A_f$ = 3510.0 m <sup>2</sup> Vertical openings, $A_v$ = 191.0 m <sup>2</sup> Horizontal openings, $A_h$ = 144.4 m <sup>2</sup>  Fire Load Energy Density = 800 MJ/m <sup>2</sup>  $F_m$ factor for FLED = Sprinklered: structural elements C/VM2 Table 2.2  <b>Burnout Rating for firecell, <math>t_e</math> = 43 minutes</b>	$k_b = 0.065$  $w_f = (6/H)^{0.3} \cdot (0.62 + 90 \cdot (0.4 + H \cdot 27)^{0.4} / (1 + (b_v \cdot H^{28})))$ Calculated $w_f = 1.60$ Use $w_f = 1.60$ Calculated $\alpha_v = A_v/A_f = 0.054$ Use $\alpha_v = A_v/A_f = 0.054$ $\alpha_h = A_h/A_f = 0.04$ $b_v = 19$ FLED = 822 MJ  $F_m = 0.50$ $e_f = 411 \text{ MJ}$	$w_f >= 0.50 \text{ (C/VM2)}$  $0.025 <= \alpha_v <= 0.25 \text{ (C/VM2)}$  $b_v >= 10$
Rating for structural material = Unprotected steel members  $A_v$ Height of Openings, $h_{eq} = 1.9$ m (relevant to unprotected steel, only) Time equivalence value, $t_e = 43$ minutes	$k_m = 1.00$ $A_v(h_{eq})0.5/At = 0.034$	$k_m >= 1 \text{ (C/VM2)}$ $0.02 <= t_e <= 0.20$

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Centre for Advanced Engineering, University of Canterbury, 2008. Ch. 6.4  
Ref 2: C/VM2 Verification Method: Framework for Fire Safety Design (July 2014)  
For New Zealand Building Code Clauses C1-6 Protection from Fire

Job No.	136249
Project Name:	HWCP Zone 1 Anchor
By:	ACC
Space:	L1 Anchor - Concrete roof

Level 1 only - with concrete roof.  
Note the roof to Level 1 is partial concrete and  
partial thin sheet steel.

$t_e = e_f k_b k_m w_f$  (minutes)  
where:

- $t_e$  = Time equivalence fire severity
- $e_f$  = Design fire load energy density
- $k_b$  = Thermal properties conversion factor
- $w_f$  = Ventilation factor
- $k_m$  = Modification factor for load-bearing structure material

Firecell lining materials = Normal weight concrete ceiling and floors  Fire cell width, W = 45 m Fire cell length, L = 74 m Fire cell height, H = 3.3 m Floor area, $A_f$ = 3330 m <sup>2</sup> Vertical openings, $A_v$ = 33.6 m <sup>2</sup> Horizontal openings, $A_h$ = m <sup>2</sup>  Fire Load Energy Density = 800 MJ/m <sup>2</sup>  $F_m$ factor for FLED = Sprinklered: structural elements C/VM2 Table 2.2  <b>Burnout Rating for firecell, <math>t_e</math> = 79 minutes</b>	$k_b = 0.065$  $w_f = (6/H)^{0.3} \cdot [0.62 + 90 \cdot (0.4 + H \cdot 27)^{0.4} / (1 + (b_v \cdot H^{28}))]$ Calculated $w_f = 2.87$ Use $w_f = 2.87$ Calculated $\alpha_v = A_v/A_f = 0.010$ Use $\alpha_v = A_v/A_f = 0.025$ $\alpha_h = A_h/A_f = 0.00$ $b_v = 16$ FLED = 847 MJ  $F_m = 0.50$ $e_f = 423.5$ MJ	$w_f >= 0.50$ (C/VM2)  $0.025 <= \alpha_v <= 0.25$ (C/VM2)  $b_v >= 10$
Rating for structural material = Unprotected steel members  $A_v$ Height of Openings, $h_{eq} = 2.3$ m (relevant to unprotected steel, only) Time equivalence value, $t_e = 79$ minutes	$k_m = 1.00$ $A_v(h_{eq})0.5/At = 0.007$	$k_m >= 1$ (C/VM2) $0.02 <= t_e <= 0.20$

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Ref 2: C/VM2 Verification Method: Framework for Fire Safety Design (July 2014)  
For New Zealand Building Code Clauses C1-6 Protection from Fire

Job No.	136249
Project Name:	HWCP Zone 1 Anchor
By:	ACC
Space:	L1 Anchor - thin sheet steel roof

Level 1 only - with thin sheet steel roof.  
Note the roof to Level 1 is partial concrete and  
partial thin sheet steel.

$t_e = e_f k_b k_m w_f$  (minutes)  
where:

- $t_e$  = Time equivalence fire severity
- $e_f$  = Design fire load energy density
- $k_b$  = Thermal properties conversion factor
- $w_f$  = Ventilation factor
- $k_m$  = Modification factor for load-bearing structure material

Firecell lining materials = Thin sheet steel roof and any wall system	$k_b = 0.04$	
Fire cell width, W = 45 m	$w_f = (6/H)^{0.3} \cdot (0.62 + 90 \cdot (0.4 + H \cdot 27)^{1/4} / (1 + (b_v \cdot H^{28})))$	
Fire cell length, L = 74 m	Calculated $w_f = 2.87$	$w_f >= 0.50$ (C/VM2)
Fire cell height, H = 3.3 m	Use $w_f = 2.87$	
Floor area, $A_f = 3330$ m <sup>2</sup>	Calculated $\alpha_v = A_v/A_f = 0.010$	
Vertical openings, $A_v = 33.62$ m <sup>2</sup>	Use $\alpha_v = A_v/A_f = 0.025$	$0.025 <= \alpha_v <= 0.25$ (C/VM2)
Horizontal openings, $A_h =$ m <sup>2</sup>	$\alpha_h = A_h/A_f = 0.00$	
Fire Load Energy Density = 800 MJ/m <sup>2</sup>	$b_v = 16$	$b_v >= 10$
$F_m$ factor for FLED = Sprinklered: structural elements	FLED = 847 MJ	
C/VM2 Table 2.2	$F_m = 0.50$	
<b>Burnout Rating for firecell, <math>t_e = 49</math> minutes</b>	$e_f = 423.5$ MJ	
Rating for structural material = Unprotected steel members	$k_m = 1.00$	$k_m >= 1$ (C/VM2)
$A_v$ Height of Openings, $h_{eq} = 2.3$ m (relevant to unprotected steel, only)	$Av(h_{eq})0.5/At = 0.007$	$0.02 <= t_e <= 0.20$
Time equivalence value, $t_e = 49$ minutes		

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Approved Burnout Calculation

BUILDING CONSENT NUMBER

2019/1381

Level 1 Anchor Space - Weighted FRR

Job No.	136249
Project Name:	HWCP Zone 1 Anchor
By:	ACC
Space:	L1 Anchor

Level 1 only - weighted FRR calculation for Level 1 anchor space to include both the concrete roof and thin sheet steel roof.

1L	Area (m2)	Weighting factors	FRR	weighted FRR
Concrete roof	1098	0.31	79.0	24.3
thin sheet steel roof	2473	0.69	49.0	33.9
Total	3571	1.00		58

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Building Division Fire Severity Calculation

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Centre for Advanced Engineering, University of Canterbury, 2008. Ch. 6.4  
Ref 2: C/VM2 Verification Method: Framework for Fire Safety Design (July 2014)  
For New Zealand Building Code Clauses C1-6 Protection from Fire

Job No.	136249
Project Name:	HWCP Zone 1 Anchor
By:	ACC
Space:	Zone 1 L2 Childcare Centre

$$t_e = e_f k_b k_m w_f \text{ (minutes)}$$

where:

- $t_e$  = Time equivalence fire severity
- $e_f$  = Design fire load energy density
- $k_b$  = Thermal properties conversion factor
- $w_f$  = Ventilation factor
- $k_m$  = Modification factor for load-bearing structure material

Firecell lining materials = <input type="text" value="Normal weight concrete ceiling and floors"/>	$k_b = 0.065$
Fire cell width, W = <input type="text" value=""/>	$w_f = (6/H)^{0.3} \cdot (0.62 + 90^{0.4} \cdot (0.4 + H \cdot 27)^{0.4} / (1 + (b_v \cdot H \cdot 28)))$
Fire cell length, L = <input type="text" value=""/>	Calculated $w_f = 1.44$
Fire cell height, H = <input type="text" value="3"/>	Use $w_f = 1.44$
Floor area, $A_f = 569 \text{ m}^2$	Calculated $\alpha_v = A_v/A_f = 0.121$
Vertical openings, $A_v = 68.58 \text{ m}^2$	Use $\alpha_v = A_v/A_f = 0.121$
Horizontal openings, $A_h = \text{m}^2$	$\alpha_h = A_h/A_f = 0.00$
Fire Load Energy Density = <input type="text" value="800 MJ/m2"/>	$b_v = 27$
$F_m$ factor for FLED = <input type="text" value="Sprinklered: structural elements"/>	FLED = 847 MJ
C/VM2 Table 2.2	$F_m = 0.50$
	$e_f = 423.5 \text{ MJ}$
<b>Burnout Rating for firecell, <math>t_e = 40</math> minutes</b>	$w_f >= 0.50 \text{ (C/VM2)}$
	$0.025 <= \alpha_v <= 0.25 \text{ (C/VM2)}$
	$b_v >= 10$

## Appendix B RSET Assessment

### B.1 Childcare Centre RSET time - Hand Calculation

RSET time for the Childcare centre has utilised hand calculation with a summary shown in Table 8 below and spreadsheet calculation shown in Section B.2.1 and B.2.2:

Table 8 - Childcare RSET Summary

CF	Smoke Detection Time, $t_d$ (s)	RSET (without $t_d$ ) (s)	RSET' (s)
CF1	41	742	783
CF2	25	742	767
CF3	29	682	711
RC1	44	742	786

Explanatory Notes:

- The RSET time is taken till the last person leaving the building.

#### B.1.1 RSET time for fire located within the Childcare centre

Zone 1 Level 2 Childcare  
Challenging Fire 3 - Fire located within the Childcare

RSET component	Inputs	Value
$t_d$	determined by B-Risk using C/VM2 input parameters (smoke activation)	29 s
$t_n$	As per C/VM2	30 s
$t_{pre}$	Pre-movement time (C/VM2 Table 3.3) for teachers	60 s
$t_{pre}$	Pre-movement time 60 seconds per staff per child (88 children + 12 staff) 88/12 = 8 trips to get children to buffer area 8 trips x 60 s each trip = 480 s	480 s
$t_{trav}$	= distance / walking speed (= distance/S) distance (assumed) = 35.4 m S = 0.7 m/s	51
$t_{flow}$	= distance / walking speed (= distance/S) distance = 30.5 m S = 0.5 m/s	61
$t_{move}$	= the combination of $t_{flow}$ and $t_{trav}$	tflow 112 s
<b>RSET</b>	= ( $t_d + t_n + t_{pre}$ ) + $t_{move}$	<b>RSET = 711 s</b>

Total time to Buffer Area = 600 s

#### B.1.2 RSET time for fire remote from Childcare centre

The RSET time for a fire remote from the Childcare centre did not include the detection time.



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Zone 1 Level 2 Childcare  
RSET for fire remote from the Childcare Centre

RSET component	Inputs	Value
$t_d$	determined by B-Risk using C/VM2 input parameters (smoke activation)	s
$t_n$	As per C/VM2	30 s
$t_{pre}$	Pre-movement time (C/VM2 Table 3.3) for teachers	120 s
$t_{pre}$	Pre-movement time 60 seconds per staff per child (88 children + 12 staff) 88/12 = 8 trips to get children to buffer area 8 trips x 60 s each trip = 480 s	480 s
$t_{trav}$	= distance / walking speed (= distance/S) distance (assumed) = 35.4 m S = 0.7 m/s	51
$t_{flow}$	= distance / walking speed (= distance/S) distance = 30.5 m S = 0.5 m/s	61
$t_{move}$	= the combination of $t_{flow}$ and $t_{trav}$	tflow 112 s
<b>RSET</b>	= ( $t_d + t_n + t_{pre}$ ) + $t_{move}$	<b>RSET = 742 s</b>

Total time to Buffer Area = 600 s

## B.2 EvacuationNZ Model Input Data

A total of two egress scenarios are assessed, a base case and the non-base case as per agreed in the Zone 1 FEB for Challenging Fire 1 and 2. Refer to the master FEB for the sketches indicating the proposed egress distributions.

The following table summarises input data utilised for the RSET calculation within the EvacuationNZ model for ground floor and first floor Anchor.

Table 9 - EvacuationNZ Input Data

Input	Comment
Occupant Loads	<p>For the base case egress model, we have limited the model to:</p> <ul style="list-style-type: none"> <li>• Ground Floor Anchor.</li> <li>• First Floor Anchor.</li> </ul> <p>For the non-base case egress model, we have included the following areas:</p> <ul style="list-style-type: none"> <li>• Ground Floor Anchor.</li> <li>• First Floor Anchor.</li> <li>• Zone 3 Carpark building L1 – L4 – utilising Zone 3 FEV occupant load.</li> <li>• Zone 3 Carpark building L5 with an occupant load of 999 people.</li> <li>• Zone 2 Mall Ground Floor – utilising Master FEB occupant load.</li> </ul> <p>Note the Zone 2 mall numbers may need to be refined at a later stage. If occupant load increased significantly in the future stage, we will re-address the assessment to incorporate the additional occupant load.</p>
Egress Routes	As agreed in Master FEB.
Detection Time	<p>Detection time is not included in EvacuationNZ modelling results.</p> <p>For all Challenging Fires, smoke detector activation time is utilised for detection time (Time derived from FDS and B-Risk Results).</p>
Notification Time	<p>Notification time of 30 seconds is utilised as agreed in Master FEB.</p> <p>This is included in EvacuationNZ modelling.</p>
Pre-Movement Time	<p>Pre-movement times, as agreed in the Master FEB, on basis of voice alarm:</p> <ul style="list-style-type: none"> <li>• 30 seconds, if within enclosure of fire origin.</li> <li>• 60 seconds, if remote from enclosure of fire origin.</li> </ul>
Modelled Areas/Nodes	<p>The actual floor areas have not been modelled in EvacuationNZ., it is expected that queuing time will govern due to the number of occupants. Therefore, floor area (thus travel time) will not be a dominant factor.</p> <p>Hand calculation was carried out to verify that travel distance is not the governing factor on both ground floor and first floor but rather the queuing time. Therefore, the actual floor areas have not been modelled in EvacuationNZ.</p> <p>Refer to attached EvacuationNZ diagram for detailed model information with hand calculation validation shown in Appendix B.5.</p>
Egress Widths	EvacuationNZ makes deduction to the input clear widths to account for the boundary layer relative to a single opening.

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Input	Comment
Distribution Weighting	As agreed in Master FEB.

**B.3 RSET for base case**

The following figure represents clearance times from each level for Base case for Challenging Fire 1, 2, 3 and RC1 utilising EvacuatioNZ model.

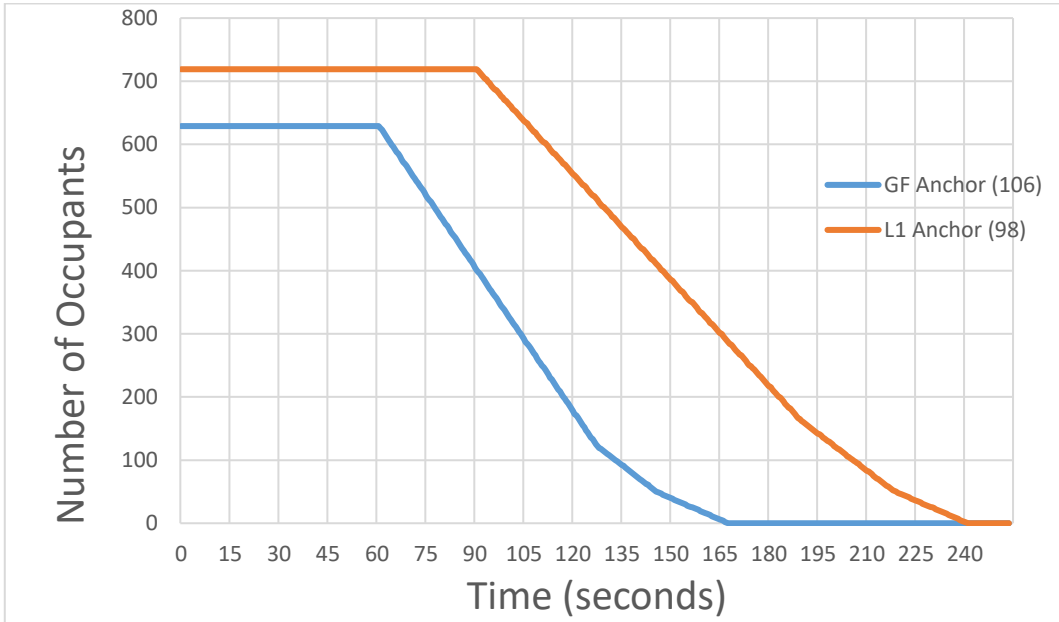


Figure 1 - EvacuatioNZ Node Clearance Times in anchor space for Base case CF1, CF2 and RC1.

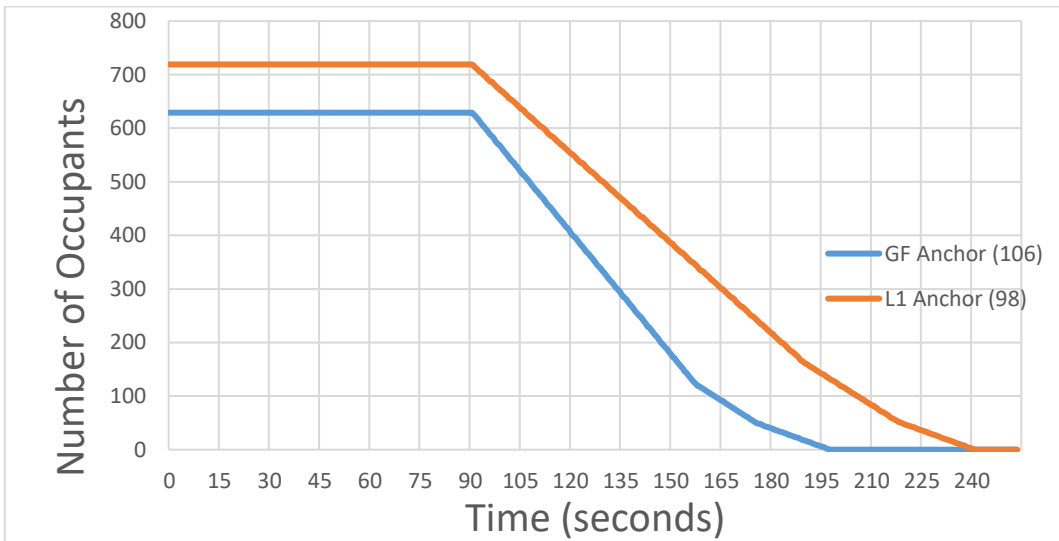


Figure 2 - EvacuatioNZ Node Clearance Times in anchor space for Base case CF3.

The following table summarises clearance times for various nodes:

Table 10 - Clearance Time for Base case.

Location <sup>1</sup>	Clearance Time <sup>2,3</sup> (excl. detection time) (s)	
	CF1, CF2 & RC1 <sup>2</sup>	CF3 <sup>3</sup>
GF Anchor	168	198
L1 Anchor	241	241
L1 Stair 3 Landing <sup>4</sup>	237	237
L1 Anchor-S BoH <sup>5</sup>	194	194
L0 Stair 3 Landing <sup>6</sup>	254	254
L0 Stair 4 landing <sup>7</sup>	226	226

Explanatory Notes:

- 1) Location is the space represented as nodes in EvacuationNZ.
- 2) The Clearance Time for Challenging Fire Scenarios CF1, CF2 and Robustness Check Scenario RC1 includes notification time of 30 sec and pre-movement time of 30 sec for ground floor anchor space and 60 sec for first floor anchor space.
- 3) The Clearance Time for Challenging Fire Scenario CF3 includes notification time of 30 sec and pre-movement time of 60 sec for ground floor and first floor anchor space.
- 4) 'L1 Stair 3 Landing' is the node that corresponds to the lobby space before entering into Stair 3 which indicates the queuing clear time preceding stair 3.
- 5) 'L1 Anchor-S BoH' is the node that corresponds to the lobby space before entering into Stair 4 which indicate the queuing clear time preceding stair 4.
- 6) 'L0 Stair3 Landing' is the node that corresponds to the space precede the final exit from Stair 3 (L1 Anchor north stairwell) which is shared by the occupants from L2 Childcare space.
- 7) 'L0 Stair4 Landing' is the node that corresponds to the space precede the final exit from Stair 4 (i.e. time to clear L1 Anchor south stairwell).

The following table summarises the RSET for various nodes:

Table 11 - RSET time for Base case.

CF	Location	Smoke Detection Time <sup>1</sup> (s)	RSET <sup>2</sup> (s)
CF1	GF Anchor	41	209
	L1 Anchor		282
	L1 Stair 3 Landing <sup>3</sup>		278
	L1 Anchor-S BoH <sup>4</sup>		235
	L0 Stair 3 Landing <sup>5</sup>		295
	L0 Stair 4 landing <sup>6</sup>		267
CF2	GF Anchor	25	193

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CF	Location	Smoke Detection Time <sup>1</sup> (s)	RSET <sup>2</sup> (s)
	L1 Anchor		266
	L1 Stair 3 Landing <sup>3</sup>		262
	L1 Anchor-S BoH <sup>4</sup>		219
	L0 Stair 3 Landing <sup>5</sup>		279
	L0 Stair 4 landing <sup>6</sup>		251
CF3	GF Anchor	29	227
	L1 Anchor		270
	L1 Stair 3 Landing <sup>3</sup>		266
	L1 Anchor-S BoH <sup>4</sup>		223
	L0 Stair 3 Landing <sup>5</sup>		283
	L0 Stair 4 landing <sup>6</sup>		255
RC1	GF Anchor	44	212
	L1 Anchor		285
	L1 Stair 3 Landing <sup>3</sup>		281
	L1 Anchor-S BoH <sup>4</sup>		238
	L0 Stair 3 Landing <sup>5</sup>		298
	L0 Stair 4 landing <sup>6</sup>		270

Explanatory notes:

- 1) Refer to Appendix C for a summary of the FDS results and smoke activation time.
- 2) RSET is calculated by the sum of 'Clearance Time' plus 'Smoke Detection Time.
- 3) 'L1 Stair 3 Landing' is the node that corresponds to the lobby space before entering into Stair 3 which indicates the queuing clear time preceding stair 3.
- 4) 'L1 Anchor-S BoH' is the node that corresponds to the lobby space before entering into Stair 4 which indicate the queuing clear time preceding stair 4.
- 5) 'L0 Stair3 Landing' is the node that corresponds to the space precede the final exit from Stair 3 (L1 Anchor north stairwell) which is shared by the occupants from L2 Childcare space.
- 6) 'L0 Stair4 Landing' is the node that corresponds to the space precede the final exit from Stair 4 (i.e. time to clear L1 Anchor south stairwell).

### B.3.1 Childcare centre Evacuation - Base Case

Stair 3 from the anchor space is the designated share egress for both Level 1 Anchor space and L2 Childcare centre. As can be seen above in Table 11, the time taken for the L1 Anchor occupant to egress via stair 3 for all three challenging fires are less than 300 seconds while the pre-movement time for the childcare building is 600 seconds for a fire within the Childcare centre and 660 seconds for a fire remote

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from the Childcare centre. Therefore, the egress time from the Childcare centre can be considered as isolated from the remainder of the building.

Attached is the following:

- EvacNZ model Setup FSK Z1 B.3.01
- Base case EvacuatioNZ Setup.
- Base case EvacuatioNZ Output file.

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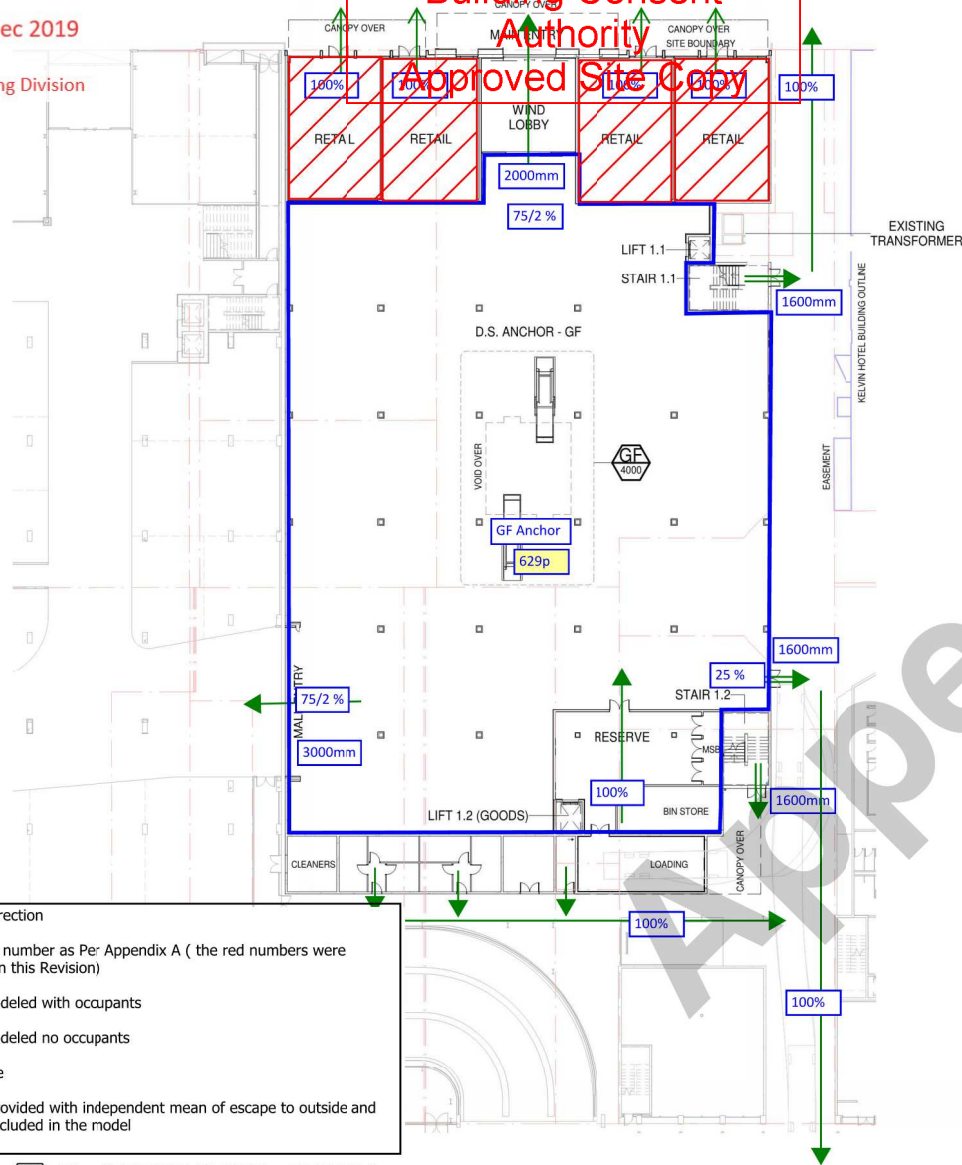
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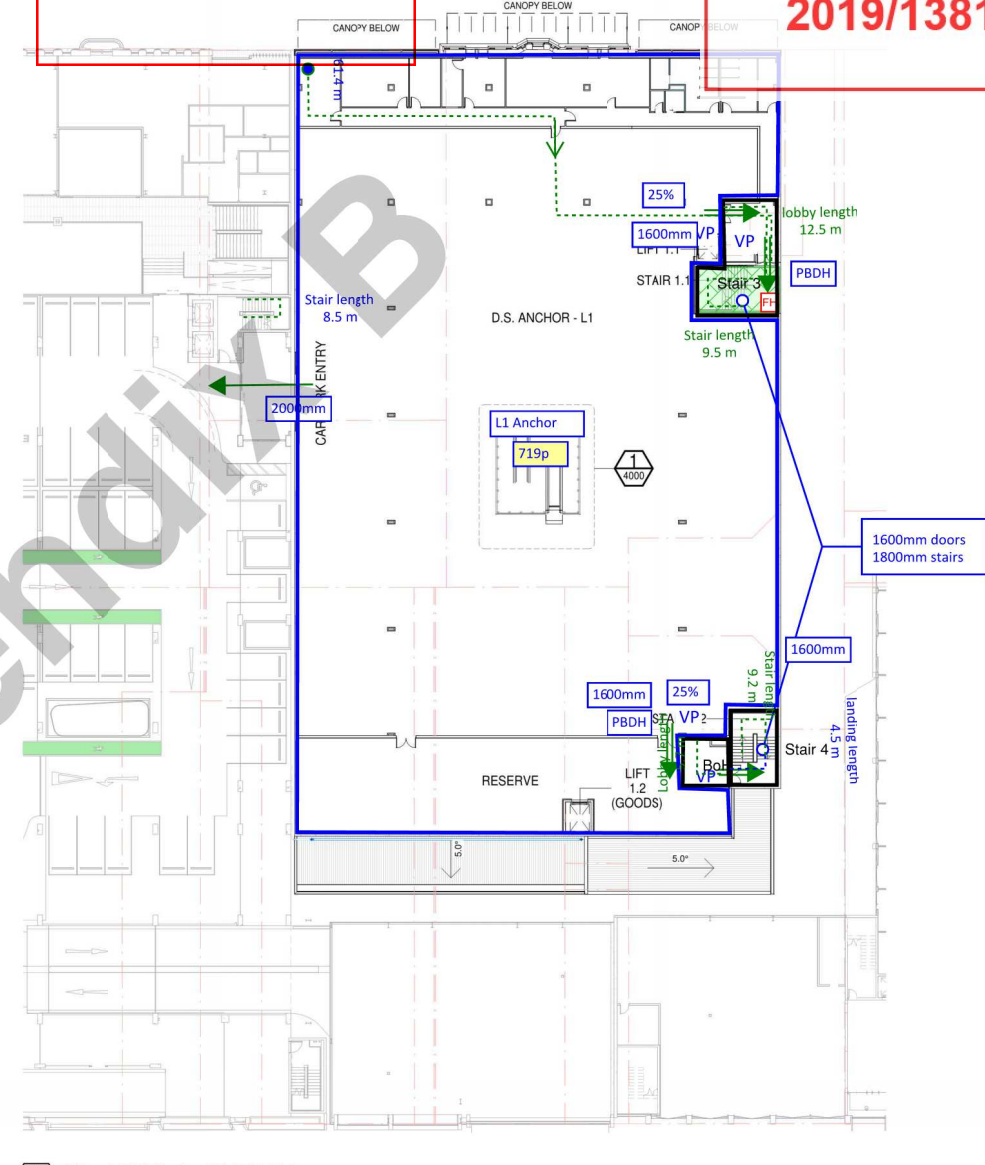
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**GF** Z1 - GROUND FLOOR - OVERALL  
1:250



**1** Z1 - LEVEL 1 - OVERALL  
1:250

→ Egress Direction

**11p** Occupant number as Per Appendix A ( the red numbers were updated in this Revision)

  Space modeled with occupants

  Space modeled no occupants

  Safe Place

  Spaces provided with independent mean of escape to outside and are not included in the model

This sketch does not constitute a complete fire engineering design or detail. Detailed construction drawings are provided by others. Best viewed in colour. Not all fire separations around ducts and shafts are shown.

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Project Title	Sketch Title	Drawn: ACC	Date: 30 / 07 / 2019
HWCP - Invercargill Central	Zone 1 GF & L1 Travel Distance Measurement	Project No.	Sheet No.
		136249	FSK Z1 B.3.01
		Rev	A

Rev.	Date	Description	Iss. Appr.	Keyplan
A	27.11.18	FOR COMMENT	BH JB	
B	19.03.19	PRELIMINARY DESIGN	BH JB	
C	21.03.19	PRELIMINARY DESIGN	BH DA	
D	17.04.19	FOR INFORMATION	JT DA	

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File: C:\BIB - Revit Projects\917077 - AR-PD - INVERCARGILL - ZONE 1 - ANCHOR - 2019\_Jessica Tuboheer.buchanan.rvt

**HWCP**

Project  
**INVERCARGILL CENTRAL - ZONE 1**  
TAY STREET & DEE STREET CORNER  
INVERCARGILL

Project Number  
917077

Status  
PRELIMINARY DESIGN

Date Issued  
17/04/2019 14:42:26 PM

Date Issued  
21.03.19

Scale  
1:250 @A1

Drawing Title  
**ZONE 1  
OVERALL FLOOR PLANS**

Drawing Number  
**Z1-PD-A-1100**

**BUCHAN**

Christchurch Studio  
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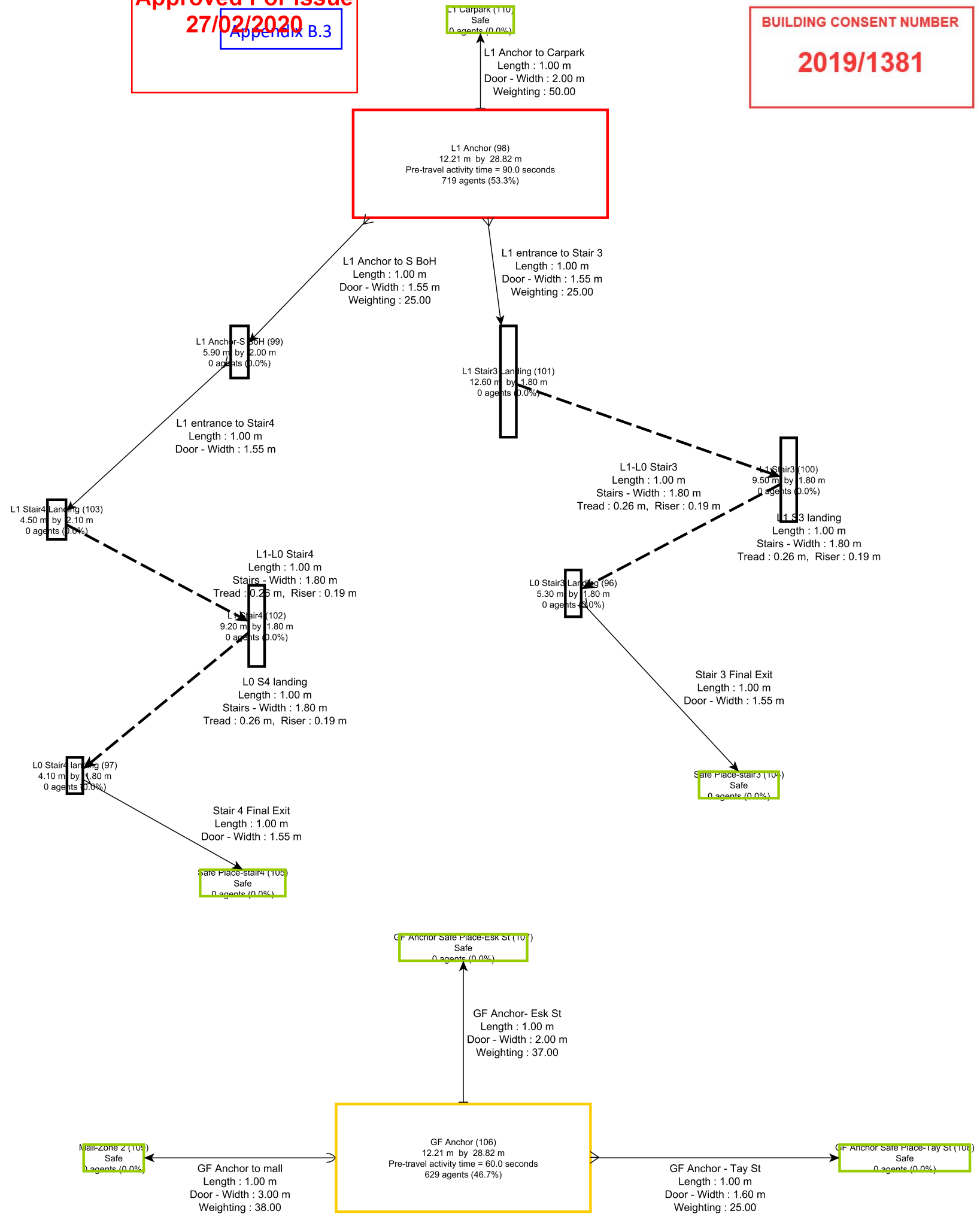
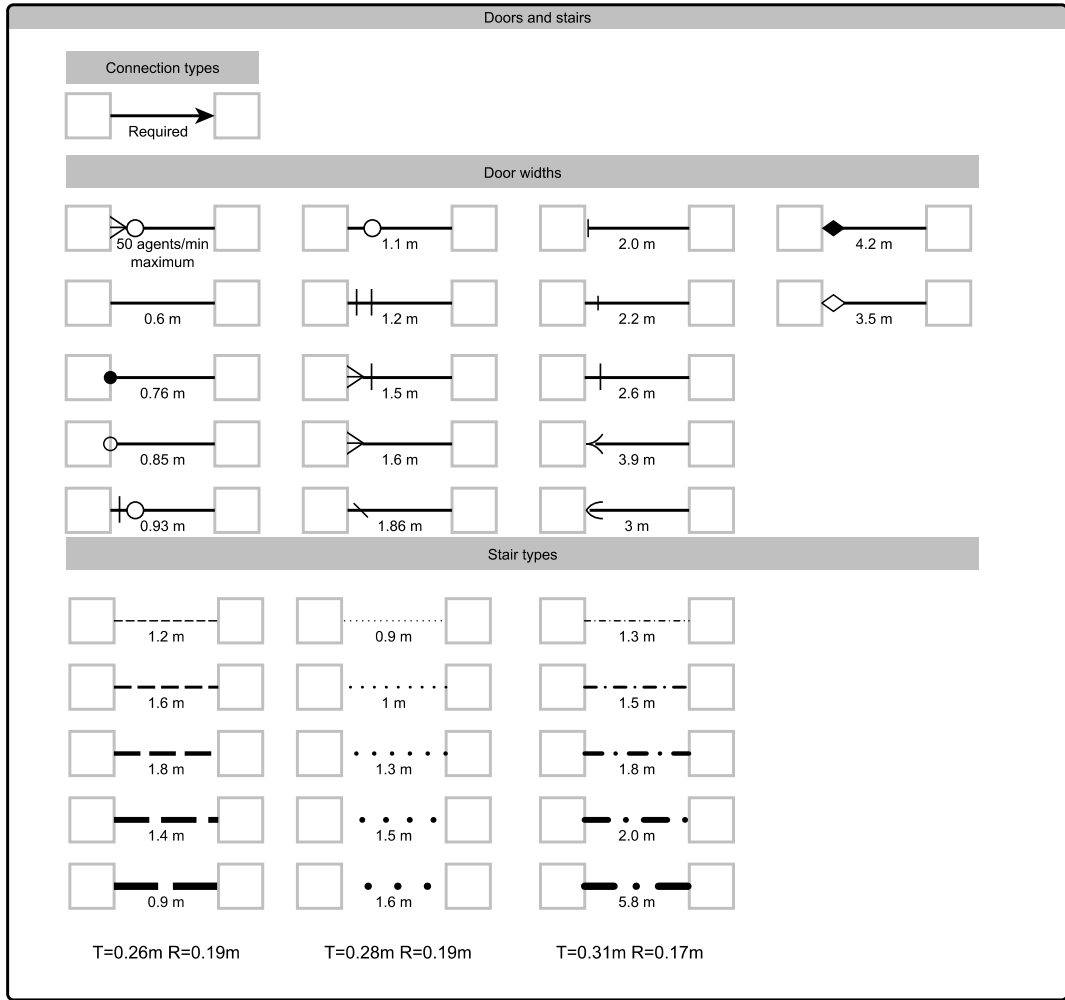
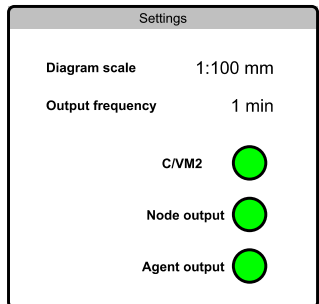
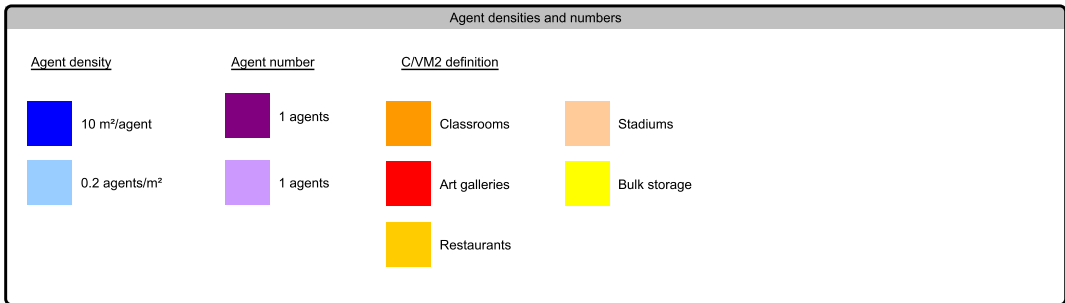
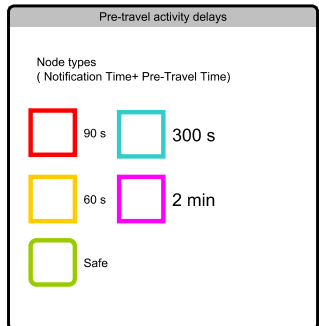
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Evacuation model for:  
Base Case  
- Challenging Fire 1 (CF1)  
- Challenging Fire 2 (CF2)  
- Robustness Check (RC1)

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## EvacuationZ

Michael Spearpoint  
University of Canterbury  
version 2.11 - Holmes Fire release (Sep 19 2016)

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### Contents

[Nodes](#)  
[Connections](#)  
[Population](#)  
[Results](#)

### Nodes

Node **L1 Carpark** - Safe  
Connections : [L1 Anchor to Carpark](#),

Node **Mall-Zone 2** - Safe  
Connections : [GF Anchor to mall](#),

Node **GF Anchor Safe Place-Tay St** - Safe  
Connections : [GF Anchor - Tay St](#),

Node **GF Anchor Safe Place-Esk St** - Safe  
Connections : [GF Anchor- Esk St](#),

Node **GF Anchor**  
Dimensions 12.21 m by 28.82 m  
Connections : [GF Anchor to mall](#), [GF Anchor - Tay St](#), [GF Anchor- Esk St](#),

Node **Safe Place-stair4** - Safe  
Connections : [Stair 4 Final Exit](#),

Node **Safe Place-stair3** - Safe  
Connections : [Stair 3 Final Exit](#),

Node **L1 Stair4 Landing**  
Dimensions 4.50 m by 2.10 m  
Connections : [L1-L0 Stair4](#), [L1 entrance to Stair4](#),

Node **L1 Stair4**  
Dimensions 9.20 m by 1.80 m  
Connections : [L0 S4 landing](#), [L1-L0 Stair4](#),

Node **L1 Stair3 Landing**

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EvacuationZ model for:  
Base Case  
- Challenging Fire 1 (CF1)  
- Challenging Fire 2 (CF2)  
- Robustness Check (RC1)

Dimensions 12.60 m by 1.80 m  
Connections : [L1 entrance to Stair3](#), [L1-L0 Stair3](#),

Node **L1 Stair3**  
Dimensions 9.50 m by 1.80 m  
Connections : [L1 S3 landing](#), [L1-L0 Stair3](#),

Node **L1 Anchor-S BoH**  
Dimensions 5.90 m by 2.00 m  
Connections : [L1 Anchor to S BoH](#), [L1 entrance to Stair4](#),

Node **L1 Anchor**  
Dimensions 12.21 m by 28.82 m  
Connections : [L1 entrance to Stair 3](#), [L1 Anchor to S BoH](#), [L1 Anchor to Carpark](#),

Node **L0 Stair4 landing**  
Dimensions 4.10 m by 1.80 m  
Connections : [Stair 4 Final Exit](#), [L0 S4 landing](#),

Node **L0 Stair3 Landing**  
Dimensions 5.30 m by 1.80 m  
Connections : [Stair 3 Final Exit](#), [L1 S3 landing](#),

### Connections

Connection **L1-L0 Stair3**  
Length 1.00 m  
Connecting [L1 Stair3 Landing](#) to [L1 Stair3](#) (target node for required path)  
Stairs width 1.80 m, tread 0.26 m, riser 0.19 m

Connection **L1 S3 landing**  
Length 1.00 m  
Connecting [L1 Stair3](#) to [L0 Stair3 Landing](#) (target node for required path)  
Stairs width 1.80 m, tread 0.26 m, riser 0.19 m

Connection **L1 entrance to Stair4**  
Length 1.00 m  
Connecting [L1 Anchor-S BoH](#) to [L1 Stair4 Landing](#) (target node for required path)  
Door width 1.55 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)

Connection **L1-L0 Stair4**  
Length 1.00 m  
Connecting [L1 Stair4 Landing](#) to [L1 Stair4](#) (target node for required path)  
Stairs width 1.80 m, tread 0.26 m, riser 0.19 m

Connection **L0 S4 landing**  
Length 1.00 m  
Connecting [L1 Stair4](#) to [L0 Stair4 landing](#) (target node for required path)  
Stairs width 1.80 m, tread 0.26 m, riser 0.19 m

Connection **Stair 4 Final Exit**  
Length 1.00 m  
Connecting [L0 Stair4 landing](#) to [Safe Place-stair4](#) (target node for required path)  
Door width 1.55 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)

Connection **Stair 3 Final Exit**  
Length 1.00 m

EvacuationNZ model for:  
 Base Case  
 - Challenging Fire 1 (CF1)  
 - Challenging Fire 2 (CF2)  
 - Robustness Check (RC1)

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 Time for last occupant to enter into stair 4 (i.e. no queuing in front of stair 4)

Connecting [L0 Stair3 Landing](#) to [Safe Place-stair3](#) (target node for required path)  
 Length 1.00 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)  
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**Connection L1 Anchor to Carpark**

Length 1.00 m  
 Connecting [L1 Anchor](#) to [L1 Carpark](#) (target node for required path)  
 Door width 2.00 m, specific flow 1.33 persons/s per m eff. width

**Connection L1 Anchor to S BoH**

Length 1.00 m  
 Connecting [L1 Anchor](#) to [L1 Anchor-S BoH](#) (target node for required path)  
 Door width 1.55 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)

**Connection L1 entrance to Stair 3**

Length 1.00 m  
 Connecting [L1 Anchor](#) to [L1 Stair3 Landing](#) (target node for required path)  
 Door width 1.55 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)

**Connection GF Anchor- Esk St**

Length 1.00 m  
 Connecting [GF Anchor](#) to [GF Anchor Safe Place-Esk St](#) (target node for required path)  
 Door width 2.00 m, specific flow 1.33 persons/s per m eff. width

**Connection GF Anchor - Tay St**

Length 1.00 m  
 Connecting [GF Anchor](#) to [GF Anchor Safe Place-Tay St](#) (target node for required path)  
 Door width 1.60 m, specific flow 1.33 persons/s per m eff. width

**Connection GF Anchor to mall**

Length 1.00 m  
 Connecting [GF Anchor](#) to [Mall-Zone 2](#) (target node for required path)  
 Door width 3.00 m, specific flow 1.33 persons/s per m eff. width

**Population**

Name	Number	Density (agents/m <sup>2</sup> )	Density (m <sup>2</sup> /agent)
<a href="#">L1 Anchor</a>	719	2.04	0.49
<a href="#">GF Anchor</a>	629	1.79	0.56

**Results**

Simulation run 1 : Total number of agents = 1348

Node [GF Anchor](#) clear at 167.5 s

Node [L1 Anchor](#) clear at 241.0 s

Last agent to leave node [GF Anchor](#) was 'Agent #720' at 167.5 s

Last agent to leave node [L1 Stair4 Landing](#) was 'Agent #12' at 210.5 s

Last agent to leave node [L1 Stair4](#) was 'Agent #12' at 220.0 s

Last agent to leave node [L1 Stair3 Landing](#) was 'Agent #1' at 236.5 s

Last agent to leave node [L1 Stair3](#) was 'Agent #1' at 248.5 s

Time to clear GF Anchor space

Time for last occupant to enter into stair 3 (i.e. no queuing in front of stair 3)

Last agent to leave node [L1 Anchor-S BoH](#) was 'Agent #7' at 193.5 s  
 Last agent to leave node [L1 Anchor](#) was 'Agent #2' at 241.0 s  
 Last agent to leave node [L0 Stair4 landing](#) was 'Agent #12' at 220.0 s  
 Last agent to leave node [L0 Stair3 Landing](#) was 'Agent #1' at 253.5 s

Total number of agents in safe node [L1 Carpark](#) = 340  
 Total number of agents in safe node [Mall-Zone 2](#) = 240  
 Total number of agents in safe node [GF Anchor Safe Place-Tay St](#) = 147  
 Total number of agents in safe node [GF Anchor Safe Place-Esk St](#) = 242  
 Total number of agents in safe node [Safe Place-stair4](#) = 166  
 Total number of agents in safe node [Safe Place-stair3](#) = 213

Total evacuation time = 253.50 s

Completed at 13:59:41 on Tuesday 27 August

Time for last person from Level 1 Anchor to leave stair 3. This stair is the designated egress stairwell for the Childcare Centre on Level 2.

Time to clear L1 Anchor space (last person to enter into L1 carpark)

Time for last person from Level 1 Anchor to leave stair 4.

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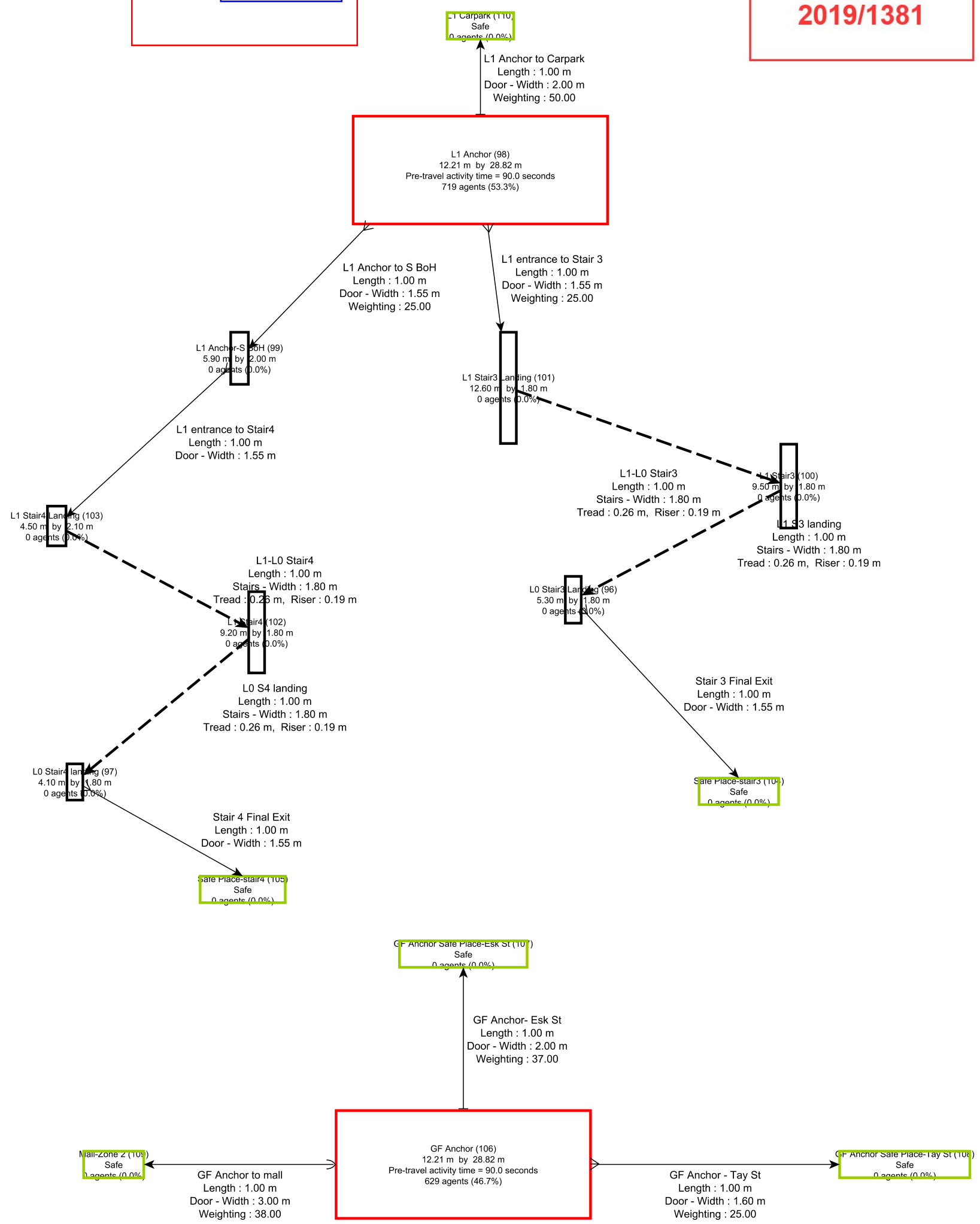
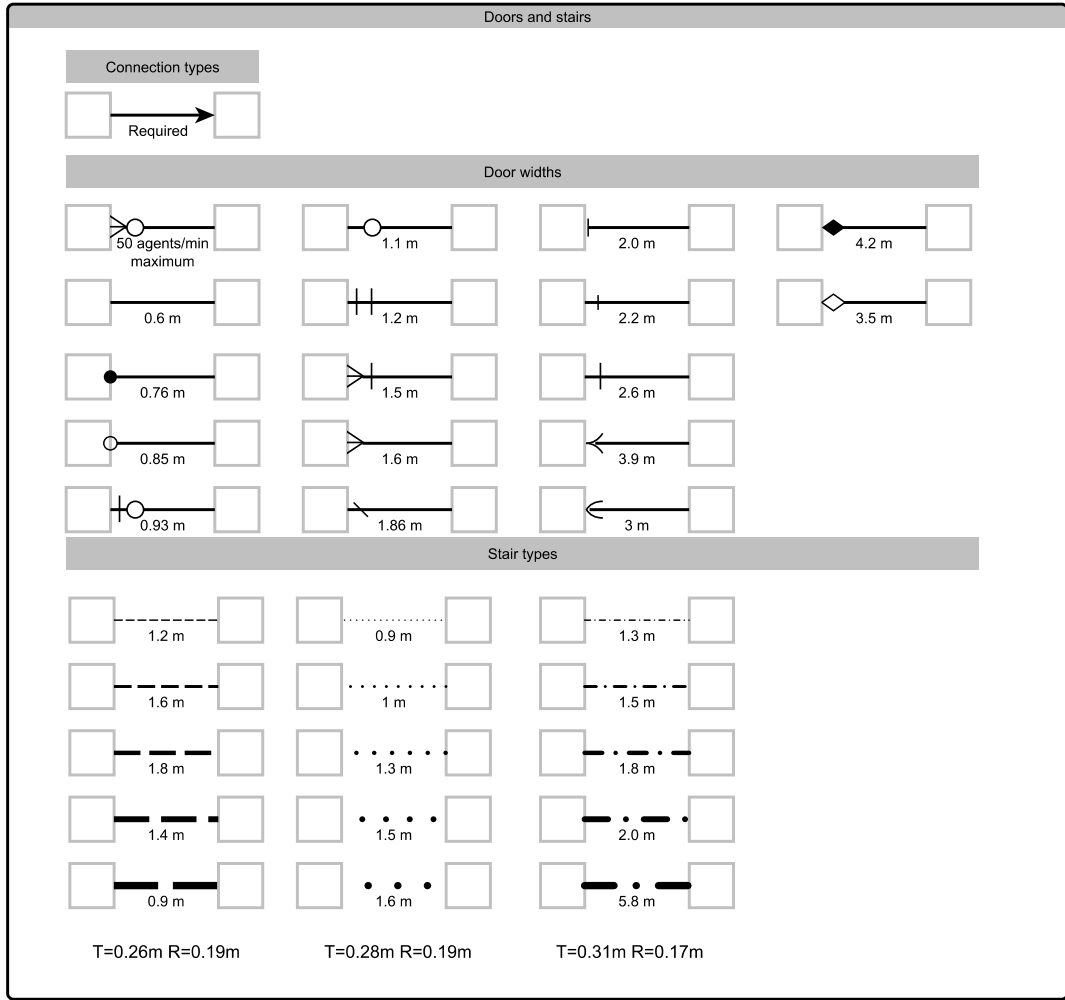
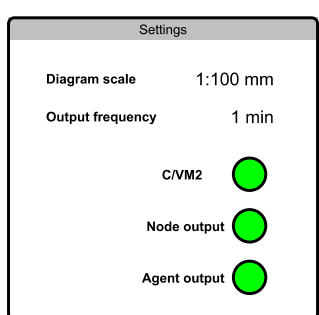
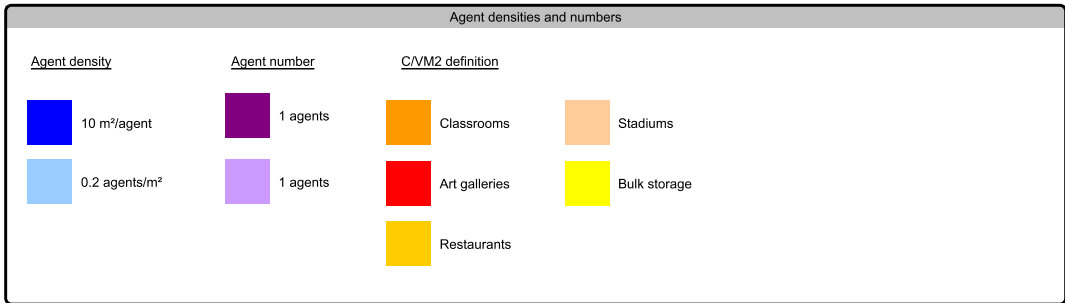
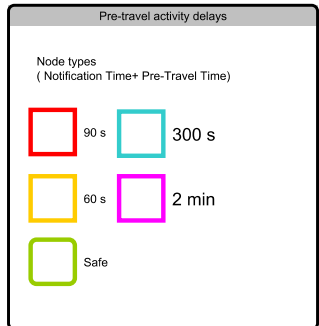
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EvacuationN2 model for:  
Base Case - Challenging Fire 3 (CF3) Childcare Fire  
Pre-movement time for GF and L1 anchor stairs = 90 sec

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## EvacuationNZ

Michael Spearpoint  
University of Canterbury  
version 2.11 - Holmes Fire release (Sep 19 2016)

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### Nodes

Node **L1 Carpark** - Safe

Connections : [L1 Anchor to Carpark](#),

Node **Mall-Zone 2** - Safe

Connections : [GF Anchor to mall](#),

Node **GF Anchor Safe Place-Tay St** - Safe

Connections : [GF Anchor - Tay St](#),

Node **GF Anchor Safe Place-Esk St** - Safe

Connections : [GF Anchor- Esk St](#),

Node **GF Anchor**

Dimensions 12.21 m by 28.82 m

Connections : [GF Anchor to mall](#), [GF Anchor - Tay St](#), [GF Anchor- Esk St](#),

Node **Safe Place-stair4** - Safe

Connections : [Stair 4 Final Exit](#),

Node **Safe Place-stair3** - Safe

Connections : [Stair 3 Final Exit](#),

Node **L1 Stair4 Landing**

Dimensions 4.50 m by 2.10 m

Connections : [L1-L0 Stair4](#), [L1 entrance to Stair4](#),

Node **L1 Stair4**

Dimensions 9.20 m by 1.80 m

Connections : [L0 S4 landing](#), [L1-L0 Stair4](#),

Node **L1 Stair3 Landing**

EvacuationNZ model for:

Base case

Challenging Fire 3 (CF3) Childcare Fire

Fire-movement time for GF and 1L

Anchor space = 60 sec

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Dimensions 12.60 m by 1.80 m

Connections : [L1 entrance to Stair3](#), [L1-L0 Stair3](#),

Node **L1 Stair3**

Dimensions 9.50 m by 1.80 m

Connections : [L1 S3 landing](#), [L1-L0 Stair3](#),

Node **L1 Anchor-S BoH**

Dimensions 5.90 m by 2.00 m

Connections : [L1 Anchor to S BoH](#), [L1 entrance to Stair4](#),

Node **L1 Anchor**

Dimensions 12.21 m by 28.82 m

Connections : [L1 entrance to Stair 3](#), [L1 Anchor to S BoH](#), [L1 Anchor to Carpark](#),

Node **L0 Stair4 landing**

Dimensions 4.10 m by 1.80 m

Connections : [Stair 4 Final Exit](#), [L0 S4 landing](#),

Node **L0 Stair3 Landing**

Dimensions 5.30 m by 1.80 m

Connections : [Stair 3 Final Exit](#), [L1 S3 landing](#),

### Connections

Connection **L1-L0 Stair3**

Length 1.00 m

Connecting [L1 Stair3 Landing](#) to [L1 Stair3](#) (target node for required path)

Stairs width 1.80 m, tread 0.26 m, riser 0.19 m

Connection **L1 S3 landing**

Length 1.00 m

Connecting [L1 Stair3](#) to [L0 Stair3 Landing](#) (target node for required path)

Stairs width 1.80 m, tread 0.26 m, riser 0.19 m

Connection **L1 entrance to Stair4**

Length 1.00 m

Connecting [L1 Anchor-S BoH](#) to [L1 Stair4 Landing](#) (target node for required path)

Door width 1.55 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)

Connection **L1-L0 Stair4**

Length 1.00 m

Connecting [L1 Stair4 Landing](#) to [L1 Stair4](#) (target node for required path)

Stairs width 1.80 m, tread 0.26 m, riser 0.19 m

Connection **L0 S4 landing**

Length 1.00 m

Connecting [L1 Stair4](#) to [L0 Stair4 landing](#) (target node for required path)

Stairs width 1.80 m, tread 0.26 m, riser 0.19 m

Connection **Stair 4 Final Exit**

Length 1.00 m

Connecting [L0 Stair4 landing](#) to [Safe Place-stair4](#) (target node for required path)

Door width 1.55 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)

Connection **Stair 3 Final Exit**

Length 1.00 m

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Appendix B.3

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EvacuationNZ model for:  
 Base Case  
 - Challenging Fire 3 (CF3)  
 Childcare Fire  
 Pre-movement time for  
 GF and 1L anchor space  
 = 60 sec

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 Time for last occupant to enter into stair 4 (i.e. no queuing in front of stair 4)

Connecting [L0 Stair3 Landing](#) to [Safe Place-stair3](#) (target node for required path)  
 Length 1.00 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)  
**17-Dec-2019** 55 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)

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**L1 Anchor to Carpark**

Length 1.00 m  
 Connecting [L1 Anchor](#) to [L1 Carpark](#) (target node for required path)  
 Door width 2.00 m, specific flow 1.33 persons/s per m eff. width

**Connection L1 Anchor to S BoH**

Length 1.00 m  
 Connecting [L1 Anchor](#) to [L1 Anchor-S BoH](#) (target node for required path)  
 Door width 1.55 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)

**Connection L1 entrance to Stair 3**

Length 1.00 m  
 Connecting [L1 Anchor](#) to [L1 Stair3 Landing](#) (target node for required path)  
 Door width 1.55 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)

**Connection GF Anchor- Esk St**

Length 1.00 m  
 Connecting [GF Anchor](#) to [GF Anchor Safe Place-Esk St](#) (target node for required path)  
 Door width 2.00 m, specific flow 1.33 persons/s per m eff. width

**Connection GF Anchor - Tay St**

Length 1.00 m  
 Connecting [GF Anchor](#) to [GF Anchor Safe Place-Tay St](#) (target node for required path)  
 Door width 1.60 m, specific flow 1.33 persons/s per m eff. width

**Connection GF Anchor to mall**

Length 1.00 m  
 Connecting [GF Anchor](#) to [Mall-Zone 2](#) (target node for required path)  
 Door width 3.00 m, specific flow 1.33 persons/s per m eff. width

**Population**

Name	Number	Density (agents/m <sup>2</sup> )	Density (m <sup>2</sup> /agent)
<a href="#">L1 Anchor</a>	719	2.04	0.49
<a href="#">GF Anchor</a>	629	1.79	0.56

**Results**

Simulation run 1 : Total number of agents = 1348

Node [GF Anchor](#) clear at 197.5 s

Node [L1 Anchor](#) clear at 241.0 s

Last agent to leave node [GF Anchor](#) was 'Agent #720' at 197.5 s  
 Last agent to leave node [L1 Stair4 Landing](#) was 'Agent #12' at 210.5 s  
 Last agent to leave node [L1 Stair4](#) was 'Agent #12' at 220.0 s  
 Last agent to leave node [L1 Stair3 Landing](#) was 'Agent #1' at 236.5 s  
 Last agent to leave node [L1 Stair3](#) was 'Agent #1' at 248.5 s

Time to clear GF Anchor space

Time for last occupant to enter into stair 3 (i.e. no queuing in front of stair 3)

Last agent to leave node [L1 Anchor-S BoH](#) was 'Agent #7' at 193.5 s  
 Last agent to leave node [L1 Anchor](#) was 'Agent #2' at 241.0 s  
 Last agent to leave node [L0 Stair4 landing](#) was 'Agent #12' at 220.5 s  
 Last agent to leave node [L0 Stair3 Landing](#) was 'Agent #1' at 253.0 s

Total number of agents in safe node [L1 Carpark](#) = 340  
 Total number of agents in safe node [Mall-Zone 2](#) = 240  
 Total number of agents in safe node [GF Anchor Safe Place-Tay St](#) = 147  
 Total number of agents in safe node [GF Anchor Safe Place-Esk St](#) = 242  
 Total number of agents in safe node [Safe Place-stair4](#) = 166  
 Total number of agents in safe node [Safe Place-stair3](#) = 213

Total evacuation time = 253.50 s

Completed at 14:47:19 on Tuesday 27 August

Time for last person from Level 1 Anchor to leave stair 3. This stair is the designated egress stairwell for the Childcare Centre on Level 2.

Time to clear L1 Anchor space (last person to enter into L1 carpark)

Time for last person from Level 1 Anchor to leave stair 4.

**B.4 RSET for non-base case**

The RSET time for Non-Base case is shown below. The non-base case egress model includes the following areas:

- Zone 2 ground floor and level one mall area, and
- Zone 3 Carpark area (utilizing the non-base case scenario where a crowd activity occurs on L5 of the carpark).

The following figure represents clearance times taken from EvacuatioNZ model for Non-Base case.

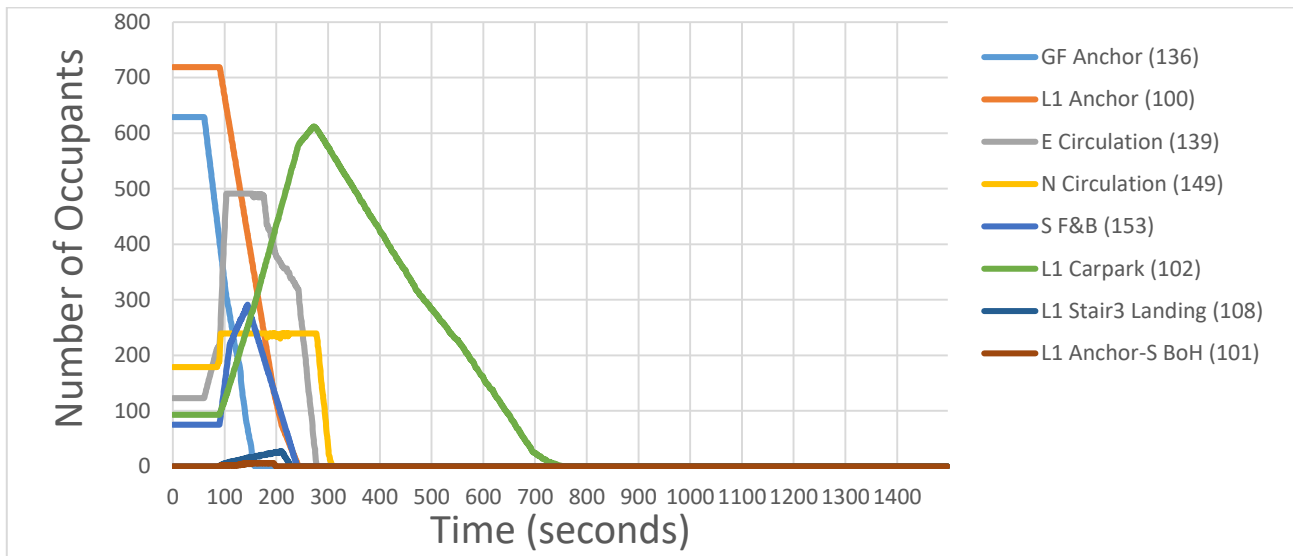


Figure 3 - EvacuatioNZ Node Clearance Times for Non-Base case CF1, CF2 and RC1.

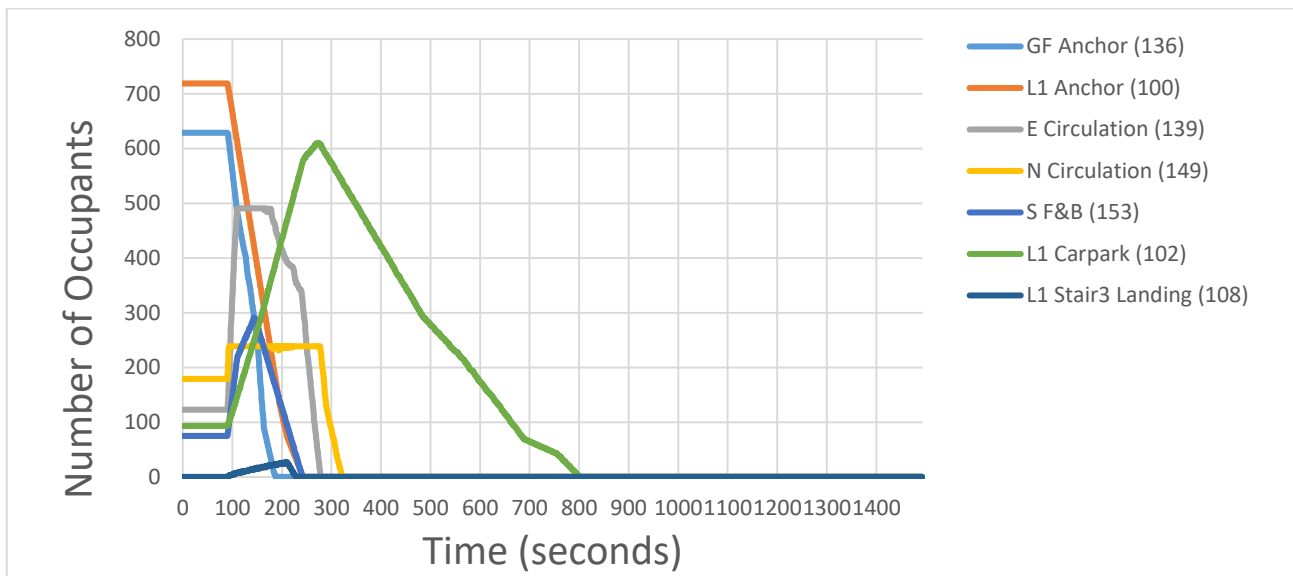


Figure 4 - EvacuatioNZ Node Clearance Times for Non-Base case CF3.

The following table summarises clearance times for various nodes:

Table 12 - Output Data for Non-Base case.

Location <sup>1</sup>	Clearance Time <sup>2,3</sup> (excl. detection time) (s)	
	CF1, CF2 & RC1 <sup>2</sup>	CF3 <sup>3</sup>
GF Anchor	158	188
L1 Anchor	243	243
L1 Stair 3 Landing <sup>4</sup>	229	229
L1 Anchor-S BoH <sup>5</sup>	199	199
L1 Carpark	751	802
N Circulation <sup>6</sup>	307	321
Corridor <sup>7</sup>	1496	1492
L0 Stair3 Landing <sup>8</sup>	246	246
L0 Stair 4 landing <sup>9</sup>	232	232

Explanatory Notes:

- 1) Location is the space represented as nodes in EvacuationNZ.
- 2) The Clearance Time for Challenging Fire Scenarios CF1, CF2 and Robustness Check Scenario RC1 includes notification time of 30 sec and pre-movement time of 30 sec for ground floor anchor space and 60 sec for first floor anchor space.
- 3) The Clearance Time for Challenging Fire Scenario CF3 includes notification time of 30 sec and pre-movement time of 60 sec for ground floor and first floor anchor space.
- 4) 'L1 Stair 3 Landing' is the node that corresponds to the lobby space before entering into Stair 3 which indicates the queuing clear time preceding stair 3.
- 5) 'L1 Anchor-S BoH' is the node that corresponds to the lobby space before entering into Stair 4 which indicate the queuing clear time preceding stair 4.
- 6) 'N Circulation' is the node that corresponds to the space precede the final exit from the Zone 2 ground floor mall space and is taken as the node where the last person leaves GF Anchor.
- 7) 'Corridor' is the node that corresponds to the space precede the final exit from Zone 3 Carpark building.
- 8) 'L0 Stair3 Landing' is the node that corresponds to the space precede the final exit from Stair 3 (i.e. time to clear L1 Anchor north stairwell) which is shared by the occupants from L2 Childcare space.
- 9) 'L0 Stair4 Landing' is the node that corresponds to the space precede the final exit from Stair 4 (i.e. time to clear L1 Anchor south stairwell).

The following table summarises RSET for various nodes:



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Table 13 - RSET time for Non-Base case.

CF	Location	Smoke Detector Activation Time <sup>1</sup> (s)	RSET <sup>2</sup> (s)
CF1	GF Anchor	41	199
	L1 Anchor		284
	L1 Stair 3 Landing <sup>3</sup>		270
	L1 Anchor-S BoH <sup>4</sup>		240
	L1 Carpark		792
	N Circulation <sup>5</sup>		348
	Corridor <sup>6</sup>		1537
	L0 Stair3 Landing <sup>7</sup>		287
	L0 Stair 4 landing <sup>8</sup>		273
CF2	GF Anchor	25	183
	L1 Anchor		268
	L1 Stair 3 Landing <sup>3</sup>		254
	L1 Anchor-S BoH <sup>4</sup>		224
	L1 Carpark		776
	N Circulation <sup>5</sup>		332
	Corridor <sup>6</sup>		1521
	L0 Stair3 Landing <sup>7</sup>		271
	L0 Stair 4 landing <sup>8</sup>		257
CF3	GF Anchor	29	217
	L1 Anchor		272
	L1 Stair 3 Landing <sup>3</sup>		258
	L1 Anchor-S BoH <sup>4</sup>		228
	L1 Carpark		831
	N Circulation <sup>5</sup>		350
	Corridor <sup>6</sup>		1521
	L0 Stair3 Landing <sup>7</sup>		275
	L0 Stair 4 landing <sup>8</sup>		261
RC1	GF Anchor	44	202
	L1 Anchor		287
	L1 Stair 3 Landing <sup>3</sup>		273
	L1 Anchor-S BoH <sup>4</sup>		243

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CF	Location	Smoke Detector Activation Time <sup>1</sup> (s)	RSET <sup>2</sup> (s)
	L1 Carpark		795
	N Circulation <sup>5</sup>		351
	Corridor <sup>6</sup>		1540
	L0 Stair3 Landing <sup>7</sup>		290
	L0 Stair 4 landing <sup>8</sup>		276

Explanatory notes:

- 1) Refer to Appendix C for a summary of the FDS results and smoke activation time.
- 2) RSET is calculated by the sum of Clearance Time plus smoke detector activation time.
- 3) 'L1 Stair 3 Landing' is the node that corresponds to the lobby space before entering into Stair 3 which indicates the queuing clear time preceding stair 3.
- 4) 'L1 Anchor-S BoH' is the node that corresponds to the lobby space before entering into Stair 4 which indicate the queuing clear time preceding stair 4.
- 5) 'N Circulation' is the node that corresponds to the space precede the final exit from the Zone 2 ground floor mall space and is taken as the node where the last person leaves GF Anchor.
- 6) 'Corridor' is the node that corresponds to the space precede the final exit from Zone 3 Carpark building and is taken as the node where the last person leaves L1 Anchor.
- 7) 'L0 Stair3 Landing' is the node that corresponds to the space precede the final exit from Stair 3 (L1 Anchor north stairwell) which is shared by the occupants from L2 Childcare space.
- 8) 'L0 Stair4 Landing' is the node that corresponds to the space precede the final exit from Stair 4 (i.e. time to clear L1 Anchor south stairwell).

#### B.4.1 Childcare Centre Evacuation - Non-Base Case

Stair 3 from the anchor space is the designated share egress for both Level 1 Anchor space and L2 Childcare centre. As can be seen above in Table 13, the time taken for the L1 Anchor occupant to egress via stair 3 for all three challenging fires are less than 300 seconds while the pre-movement time for the childcare building is 600 seconds for a fire within the Childcare centre and 660 seconds for a fire remote from the Childcare centre. Therefore, the egress time from the Childcare centre can be considered as isolated from the remainder of the building.

Attached is the following:

- EvacNZ model Setup FSK B.01 – B.06
- Non-Base case EvacuationNZ Setup.
- Non-Base case EvacuationNZ Output file.

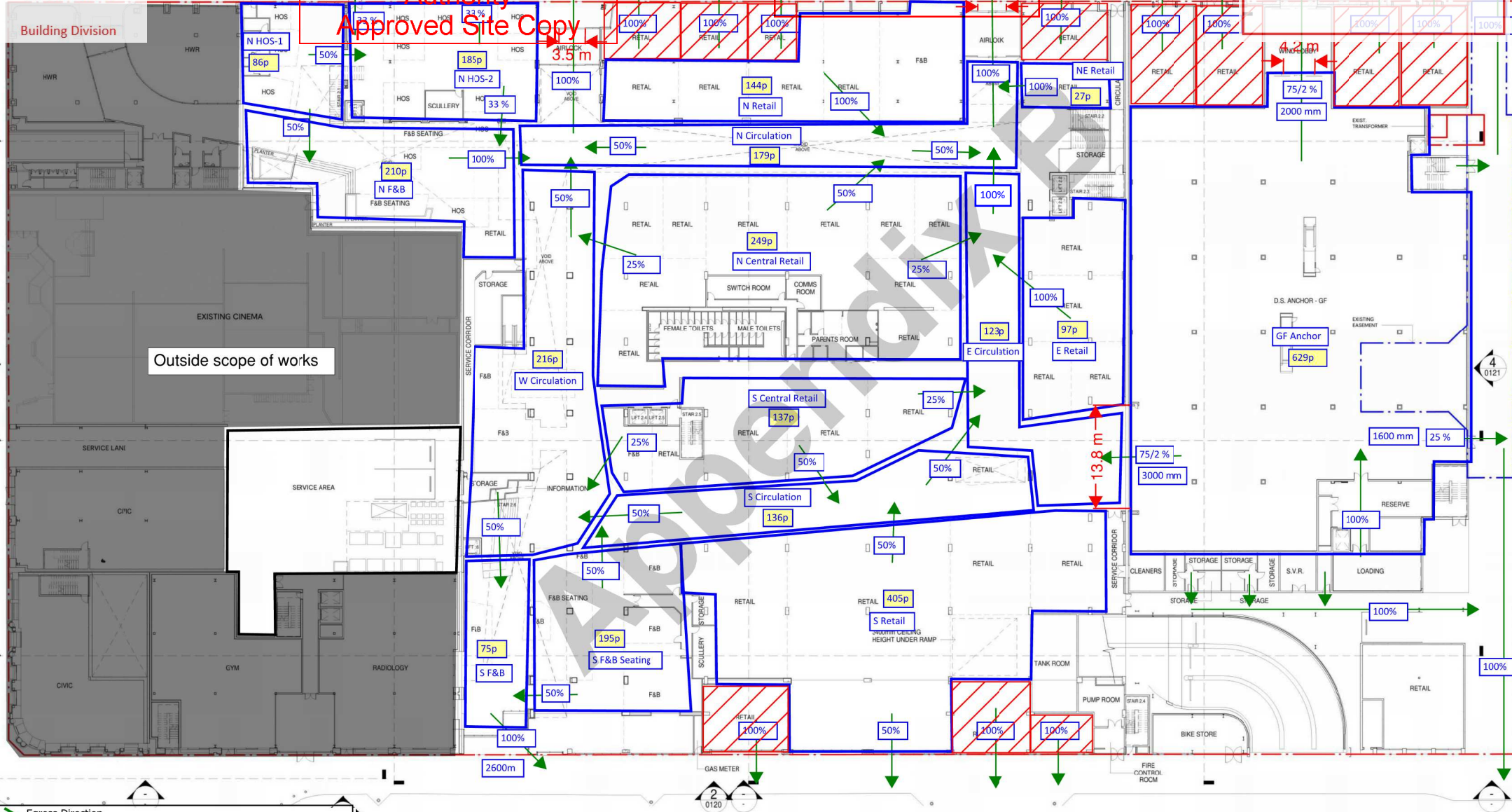
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- Egress Direction
- Occupant number as Per Appendix A ( the red numbers were updated in this Revision)
- Space modeled with occupants
- Space modeled no occupants
- Safe Place
- Spaces provided with independent mean of escape to outside and are not included in the model

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JOB NO.: 136249 DATE: 27/06/2019  
FSK.B.02 - Evacuation2 modelling setup L1\_REV: A

Revisions on site before commencing  
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INVERCARGILL  
Job Number  
317077

Scale: 1: 250 @A1  
Date Issued: 30/04/2019 11:45:05 AM  
Date Printed: 30/04/2019 11:45:05 AM  
Drawing Title: PRELIMINARY DESIGN

Drawing Title: SITE PLAN  
Z1 - Z6 OVERALL GROUND FLOOR PLAN  
Drawing Number: Z0-PD-A-0110

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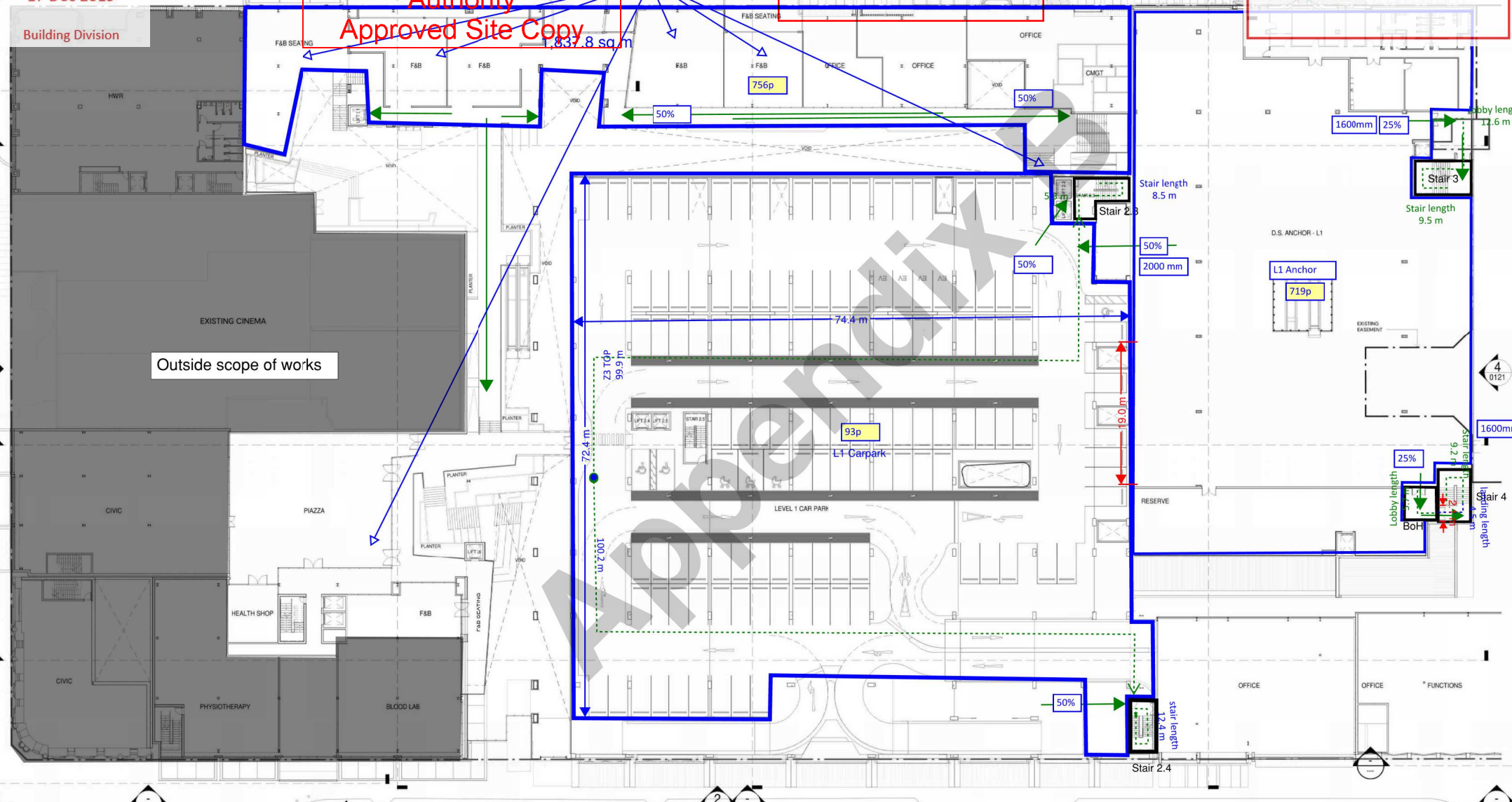
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To be developed further



Outside scope of works

- Egress Direction
- Occupant number as Per Appendix A ( the red numbers were updated in this Revision)
- Space modeled with occupants
- Space modeled no occupants
- Safe Place
- Spaces provided with independent mean of escape to outside and are not included in the model

PROJECT: HWCP Invercargill CBD Development  
JOB NO: 136249 DATE: 27/06/2019  
FSK.B.02 - EvacuationZ modelling setup L1\_REV\_A

**HWCP**  
INVERCARGILL CENTRAL  
TAY STREET & DEE STREET CORNER  
INVERCARGILL  
Project Number  
317077

Drawing Title  
SITE PLAN  
Z1 - Z6 OVERALL LEVEL 1 FLOOR PLAN  
Drawing Number  
Z0-PD-A-0111

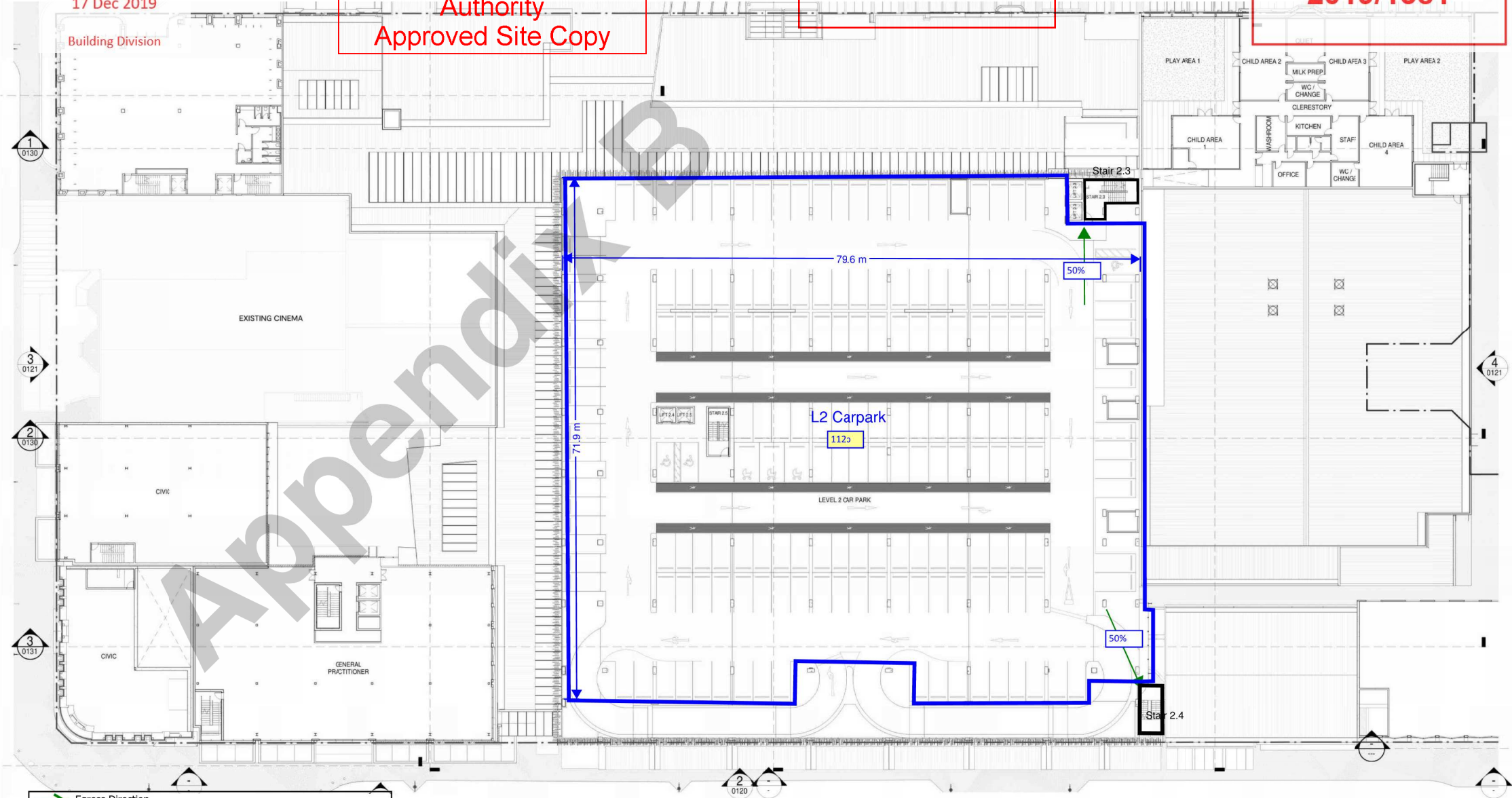
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- Egress Direction
- Occupant number as Per Appendix A ( the red numbers were updated in this Revision)
- Space modeled with occupants
- Space modeled no occupants
- Safe Place
- Spaces provided with independent mean of escape to outside and are not included in the model

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 Holmes JOB NO: 136249 DATE: 27/06/2019  
 FSK.B.03 - EvacuationZ modelling setup L2\_REV: A

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 INVERCARGILL  
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 317077

Drawing Title  
 SITE PLAN  
 Z1 - Z6 OVERALL LEVEL 2 FLOOR PLAN  
 Drawing Number  
 Z0-PD-A-0112

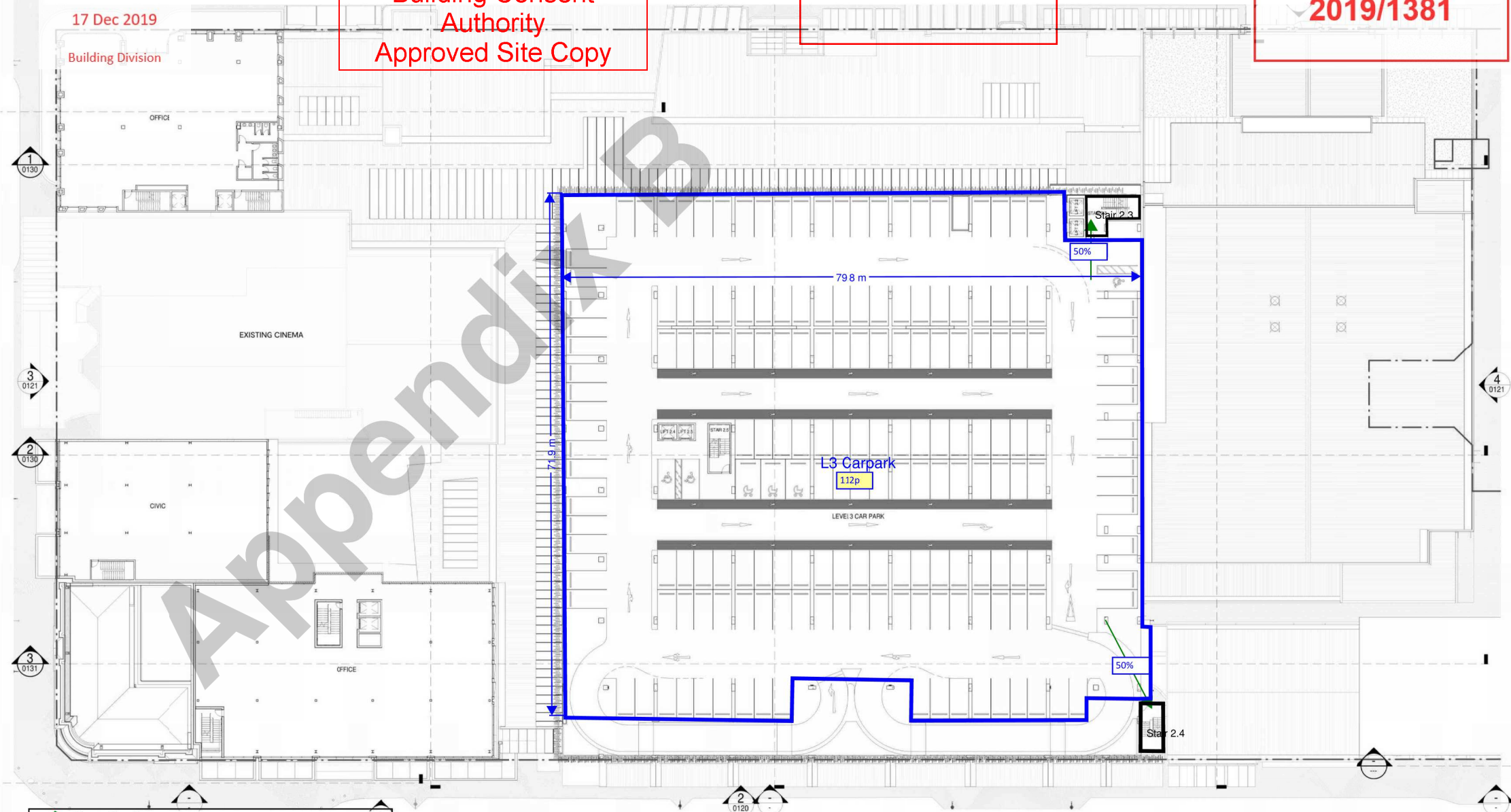
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Appendix B

- Egress Direction
- Occupant number as Per Appendix A ( the red numbers were updated in this Revision)
- Space modeled with occupants
- Space modeled no occupants
- Safe Place
- Spaces provided with independent mean of escape to outside and are not included in the model

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Holmes JOB NO: 136249 DATE: 27/06/2019  
FSK\_B.04 - EvacuationZ modelling setup L3\_REV\_A

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Drawing Title  
SITE PLAN  
Z1 - Z6 OVERALL LEVEL 3 FLOOR PLAN  
Drawing Number  
Z0-PD-A-0113

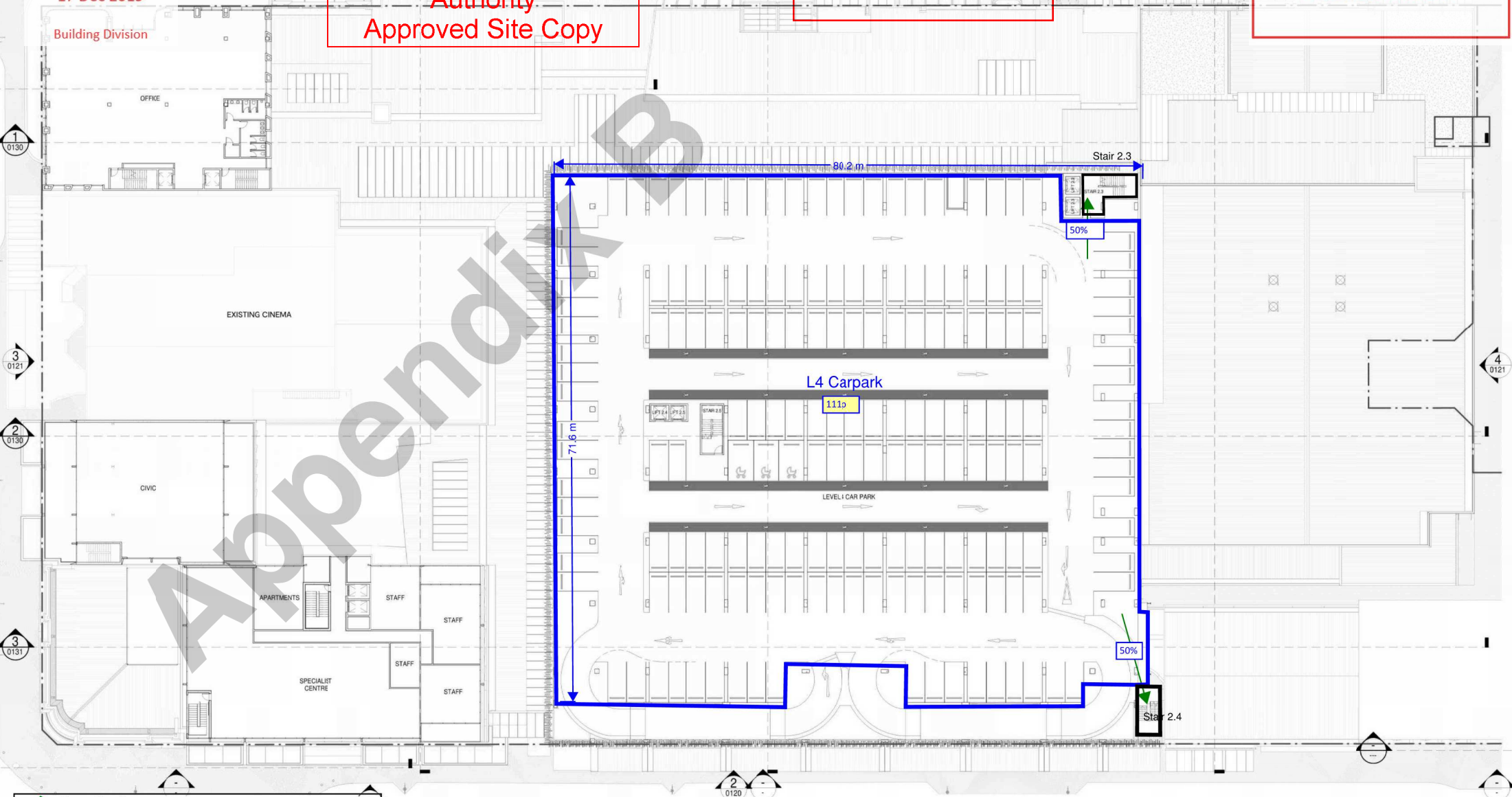
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Appendix B.4  
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- Egress Direction
- 11p Occupant number as Per Appendix A ( the red numbers were updated in this Revision)
- Space modeled with occupants
- Space modeled no occupants
- Safe Place
- Spaces provided with independent mean of escape to outside and are not included in the model

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JOB NO: 136249 DATE: 27/06/2019  
FSK.B.05 - EvacuationZ modelling setup L4\_REV\_A

ENG  
VGP  
DRT

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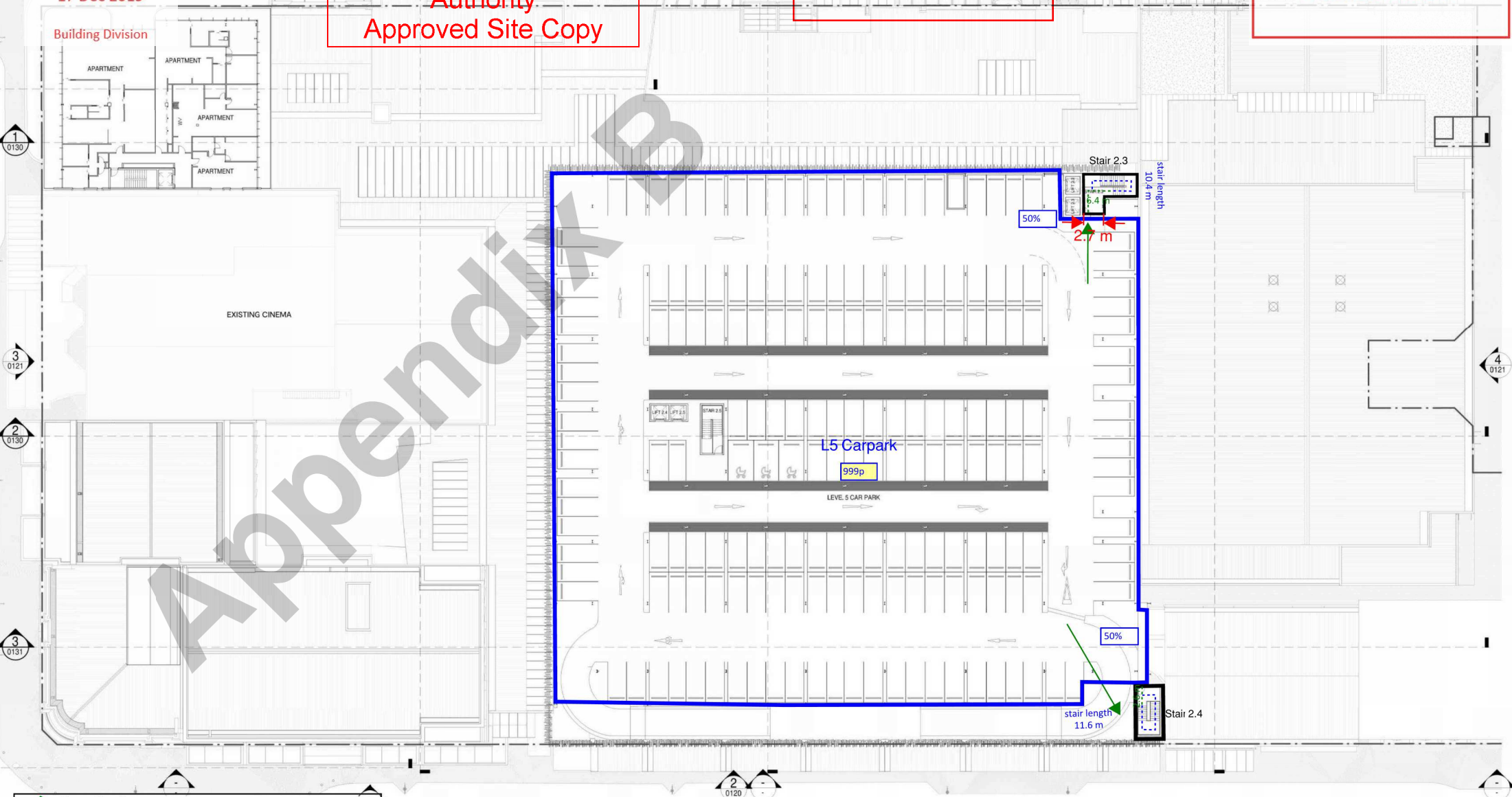
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Drawing Number  
Z0-PD-A-0114

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BUILDING CONSENT NUMBER  
Appendix B.4  
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- Egress Direction
- Occupant number as Per Appendix A ( the red numbers were updated in this Revision)
- Space modeled with occupants
- Space modeled no occupants
- Safe Place
- Spaces provided with independent mean of escape to outside and are not included in the model

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 FSK.B.06 - EvacuationZ modelling setup L5\_REV: A

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Drawing Title  
 SITE PLAN  
 Z1 - Z6 OVERALL LEVEL 5 FLOOR PLAN  
 Drawing Number  
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EvacuationNZ model for:  
Non-base Case  
- Challenging Fire 1 (CF1)  
- Challenging Fire 2 (CF2)  
- Robustness Check (RC1)

Appendix B.4

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**Personnel activity status**

Node type: 300 s, 2 min, 1 min, Safe

**Agent density and number**

Agent density: 0.2 agents/m<sup>2</sup>, 1 agents, 0.5 agents/m<sup>2</sup>

Agent number: 1 agents, 0.5 agents/m<sup>2</sup>

Agent status: Chromosome, Art gallery, Restaurants, Staircase, Bulk storage

**Doors and stairs**

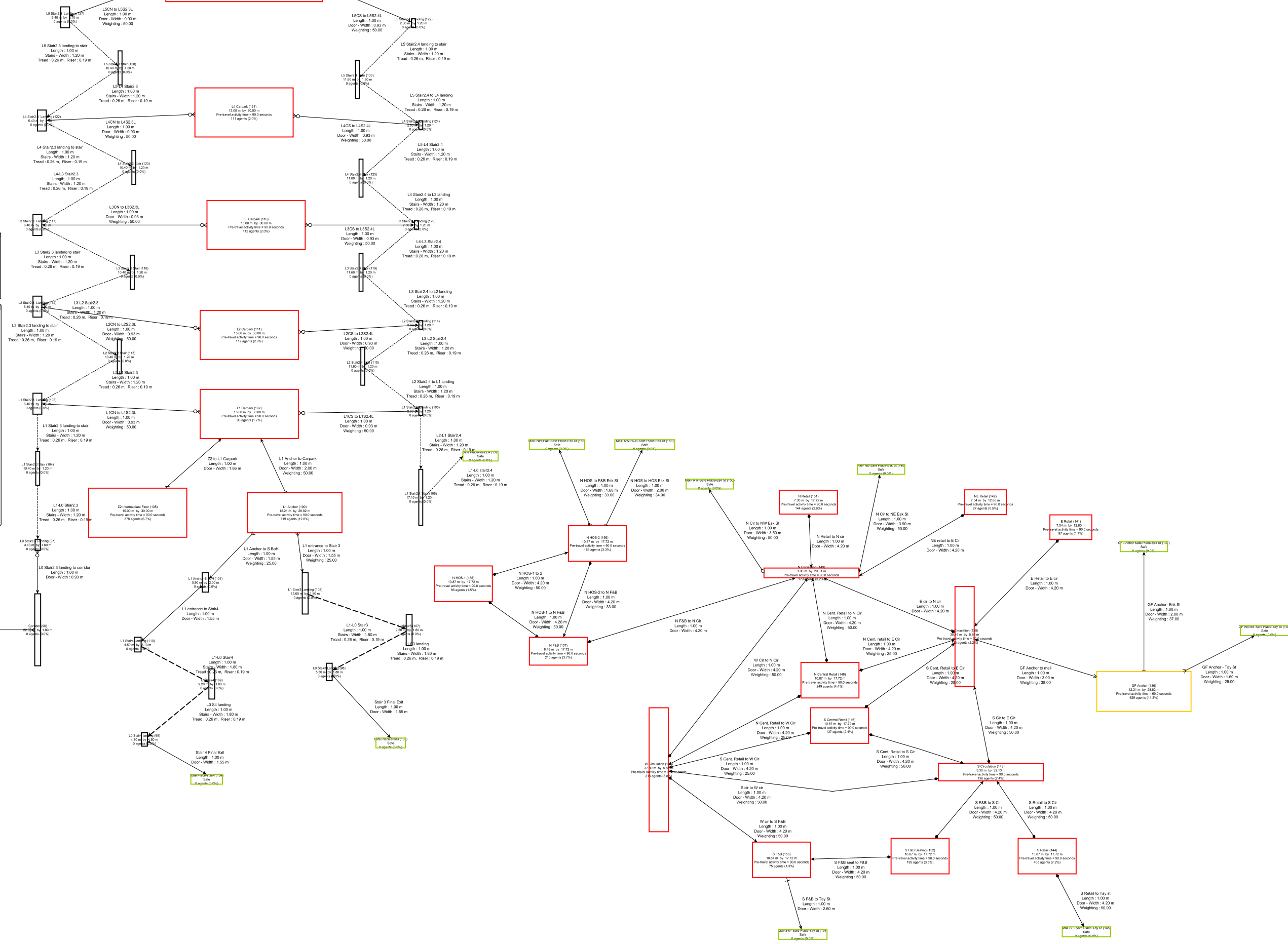
Connection types: Required

Door widths: 0.6m, 0.7m, 0.8m, 0.9m, 1.0m, 1.1m, 1.2m, 1.3m, 1.4m, 1.5m, 1.6m, 1.7m, 1.8m, 1.9m, 2.0m, 2.1m, 2.2m, 2.3m, 2.4m, 2.5m, 2.6m, 2.7m, 2.8m, 2.9m, 3.0m, 3.1m, 3.2m, 3.3m, 3.4m, 3.5m

Stair types: T=0.26m R=0.19m, T=0.28m R=0.19m, T=0.31m R=0.17m

**Settings**

Diagram scale: 1:100 mm, Output frequency: 1 min, CWI2, Node output, Agent output



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EvacuationNZ

Michael Spearpoint  
University of Canterbury  
version 2.11 - Holmes Fire release (Sep 19 2016)

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## Nodes

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Connections : [N HOS to HOS Esk St](#),

Node **Mall- NW-F&B-Safe Place-Esk St** - Safe  
Connections : [N HOS to F&B Esk St](#),

Node **N F&B**  
Dimensions 8.48 m by 17.72 m  
Connections : [N F&B to N Cir](#), [N HOS-2 to N F&B](#), [N HOS-1 to N F&B](#),

Node **N HOS-2**  
Dimensions 10.87 m by 17.72 m  
Connections : [N HOS-2 to N F&B](#), [N HOS to HOS Esk St](#), [N HOS to F&B Esk St](#), [N HOS-1 to 2](#),

Node **N HOS-1**  
Dimensions 10.87 m by 17.72 m  
Connections : [N HOS-1 to N F&B](#), [N HOS-1 to 2](#),

Node **Mall-SW- Safe Place-Tay St** - Safe  
Connections : [S F&B to Tay St](#),

Node **S F&B**  
Dimensions 10.87 m by 17.72 m  
Connections : [W cir to S F&B](#), [S F&B seat to F&B](#), [S F&B to Tay St](#),

Node **S F&B Seating**  
Dimensions 10.87 m by 17.72 m  
Connections : [S F&B to S Cir](#), [S F&B seat to F&B](#),

Node **N Retail**  
Dimensions 7.30 m by 17.72 m  
Connections : [N Retail to N cir](#),

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Node **Mall- NW-Safe Place-Esk St** - Safe  
Connections : [N Cir to NW Esk St](#),

Node **N Circulation**  
Dimensions 3.00 m by 29.01 m  
Connections : [E cir to N cir](#), [N F&B to N Cir](#), [W Cir to N Cir](#), [N Retail to N cir](#), [N Cir to NW Esk St](#),  
[N Cent. Retail to N Cir](#), [NE retail to E Cir](#), [N Cir to NE Esk St](#),

Node **N Central Retail**  
Dimensions 10.87 m by 17.72 m  
Connections : [N Cent. Retail to W Cir](#), [N Cent. retail to E Cir](#), [N Cent. Retail to N Cir](#),

Node **W Circulation**  
Dimensions 37.89 m by 5.86 m  
Connections : [S cir to W cir](#), [W cir to S F&B](#), [W Cir to N Cir](#), [N Cent. Retail to W Cir](#), [S Cent. Retail to W Cir](#),

Node **S Central Retail**  
Dimensions 10.87 m by 17.72 m  
Connections : [S Cent. Retail to W Cir](#), [S Cent. Retail to E Cir](#), [S Cent. Retail to S Cir](#),

Node **Mall-SE- Safe Place-Tay St** - Safe  
Connections : [S Retail to Tay st](#),

Node **S Retail**  
Dimensions 10.87 m by 17.72 m  
Connections : [S Retail to Tay st](#), [S Retail to S Cir](#),

Node **S Circulation**  
Dimensions 5.30 m by 32.13 m  
Connections : [S cir to W cir](#), [S F&B to S Cir](#), [S Cent. Retail to S Cir](#), [S Retail to S Cir](#), [S Cir to E Cir](#),

Node **NE Retail**  
Dimensions 7.54 m by 12.80 m  
Connections : [NE retail to E Cir](#),

Node **E Retail**  
Dimensions 7.54 m by 12.80 m  
Connections : [E Retail to E cir](#),

Node **Mall- NE-Safe Place-Esk St** - Safe  
Connections : [N Cir to NE Esk St](#),

Node **E Circulation**  
Dimensions 30.49 m by 5.86 m  
Connections : [E cir to N cir](#), [N Cent. retail to E Cir](#), [S Cent. Retail to E Cir](#), [S Cir to E Cir](#), [E Retail to E cir](#), [GF Anchor to mall](#),

Node **GF Anchor Safe Place-Tay St** - Safe  
Connections : [GF Anchor - Tay St](#),

Node **GF Anchor Safe Place-Esk St** - Safe  
Connections : [GF Anchor- Esk St](#),

Node **GF Anchor**  
Dimensions 12.21 m by 28.82 m  
Connections : [GF Anchor to mall](#), [GF Anchor - Tay St](#), [GF Anchor- Esk St](#),

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Node **Z2 Intermediate Floor**  
17 Dec 2019 15.00 m by 30.00 m  
Connections : [Z2 to L1 Carpark,](#)

Building Division  
Node **Safe Place-stair4** - Safe  
Connections : [Stair 4 Final Exit,](#)

Node **Safe Place-stair3** - Safe  
Connections : [Stair 3 Final Exit,](#)

Node **Safe Place-stair2.4** - Safe  
Connections : [L1-L0 stair2.4,](#)

Node **Safe Place-stair2.3** - Safe  
Connections : [Stair 2.3 Final Exit,](#)

Node **L5 Stair2.4 stair**  
Dimensions 11.60 m by 1.20 m  
Connections : [L5 Stair2.4 landing to stair,](#) [L5 Stair2.4 to L4 landing,](#)

Node **L5 Stair2.4 Landing**  
Dimensions 2.60 m by 1.20 m  
Connections : [L5 Stair2.4 landing to stair,](#) [L5CS to L5S2.4L,](#)

Node **L5 Stair2.3 Stair**  
Dimensions 10.40 m by 1.20 m  
Connections : [L5 Stair2.3 landing to stair,](#) [L5-L4 Stair2.3,](#)

Node **L5 Stair2.3 Landing**  
Dimensions 6.40 m by 2.70 m  
Connections : [L5 Stair2.3 landing to stair,](#) [L5CN to L5S2.3L,](#)

Node **L5 Carpark**  
Dimensions 30.00 m by 47.80 m  
Connections : [L5CN to L5S2.3L,](#) [L5CS to L5S2.4L,](#)

Node **L4 Stair2.4 Stair**  
Dimensions 11.60 m by 1.20 m  
Connections : [L5-L4 Stair2.4,](#) [L4 Stair2.4 to L3 landing,](#)

Node **L4 Stair2.4 Landing**  
Dimensions 2.60 m by 1.20 m  
Connections : [L5-L4 Stair2.4,](#) [L4CS to L4S2.4L,](#) [L5 Stair2.4 to L4 landing,](#)

Node **L4 Stair2.3 Stair**  
Dimensions 10.40 m by 1.20 m  
Connections : [L4 Stair2.3 landing to stair,](#) [L4-L3 Stair2.3,](#)

Node **L4 Stair2.3 Landing**  
Dimensions 6.40 m by 2.70 m  
Connections : [L4 Stair2.3 landing to stair,](#) [L4CN to L4S2.3L,](#) [L5-L4 Stair2.3,](#)

Node **L4 Carpark**  
Dimensions 15.00 m by 30.00 m  
Connections : [L4CN to L4S2.3L,](#) [L4CS to L4S2.4L,](#)

Node **L3 Stair2.4 Landing**  
Dimensions 2.60 m by 1.20 m

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Connections : [L4-L3 Stair2.4,](#) [L3CS to L3S2.4L,](#) [L4 Stair2.4 to L3 landing,](#)

Node **L3 Stair2.3 Stair**  
Dimensions 11.60 m by 1.20 m  
Connections : [L4-L3 Stair2.4,](#) [L3 Stair2.4 to L2 landing,](#)

Node **L3 Stair2.3 Stair**  
Dimensions 10.40 m by 1.20 m  
Connections : [L3 Stair2.3 landing to stair,](#) [L3-L2 Stair2.3,](#)

Node **L3 Stair2.3 Landing**  
Dimensions 6.40 m by 2.70 m  
Connections : [L3 Stair2.3 landing to stair,](#) [L3CN to L3S2.3L,](#) [L4-L3 Stair2.3,](#)

Node **L3 Carpark**  
Dimensions 15.00 m by 30.00 m  
Connections : [L3CS to L3S2.4L,](#) [L3CN to L3S2.3L,](#)

Node **L2 Stair2.4 Stair**  
Dimensions 11.60 m by 1.20 m  
Connections : [L3-L2 Stair2.4,](#) [L2 Stair2.4 to L1 landing,](#)

Node **L2 Stair2.4 Landing**  
Dimensions 2.60 m by 1.20 m  
Connections : [L3-L2 Stair2.4,](#) [L2CS to L2S2.4L,](#) [L3 Stair2.4 to L2 landing,](#)

Node **L2 Stair2.3 Stair**  
Dimensions 10.40 m by 1.20 m  
Connections : [L2 Stair2.3 landing to stair,](#) [L2-L1 Stair2.3,](#)

Node **L2 Stair2.3 Landing**  
Dimensions 6.40 m by 2.70 m  
Connections : [L2 Stair2.3 landing to stair,](#) [L2CN to L2S2.3L,](#) [L3-L2 Stair2.3,](#)

Node **L2 Carpark**  
Dimensions 15.00 m by 30.00 m  
Connections : [L2CS to L2S2.4L,](#) [L2CN to L2S2.3L,](#)

Node **L1 Stair4 Landing**  
Dimensions 4.50 m by 2.10 m  
Connections : [L1-L0 Stair4,](#) [L1 entrance to Stair4,](#)

Node **L1 Stair4**  
Dimensions 9.20 m by 1.80 m  
Connections : [L0 S4 landing,](#) [L1-L0 Stair4,](#)

Node **L1 Stair3 Landing**  
Dimensions 12.60 m by 1.80 m  
Connections : [L1 entrance to Stair 3,](#) [L1-L0 Stair3,](#)

Node **L1 Stair3**  
Dimensions 9.50 m by 1.80 m  
Connections : [L1 S3 landing,](#) [L1-L0 Stair3,](#)

Node **L1 Stair2.4 Stair**  
Dimensions 17.10 m by 1.20 m  
Connections : [L2-L1 Stair2.4,](#) [L1-L0 stair2.4,](#)

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Node **L1 Stair2.4 Landing**  
17 Dec 2019 1.60 m by 1.20 m

Connections : [L2-L1 Stair2.4](#), [L1CS to L1S2.4L](#), [L2 Stair2.4 to L1 landing](#),

Building Division  
Node **L1 Stair2.3 Stair**

Dimensions 10.40 m by 1.20 m

Connections : [L1 Stair2.3 landing to stair](#), [L1-L0 Stair2.3](#),

Node **L1 Stair2.3 Landing**

Dimensions 6.40 m by 2.70 m

Connections : [L1 Stair2.3 landing to stair](#), [L1CN to L1S2.3L](#), [L2-L1 Stair2.3](#),

Node **L1 Carpark**

Dimensions 15.00 m by 30.00 m

Connections : [Z2 to L1 Carpark](#), [L1 Anchor to Carpark](#), [L1CS to L1S2.4L](#), [L1CN to L1S2.3L](#),

Node **L1 Anchor-S BoH**

Dimensions 5.90 m by 2.00 m

Connections : [L1 Anchor to S BoH](#), [L1 entrance to Stair4](#),

Node **L1 Anchor**

Dimensions 12.21 m by 28.82 m

Connections : [L1 entrance to Stair 3](#), [L1 Anchor to S BoH](#), [L1 Anchor to Carpark](#),

Node **L0 Stair4 landing**

Dimensions 4.10 m by 1.80 m

Connections : [Stair 4 Final Exit](#), [L0 S4 landing](#),

Node **L0 Stair3 Landing**

Dimensions 5.30 m by 1.80 m

Connections : [Stair 3 Final Exit](#), [L1 S3 landing](#),

Node **L0 Stair2.3 Landing**

Dimensions 3.40 m by 1.60 m

Connections : [L1-L0 Stair2.3](#), [L0 Stair2.3 landing to corridor](#),

Node **Corridor**

Dimensions 22.00 m by 1.80 m

Connections : [Stair 2.3 Final Exit](#), [L0 Stair2.3 landing to corridor](#),

**Connections**

Connection **L0 Stair2.3 landing to corridor**

Length 1.00 m

Connecting [L0 Stair2.3 Landing](#) to [Corridor](#) (target node for required path)

Door width 0.93 m, specific flow 1.33 persons/s per m eff. width

Connection **Stair 2.3 Final Exit**

Length 1.00 m

Connecting [Corridor](#) to [Safe Place-stair2.3](#) (target node for required path)

Door width 0.93 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)

Connection **L1-L0 stair2.4**

Length 1.00 m

Connecting [L1 Stair2.4 Stair](#) to [Safe Place-stair2.4](#) (target node for required path)

Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

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Connection **L2 Stair2.4 to L1 landing**

Length 1.00 m

Connecting [L2 Stair2.4 Stair](#) to [L1 Stair2.4 Landing](#) (target node for required path)

Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L3 Stair2.4 to L2 landing**

Length 1.00 m

Connecting [L3 Stair2.3 Stair](#) to [L2 Stair2.4 Landing](#) (target node for required path)

Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L4 Stair2.4 to L3 landing**

Length 1.00 m

Connecting [L4 Stair2.4 Stair](#) to [L3 Stair2.4 Landing](#) (target node for required path)

Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L5 Stair2.4 to L4 landing**

Length 1.00 m

Connecting [L5 Stair2.4 stair](#) to [L4 Stair2.4 Landing](#) (target node for required path)

Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L1-L0 Stair2.3**

Length 1.00 m

Connecting [L1 Stair2.3 Stair](#) to [L0 Stair2.3 Landing](#) (target node for required path)

Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L2-L1 Stair2.3**

Length 1.00 m

Connecting [L2 Stair2.3 Stair](#) to [L1 Stair2.3 Landing](#) (target node for required path)

Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L3-L2 Stair2.3**

Length 1.00 m

Connecting [L3 Stair2.3 Stair](#) to [L2 Stair2.3 Landing](#) (target node for required path)

Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L4-L3 Stair2.3**

Length 1.00 m

Connecting [L4 Stair2.3 Stair](#) to [L3 Stair2.3 Landing](#) (target node for required path)

Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L5CS to L5S2.4L**

Length 1.00 m

Connecting [L5 Carpark](#) to [L5 Stair2.4 Landing](#) (target node for required path)

Door width 0.93 m, specific flow 1.33 persons/s per m eff. width

Connection **L5CN to L5S2.3L**

Length 1.00 m

Connecting [L5 Carpark](#) to [L5 Stair2.3 Landing](#) (target node for required path)

Door width 0.93 m, specific flow 1.33 persons/s per m eff. width

Connection **L5-L4 Stair2.3**

Length 1.00 m

Connecting [L5 Stair2.3 Stair](#) to [L4 Stair2.3 Landing](#) (target node for required path)

Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L1CN to L1S2.3L**

Length 1.00 m

Connecting [L1 Carpark](#) to [L1 Stair2.3 Landing](#) (target node for required path)

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Door width 0.93 m, specific flow 1.33 persons/s per m eff. width  
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Connection **L1CS to L1S2.4L**

Length 1.00 m  
Connecting [L1 Carpark](#) to [L1 Stair2.4 Landing](#) (target node for required path)  
Door width 0.93 m, specific flow 1.33 persons/s per m eff. width

Connection **L2CN to L2S2.3L**

Length 1.00 m  
Connecting [L2 Carpark](#) to [L2 Stair2.3 Landing](#) (target node for required path)  
Door width 0.93 m, specific flow 1.33 persons/s per m eff. width

Connection **L2CS to L2S2.4L**

Length 1.00 m  
Connecting [L2 Carpark](#) to [L2 Stair2.4 Landing](#) (target node for required path)  
Door width 0.93 m, specific flow 1.33 persons/s per m eff. width

Connection **L3CN to L3S2.3L**

Length 1.00 m  
Connecting [L3 Carpark](#) to [L3 Stair2.3 Landing](#) (target node for required path)  
Door width 0.93 m, specific flow 1.33 persons/s per m eff. width

Connection **L3CS to L3S2.4L**

Length 1.00 m  
Connecting [L3 Carpark](#) to [L3 Stair2.4 Landing](#) (target node for required path)  
Door width 0.93 m, specific flow 1.33 persons/s per m eff. width

Connection **L4CS to L4S2.4L**

Length 1.00 m  
Connecting [L4 Carpark](#) to [L4 Stair2.4 Landing](#) (target node for required path)  
Door width 0.93 m, specific flow 1.33 persons/s per m eff. width

Connection **L4CN to L4S2.3L**

Length 1.00 m  
Connecting [L4 Carpark](#) to [L4 Stair2.3 Landing](#) (target node for required path)  
Door width 0.93 m, specific flow 1.33 persons/s per m eff. width

Connection **L5 Stair2.4 landing to stair**

Length 1.00 m  
Connecting [L5 Stair2.4 Landing](#) to [L5 Stair2.4 stair](#) (target node for required path)  
Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L5-L4 Stair2.4**

Length 1.00 m  
Connecting [L4 Stair2.4 Landing](#) to [L4 Stair2.4 Stair](#) (target node for required path)  
Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L4-L3 Stair2.4**

Length 1.00 m  
Connecting [L3 Stair2.4 Landing](#) to [L3 Stair2.3 Stair](#) (target node for required path)  
Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L3-L2 Stair2.4**

Length 1.00 m  
Connecting [L2 Stair2.4 Landing](#) to [L2 Stair2.4 Stair](#) (target node for required path)  
Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L2-L1 Stair2.4**

Length 1.00 m

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Length 1.00 m  
Connecting [L1 Stair2.4 Landing](#) to [L1 Stair2.4 Stair](#) (target node for required path)  
Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L5 Stair2.3 landing to stair**

Length 1.00 m  
Connecting [L5 Stair2.3 Landing](#) to [L5 Stair2.3 Stair](#) (target node for required path)  
Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L4 Stair2.3 landing to stair**

Length 1.00 m  
Connecting [L4 Stair2.3 Landing](#) to [L4 Stair2.3 Stair](#) (target node for required path)  
Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L3 Stair2.3 landing to stair**

Length 1.00 m  
Connecting [L3 Stair2.3 Landing](#) to [L3 Stair2.3 Stair](#) (target node for required path)  
Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L2 Stair2.3 landing to stair**

Length 1.00 m  
Connecting [L2 Stair2.3 Landing](#) to [L2 Stair2.3 Stair](#) (target node for required path)  
Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L1 Stair2.3 landing to stair**

Length 1.00 m  
Connecting [L1 Stair2.3 Landing](#) to [L1 Stair2.3 Stair](#) (target node for required path)  
Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L1-L0 Stair3**

Length 1.00 m  
Connecting [L1 Stair3 Landing](#) to [L1 Stair3](#) (target node for required path)  
Stairs width 1.80 m, tread 0.26 m, riser 0.19 m

Connection **L1 S3 landing**

Length 1.00 m  
Connecting [L1 Stair3](#) to [L0 Stair3 Landing](#) (target node for required path)  
Stairs width 1.80 m, tread 0.26 m, riser 0.19 m

Connection **L1 entrance to Stair4**

Length 1.00 m  
Connecting [L1 Anchor-S BoH](#) to [L1 Stair4 Landing](#) (target node for required path)  
Door width 1.55 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)

Connection **L1-L0 Stair4**

Length 1.00 m  
Connecting [L1 Stair4 Landing](#) to [L1 Stair4](#) (target node for required path)  
Stairs width 1.80 m, tread 0.26 m, riser 0.19 m

Connection **L0 S4 landing**

Length 1.00 m  
Connecting [L1 Stair4](#) to [L0 Stair4 landing](#) (target node for required path)  
Stairs width 1.80 m, tread 0.26 m, riser 0.19 m

Connection **Stair 4 Final Exit**

Length 1.00 m  
Connecting [L0 Stair4 landing](#) to [Safe Place-stair4](#) (target node for required path)  
Door width 1.55 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)

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Connection **Stair 3 Final Exit**  
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Connecting [L0 Stair3 Landing](#) to [Safe Place-stair3](#) (target node for required path)  
Door width 1.55 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)

Connection **L1 Anchor to Carpark**

Length 1.00 m  
Connecting [L1 Anchor](#) to [L1 Carpark](#) (target node for required path)  
Door width 2.00 m, specific flow 1.33 persons/s per m eff. width

Connection **Z2 to L1 Carpark**

Length 1.00 m  
Connecting [Z2 Intermediate Floor](#) to [L1 Carpark](#) (target node for required path)  
Door width 1.86 m, specific flow 1.33 persons/s per m eff. width

Connection **L1 Anchor to S BoH**

Length 1.00 m  
Connecting [L1 Anchor](#) to [L1 Anchor-S BoH](#) (target node for required path)  
Door width 1.55 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)

Connection **L1 entrance to Stair 3**

Length 1.00 m  
Connecting [L1 Anchor](#) to [L1 Stair3 Landing](#) (target node for required path)  
Door width 1.55 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)

Connection **GF Anchor- Esk St**

Length 1.00 m  
Connecting [GF Anchor](#) to [GF Anchor Safe Place-Esk St](#) (target node for required path)  
Door width 2.00 m, specific flow 1.33 persons/s per m eff. width

Connection **GF Anchor - Tay St**

Length 1.00 m  
Connecting [GF Anchor](#) to [GF Anchor Safe Place-Tay St](#) (target node for required path)  
Door width 1.60 m, specific flow 1.33 persons/s per m eff. width

Connection **GF Anchor to mall**

Length 1.00 m  
Connecting [GF Anchor](#) to [E Circulation](#) (target node for required path)  
Door width 3.00 m, specific flow 1.33 persons/s per m eff. width

Connection **N Cir to NE Esk St**

Length 1.00 m  
Connecting [N Circulation](#) to [Mall- NE-Safe Place-Esk St](#) (target node for required path)  
Door width 3.90 m, specific flow 1.33 persons/s per m eff. width

Connection **NE retail to E Cir**

Length 1.00 m  
Connecting [NE Retail](#) to [N Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **E Retail to E cir**

Length 1.00 m  
Connecting [E Retail](#) to [E Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **S Cir to E Cir**

Length 1.00 m  
Connecting [S Circulation](#) to [E Circulation](#) (target node for required path)

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Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **S Retail to S Cir**

Length 1.00 m  
Connecting [S Retail](#) to [S Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **S Retail to Tay st**

Length 1.00 m  
Connecting [S Retail](#) to [Mall-SE- Safe Place-Tay St](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **S Cent. Retail to S Cir**

Length 1.00 m  
Connecting [S Central Retail](#) to [S Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **S Cent. Retail to E Cir**

Length 1.00 m  
Connecting [S Central Retail](#) to [E Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **S Cent. Retail to W Cir**

Length 1.00 m  
Connecting [S Central Retail](#) to [W Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **N Cent. Retail to N Cir**

Length 1.00 m  
Connecting [N Central Retail](#) to [N Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **N Cent. retail to E Cir**

Length 1.00 m  
Connecting [N Central Retail](#) to [E Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **N Cent. Retail to W Cir**

Length 1.00 m  
Connecting [N Central Retail](#) to [W Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **N Cir to NW Esk St**

Length 1.00 m  
Connecting [N Circulation](#) to [Mall- NW-Safe Place-Esk St](#) (target node for required path)  
Door width 3.50 m, specific flow 1.33 persons/s per m eff. width

Connection **N Retail to N cir**

Length 1.00 m  
Connecting [N Retail](#) to [N Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **W Cir to N Cir**

Length 1.00 m  
Connecting [W Circulation](#) to [N Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **S F&B to Tay St**

**Approved For Issue**  
**27/02/2020**

**BUILDING CONSENT NUMBER**  
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**2019/1381**

**Invercargill City Council**  
**Building Consent Authority**  
**Approved Site Copy**

EvacuationNZ model for:  
Non-base Case  
- Challenging Fire 1 (CF1)  
- Challenging Fire 2 (CF2)  
Robustness Check (RC1)

**Document Received**

Length 1.00 m  
**17-Dec-2019** F&B to Mall-SW- Safe Place-Tay St (target node for required path)  
Door width 2.60 m, specific flow 1.33 persons/s per m eff. width

**Building Division**

Connection **S F&B seat to F&B**  
Length 1.00 m  
Connecting [S F&B Seating](#) to [S F&B](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **S F&B to S Cir**  
Length 1.00 m  
Connecting [S F&B Seating](#) to [S Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **W cir to S F&B**  
Length 1.00 m  
Connecting [W Circulation](#) to [S F&B](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **N HOS-1 to 2**  
Length 1.00 m  
Connecting [N HOS-1](#) to [N HOS-2](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **N HOS-1 to N F&B**  
Length 1.00 m  
Connecting [N HOS-1](#) to [N F&B](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **N HOS to F&B Esk St**  
Length 1.00 m  
Connecting [N HOS-2](#) to [Mall- NW-F&B-Safe Place-Esk St](#) (target node for required path)  
Door width 1.60 m, specific flow 1.33 persons/s per m eff. width

Connection **N HOS to HOS Esk St**  
Length 1.00 m  
Connecting [N HOS-2](#) to [Mall- NW-HOS-Safe Place-Esk St](#) (target node for required path)  
Door width 2.00 m, specific flow 1.33 persons/s per m eff. width

Connection **N HOS-2 to N F&B**  
Length 1.00 m  
Connecting [N HOS-2](#) to [N F&B](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **N F&B to N Cir**  
Length 1.00 m  
Connecting [N F&B](#) to [N Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **S cir to W cir**  
Length 1.00 m  
Connecting [S Circulation](#) to [W Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **E cir to N cir**  
Length 1.00 m  
Connecting [E Circulation](#) to [N Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

**Population**

Name	Number	Density (agents/m <sup>2</sup> )	Density (m <sup>2</sup> /agent)
<a href="#">L1 Anchor</a>	719	2.04	0.49
<a href="#">L1 Carpark</a>	93	0.21	4.84
<a href="#">L2 Carpark</a>	112	0.25	4.02
<a href="#">L3 Carpark</a>	112	0.25	4.02
<a href="#">L4 Carpark</a>	111	0.25	4.05
<a href="#">L5 Carpark</a>	999	0.70	1.44
<a href="#">Z2 Intermediate Floor</a>	378	0.84	1.19
<a href="#">GF Anchor</a>	629	1.79	0.56
<a href="#">E Circulation</a>	123	0.69	1.45
<a href="#">E Retail</a>	97	1.01	0.99
<a href="#">NE Retail</a>	27	0.28	3.57
<a href="#">S Circulation</a>	136	0.80	1.25
<a href="#">S Retail</a>	405	2.10	0.48
<a href="#">S Central Retail</a>	137	0.71	1.41
<a href="#">W Circulation</a>	216	0.97	1.03
<a href="#">N Central Retail</a>	249	1.29	0.77
<a href="#">N Circulation</a>	179	2.06	0.49
<a href="#">N Retail</a>	144	1.11	0.90
<a href="#">S F&amp;B Seating</a>	195	1.01	0.99
<a href="#">S F&amp;B</a>	75	0.39	2.57
<a href="#">N HOS-1</a>	86	0.45	2.24
<a href="#">N HOS-2</a>	185	0.96	1.04
<a href="#">N F&amp;B</a>	210	1.40	0.72

**Results**

Simulation run 1 : Total number of agents = 5617

- Node [N HOS-1](#) clear at 98.5 s
- Node [S Central Retail](#) clear at 103.5 s
- Node [S F&B Seating](#) clear at 109.5 s
- Node [NE Retail](#) clear at 130.0 s
- Node [S Retail](#) clear at 132.0 s

Node **N HOS-2** clear at 136.0 s  
Node **L Retail** clear at 152.0 s  
Node **GF Anchor** clear at 157.5 s  
Node **N Central Retail** clear at 160.0 s  
Node **S Circulation** clear at 176.0 s  
Node **L3 Carpark** clear at 185.5 s  
Node **L2 Carpark** clear at 201.0 s  
Node **N F&B** clear at 228.5 s  
Node **W Circulation** clear at 231.0 s  
Node **S F&B** clear at 239.5 s  
Node **N Retail** clear at 242.5 s  
Node **L1 Anchor** clear at 243.0 s  
Node **Z2 Intermediate Floor** clear at 272.5 s  
Node **E Circulation** clear at 277.5 s  
Node **N Circulation** clear at 307.0 s  
Node **L4 Carpark** clear at 508.5 s  
Node **L1 Carpark** clear at 751.0 s  
Node **L5 Carpark** clear at 1050.5 s

Last agent to leave node **N F&B** was 'Agent #5137' at 228.5 s  
Last agent to leave node **N HOS-2** was 'Agent #5144' at 136.0 s  
Last agent to leave node **N HOS-1** was 'Agent #5137' at 98.5 s  
Last agent to leave node **S F&B** was 'Agent #3538' at 239.5 s  
Last agent to leave node **S F&B Seating** was 'Agent #4867' at 109.5 s  
Last agent to leave node **N Retail** was 'Agent #4723' at 242.5 s  
Last agent to leave node **N Circulation** was 'Agent #2529' at 307.0 s  
Last agent to leave node **N Central Retail** was 'Agent #4300' at 160.0 s  
Last agent to leave node **W Circulation** was 'Agent #4869' at 231.0 s  
Last agent to leave node **S Central Retail** was 'Agent #3943' at 103.5 s  
Last agent to leave node **S Retail** was 'Agent #3539' at 132.0 s  
Last agent to leave node **S Circulation** was 'Agent #3537' at 176.0 s  
Last agent to leave node **NE Retail** was 'Agent #3374' at 130.0 s  
Last agent to leave node **E Retail** was 'Agent #3277' at 152.0 s  
Last agent to leave node **E Circulation** was 'Agent #2526' at 277.5 s  
Last agent to leave node **GF Anchor** was 'Agent #2525' at 157.5 s  
Last agent to leave node **Z2 Intermediate Floor** was 'Agent #2147' at 272.5 s  
Last agent to leave node **L5 Stair2.4 stair** was 'Agent #1148' at 1105.0 s  
Last agent to leave node **L5 Stair2.4 Landing** was 'Agent #1148' at 1061.0 s  
Last agent to leave node **L5 Stair2.3 Stair** was 'Agent #1149' at 1038.5 s  
Last agent to leave node **L5 Stair2.3 Landing** was 'Agent #1149' at 996.5 s  
Last agent to leave node **L5 Carpark** was 'Agent #1148' at 1050.5 s  
Last agent to leave node **L4 Stair2.4 Stair** was 'Agent #1148' at 1159.0 s  
Last agent to leave node **L4 Stair2.4 Landing** was 'Agent #1148' at 1115.5 s  
Last agent to leave node **L4 Stair2.3 Stair** was 'Agent #1149' at 1136.5 s  
Last agent to leave node **L4 Stair2.3 Landing** was 'Agent #1149' at 1095.0 s  
Last agent to leave node **L4 Carpark** was 'Agent #1040' at 508.5 s  
Last agent to leave node **L3 Stair2.4 Landing** was 'Agent #1148' at 1170.0 s  
Last agent to leave node **L3 Stair2.3 Stair** was 'Agent #1148' at 1213.5 s  
Last agent to leave node **L3 Stair2.3 Stair** was 'Agent #1149' at 1235.5 s  
Last agent to leave node **L3 Stair2.3 Landing** was 'Agent #1149' at 1194.5 s  
Last agent to leave node **L3 Carpark** was 'Agent #928' at 185.5 s  
Last agent to leave node **L2 Stair2.4 Stair** was 'Agent #1148' at 1266.5 s

Time for last person to leave the ground floor mall space.

Time for GF Anchor space to clear.

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EvacuationNZ model for:  
Non-base Case  
- Challenging Fire 1 (CF1)  
- Challenging Fire 2 (CF2)  
- Robustness Check (RC1)

Approved For Issue 27/02/2020

Last agent to leave node **L2 Stair2.4 Landing** was 'Agent #1148' at 1224.0 s  
Last agent to leave node **L2 Stair2.3 Stair** was 'Agent #1149' at 1333.5 s  
Last agent to leave node **L2 Stair2.3 Landing** was 'Agent #1149' at 1293.0 s  
Last agent to leave node **L2 Carpark** was 'Agent #813' at 201.0 s  
Last agent to leave node **L1 Stair4 Landing** was 'Agent #3' at 215.0 s  
Last agent to leave node **L1 Stair4** was 'Agent #3' at 226.0 s  
Last agent to leave node **L1 Stair3 Landing** was 'Agent #5' at 228.5 s  
Last agent to leave node **L1 Stair3** was 'Agent #5' at 240.0 s  
Last agent to leave node **L1 Stair2.4 Stair** was 'Agent #1148' at 1335.5 s  
Last agent to leave node **L1 Stair2.4 Landing** was 'Agent #1148' at 1277.0 s  
Last agent to leave node **L1 Stair2.3 Stair** was 'Agent #1149' at 1432.0 s  
Last agent to leave node **L1 Stair2.3 Landing** was 'Agent #1149' at 1390.5 s  
Last agent to leave node **L1 Carpark** was 'Agent #1' at 751.0 s  
Last agent to leave node **L1 Anchor-S BoH** was 'Agent #3' at 198.5 s  
Last agent to leave node **L1 Anchor** was 'Agent #1' at 243.0 s  
Last agent to leave node **L0 Stair4 landing** was 'Agent #3' at 231.5 s  
Last agent to leave node **L0 Stair3 Landing** was 'Agent #5' at 245.5 s  
Last agent to leave node **L0 Stair2.3 Landing** was 'Agent #1151' at 1449.5 s  
Last agent to leave node **Corridor** was 'Agent #1151' at 1496.0 s

Total number of agents in safe node **Mall- NW-HOS-Safe Place-Esk St** = 69  
Total number of agents in safe node **Mall- NW-F&B-Safe Place-Esk St** = 78  
Total number of agents in safe node **Mall-SW- Safe Place-Tay St** = 454  
Total number of agents in safe node **Mall- NW-Safe Place-Esk St** = 906  
Total number of agents in safe node **Mall-SE- Safe Place-Tay St** = 214  
Total number of agents in safe node **Mall- NE-Safe Place-Esk St** = 992  
Total number of agents in safe node **GF Anchor Safe Place-Tay St** = 161  
Total number of agents in safe node **GF Anchor Safe Place-Esk St** = 219  
Total number of agents in safe node **Safe Place-stair4** = 174  
Total number of agents in safe node **Safe Place-stair3** = 200  
Total number of agents in safe node **Safe Place-stair2.4** = 1050  
Total number of agents in safe node **Safe Place-stair2.3** = 1100

Total evacuation time = 1496.50 s

Completed at 10:51:21 on Monday 26 August 2019

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Time for last person to enter into stair 3 (i.e. time to clear the queue in front of stair 3).

Time for last person to enter into stair 4 (i.e. time to clear the queue in front of stair 4).

Time for last person from Level 1 anchor space to leave Stair 4.

Time for last person from Level 1 anchor space to leave Stair 3. This is the designated egress stair for the Childcare Centre on Level 2.

Time for L1 Anchor space to clear.

Time for last person to leave the car park building.



17 Dec 2019

Building Division

Invercargill City  
Council  
Building Consent  
Authority  
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EvacuationNZ model for:  
Non-base Case  
- Challenging Fire 3 (CF3) Childcare Fire  
Pre-movement time for GF and 1L anchor space = 60 sec

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**Person activity status**

Node type: Walkway, Stair, Pre-Fire Zone

Node weight: 300 g

Node color: 300 g (Red), 150 g (Yellow), 75 g (Green)

Node shape: 2 min (Square), 1 min (Circle)

**Agent density**

Agent number: 10 m<sup>2</sup> agent, 0.2 agents/m<sup>2</sup>

Agent color: Classroom (Blue), Classroom (Purple), Classroom (Orange), Classroom (Green), Classroom (Red), Classroom (Yellow)

Agent shape: Classroom (Square), Classroom (Circle), Classroom (Triangle), Classroom (Diamond), Classroom (Hexagon), Classroom (Octagon), Classroom (Star), Classroom (Cross), Classroom (Circle with cross), Classroom (Circle with dot), Classroom (Circle with horizontal line), Classroom (Circle with vertical line), Classroom (Circle with diagonal line), Classroom (Circle with X), Classroom (Circle with O), Classroom (Circle with I), Classroom (Circle with L), Classroom (Circle with T), Classroom (Circle with F), Classroom (Circle with H), Classroom (Circle with S), Classroom (Circle with B), Classroom (Circle with N), Classroom (Circle with E), Classroom (Circle with W), Classroom (Circle with C), Classroom (Circle with R), Classroom (Circle with A), Classroom (Circle with M), Classroom (Circle with D), Classroom (Circle with P), Classroom (Circle with Q), Classroom (Circle with Z)

**Doors and stairs**

Connection types: Required

Door widths: 0.6m, 0.7m, 0.8m, 0.9m, 1.0m, 1.1m, 1.2m, 1.3m, 1.4m, 1.5m, 1.6m, 1.7m, 1.8m, 1.9m, 2.0m, 2.1m, 2.2m, 2.3m, 2.4m, 2.5m, 2.6m, 2.7m, 2.8m, 2.9m, 3.0m, 3.1m, 3.2m, 3.3m, 3.4m, 3.5m, 3.6m, 3.7m, 3.8m, 3.9m, 4.0m, 4.1m, 4.2m, 4.3m, 4.4m, 4.5m, 4.6m, 4.7m, 4.8m, 4.9m, 5.0m

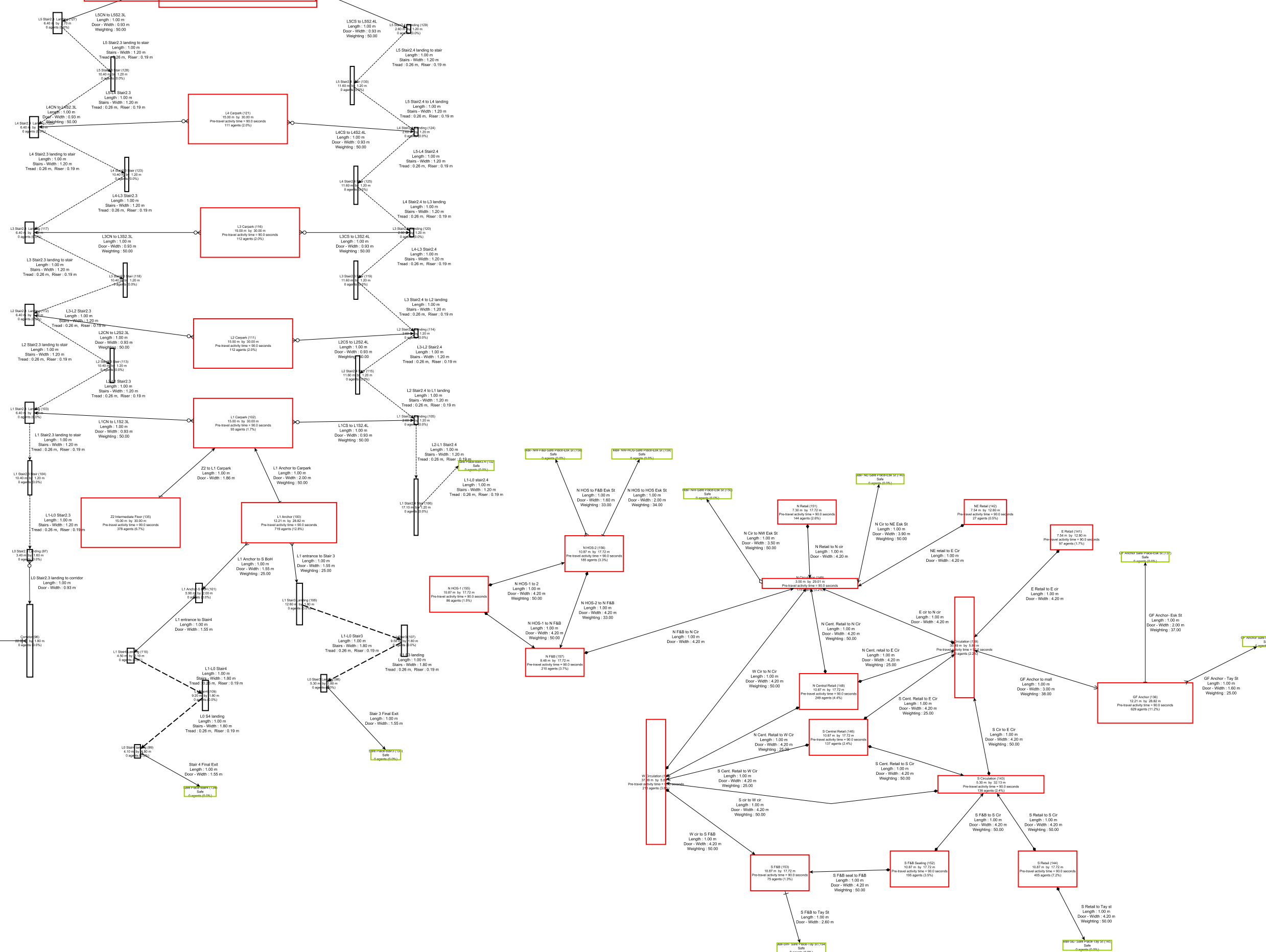
Stair types: T=0.26m R=0.19m, T=0.28m R=0.19m, T=0.31m R=0.17m

**Settings**

Diagram scale: 1:100 mm

Output frequency: 1 min

Output: CWI, Node output, Agent output



EvacuationNZ mode for  
Non-base Case  
- Challenge Time (Childcare Fire)  
Pre-movement time for GF and 1L anchor space = 60 sec

### EvacuationNZ

Michael Spearpoint  
University of Canterbury  
version 2.11 - Holmes Fire release (Sep 19 2016)

*This software version is exclusively licensed to Holmes Fire Ltd and is not to be used by any other party.*

### Contents

- [Nodes](#)
- [Connections](#)
- [Population](#)
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### Nodes

Node **Mall- NW-HOS-Safe Place-Esk St** - Safe  
Connections : [N HOS to HOS Esk St](#),

Node **Mall- NW-F&B-Safe Place-Esk St** - Safe  
Connections : [N HOS to F&B Esk St](#),

Node **N F&B**  
Dimensions 8.48 m by 17.72 m  
Connections : [N F&B to N Cir](#), [N HOS-2 to N F&B](#), [N HOS-1 to N F&B](#),

Node **N HOS-2**  
Dimensions 10.87 m by 17.72 m  
Connections : [N HOS-2 to N F&B](#), [N HOS to HOS Esk St](#), [N HOS to F&B Esk St](#), [N HOS-1 to 2](#),

Node **N HOS-1**  
Dimensions 10.87 m by 17.72 m  
Connections : [N HOS-1 to N F&B](#), [N HOS-1 to 2](#),

Node **Mall-SW- Safe Place-Tay St** - Safe  
Connections : [S F&B to Tay St](#),

Node **S F&B**  
Dimensions 10.87 m by 17.72 m  
Connections : [W cir to S F&B](#), [S F&B seat to F&B](#), [S F&B to Tay St](#),

Node **S F&B Seating**  
Dimensions 10.87 m by 17.72 m  
Connections : [S F&B to S Cir](#), [S F&B seat to F&B](#),

Node **N Retail**  
Dimensions 7.30 m by 17.72 m  
Connections : [N Retail to N cir](#),

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Node **Mall- NW-Safe Place-Esk St** - Safe  
Connections : [N Cir to NW Esk St](#),

Node **N Circulation**  
Dimensions 3.00 m by 29.01 m  
Connections : [E cir to N cir](#), [N F&B to N Cir](#), [W Cir to N Cir](#), [N Retail to N cir](#), [N Cir to NW Esk St](#), [N Cent. Retail to N Cir](#), [NE retail to E Cir](#), [N Cir to NE Esk St](#),

Node **N Central Retail**  
Dimensions 10.87 m by 17.72 m  
Connections : [N Cent. Retail to W Cir](#), [N Cent. retail to E Cir](#), [N Cent. Retail to N Cir](#),

Node **W Circulation**  
Dimensions 37.89 m by 5.86 m  
Connections : [S cir to W cir](#), [W cir to S F&B](#), [W Cir to N Cir](#), [N Cent. Retail to W Cir](#), [S Cent. Retail to W Cir](#),

Node **S Central Retail**  
Dimensions 10.87 m by 17.72 m  
Connections : [S Cent. Retail to W Cir](#), [S Cent. Retail to E Cir](#), [S Cent. Retail to S Cir](#),

Node **Mall-SE- Safe Place-Tay St** - Safe  
Connections : [S Retail to Tay st](#),

Node **S Retail**  
Dimensions 10.87 m by 17.72 m  
Connections : [S Retail to Tay st](#), [S Retail to S Cir](#),

Node **S Circulation**  
Dimensions 5.30 m by 32.13 m  
Connections : [S cir to W cir](#), [S F&B to S Cir](#), [S Cent. Retail to S Cir](#), [S Retail to S Cir](#), [S Cir to E Cir](#),

Node **NE Retail**  
Dimensions 7.54 m by 12.80 m  
Connections : [NE retail to E Cir](#),

Node **E Retail**  
Dimensions 7.54 m by 12.80 m  
Connections : [E Retail to E cir](#),

Node **Mall- NE-Safe Place-Esk St** - Safe  
Connections : [N Cir to NE Esk St](#),

Node **E Circulation**  
Dimensions 30.49 m by 5.86 m  
Connections : [E cir to N cir](#), [N Cent. retail to E Cir](#), [S Cent. Retail to E Cir](#), [S Cir to E Cir](#), [E Retail to E cir](#), [GF Anchor to mall](#),

Node **GF Anchor Safe Place-Tay St** - Safe  
Connections : [GF Anchor - Tay St](#),

Node **GF Anchor Safe Place-Esk St** - Safe  
Connections : [GF Anchor- Esk St](#),

Node **GF Anchor**  
Dimensions 12.21 m by 28.82 m  
Connections : [GF Anchor to mall](#), [GF Anchor - Tay St](#), [GF Anchor- Esk St](#),

Invercargill City Council  
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Evacuation mode for Non-base Case  
- Challenge time for Childcare Fire  
Pre-movement time for GF and 1L anchor space = 60 sec

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Node **Z2 Intermediate Floor**  
17 Dec 2019 15.00 m by 30.00 m  
Connections : [Z2 to L1 Carpark](#),

Building Division  
Node **Safe Place-stair4** - Safe  
Connections : [Stair 4 Final Exit](#),

Node **Safe Place-stair3** - Safe  
Connections : [Stair 3 Final Exit](#),

Node **Safe Place-stair2.4** - Safe  
Connections : [L1-L0 stair2.4](#),

Node **Safe Place-stair2.3** - Safe  
Connections : [Stair 2.3 Final Exit](#),

Node **L5 Stair2.4 stair**  
Dimensions 11.60 m by 1.20 m  
Connections : [L5 Stair2.4 landing to stair](#), [L5 Stair2.4 to L4 landing](#),

Node **L5 Stair2.4 Landing**  
Dimensions 2.60 m by 1.20 m  
Connections : [L5 Stair2.4 landing to stair](#), [L5CS to L5S2.4L](#),

Node **L5 Stair2.3 Stair**  
Dimensions 10.40 m by 1.20 m  
Connections : [L5 Stair2.3 landing to stair](#), [L5-L4 Stair2.3](#),

Node **L5 Stair2.3 Landing**  
Dimensions 6.40 m by 2.70 m  
Connections : [L5 Stair2.3 landing to stair](#), [L5CN to L5S2.3L](#),

Node **L5 Carpark**  
Dimensions 30.00 m by 47.80 m  
Connections : [L5CN to L5S2.3L](#), [L5CS to L5S2.4L](#),

Node **L4 Stair2.4 Stair**  
Dimensions 11.60 m by 1.20 m  
Connections : [L5-L4 Stair2.4](#), [L4 Stair2.4 to L3 landing](#),

Node **L4 Stair2.4 Landing**  
Dimensions 2.60 m by 1.20 m  
Connections : [L5-L4 Stair2.4](#), [L4CS to L4S2.4L](#), [L5 Stair2.4 to L4 landing](#),

Node **L4 Stair2.3 Stair**  
Dimensions 10.40 m by 1.20 m  
Connections : [L4 Stair2.3 landing to stair](#), [L4-L3 Stair2.3](#),

Node **L4 Stair2.3 Landing**  
Dimensions 6.40 m by 2.70 m  
Connections : [L4 Stair2.3 landing to stair](#), [L4CN to L4S2.3L](#), [L5-L4 Stair2.3](#),

Node **L4 Carpark**  
Dimensions 15.00 m by 30.00 m  
Connections : [L4CN to L4S2.3L](#), [L4CS to L4S2.4L](#),

Node **L3 Stair2.4 Landing**  
Dimensions 2.60 m by 1.20 m

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Connections : [L4-L3 Stair2.4](#), [L3CS to L3S2.4L](#), [L4 Stair2.4 to L3 landing](#),

Node **L3 Stair2.3 Stair**  
Dimensions 11.60 m by 1.20 m  
Connections : [L4-L3 Stair2.4](#), [L3 Stair2.4 to L2 landing](#),

Node **L3 Stair2.3 Stair**  
Dimensions 10.40 m by 1.20 m  
Connections : [L3 Stair2.3 landing to stair](#), [L3-L2 Stair2.3](#),

Node **L3 Stair2.3 Landing**  
Dimensions 6.40 m by 2.70 m  
Connections : [L3 Stair2.3 landing to stair](#), [L3CN to L3S2.3L](#), [L4-L3 Stair2.3](#),

Node **L3 Carpark**  
Dimensions 15.00 m by 30.00 m  
Connections : [L3CS to L3S2.4L](#), [L3CN to L3S2.3L](#),

Node **L2 Stair2.4 Stair**  
Dimensions 11.60 m by 1.20 m  
Connections : [L3-L2 Stair2.4](#), [L2 Stair2.4 to L1 landing](#),

Node **L2 Stair2.4 Landing**  
Dimensions 2.60 m by 1.20 m  
Connections : [L3-L2 Stair2.4](#), [L2CS to L2S2.4L](#), [L3 Stair2.4 to L2 landing](#),

Node **L2 Stair2.3 Stair**  
Dimensions 10.40 m by 1.20 m  
Connections : [L2 Stair2.3 landing to stair](#), [L2-L1 Stair2.3](#),

Node **L2 Stair2.3 Landing**  
Dimensions 6.40 m by 2.70 m  
Connections : [L2 Stair2.3 landing to stair](#), [L2CN to L2S2.3L](#), [L3-L2 Stair2.3](#),

Node **L2 Carpark**  
Dimensions 15.00 m by 30.00 m  
Connections : [L2CS to L2S2.4L](#), [L2CN to L2S2.3L](#),

Node **L1 Stair4 Landing**  
Dimensions 4.50 m by 2.10 m  
Connections : [L1-L0 Stair4](#), [L1 entrance to Stair4](#),

Node **L1 Stair4**  
Dimensions 9.20 m by 1.80 m  
Connections : [L0 S4 landing](#), [L1-L0 Stair4](#),

Node **L1 Stair3 Landing**  
Dimensions 12.60 m by 1.80 m  
Connections : [L1 entrance to Stair 3](#), [L1-L0 Stair3](#),

Node **L1 Stair3**  
Dimensions 9.50 m by 1.80 m  
Connections : [L1 S3 landing](#), [L1-L0 Stair3](#),

Node **L1 Stair2.4 Stair**  
Dimensions 17.10 m by 1.20 m  
Connections : [L2-L1 Stair2.4](#), [L1-L0 stair2.4](#),

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EvacuationNZ model for:  
- Base Case  
- Challenging Fire 3 (CF3) Childcare Fire  
Pre-movement time for GF and 1L  
and 1R space = 60 sec

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Node **L1 Stair2.4 Landing**  
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Dimensions 1.60 m by 1.20 m

Connections : [L2-L1 Stair2.4](#), [L1CS to L1S2.4L](#), [L2 Stair2.4 to L1 landing](#),

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Node **L1 Stair2.3 Stair**

Dimensions 10.40 m by 1.20 m

Connections : [L1 Stair2.3 landing to stair](#), [L1-L0 Stair2.3](#),

Node **L1 Stair2.3 Landing**

Dimensions 6.40 m by 2.70 m

Connections : [L1 Stair2.3 landing to stair](#), [L1CN to L1S2.3L](#), [L2-L1 Stair2.3](#),

Node **L1 Carpark**

Dimensions 15.00 m by 30.00 m

Connections : [Z2 to L1 Carpark](#), [L1 Anchor to Carpark](#), [L1CS to L1S2.4L](#), [L1CN to L1S2.3L](#),

Node **L1 Anchor-S BoH**

Dimensions 5.90 m by 2.00 m

Connections : [L1 Anchor to S BoH](#), [L1 entrance to Stair4](#),

Node **L1 Anchor**

Dimensions 12.21 m by 28.82 m

Connections : [L1 entrance to Stair 3](#), [L1 Anchor to S BoH](#), [L1 Anchor to Carpark](#),

Node **L0 Stair4 landing**

Dimensions 4.10 m by 1.80 m

Connections : [Stair 4 Final Exit](#), [L0 S4 landing](#),

Node **L0 Stair3 Landing**

Dimensions 5.30 m by 1.80 m

Connections : [Stair 3 Final Exit](#), [L1 S3 landing](#),

Node **L0 Stair2.3 Landing**

Dimensions 3.40 m by 1.60 m

Connections : [L1-L0 Stair2.3](#), [L0 Stair2.3 landing to corridor](#),

Node **Corridor**

Dimensions 22.00 m by 1.80 m

Connections : [Stair 2.3 Final Exit](#), [L0 Stair2.3 landing to corridor](#),

### Connections

Connection **L0 Stair2.3 landing to corridor**

Length 1.00 m

Connecting [L0 Stair2.3 Landing](#) to [Corridor](#) (target node for required path)

Door width 0.93 m, specific flow 1.33 persons/s per m eff. width

Connection **Stair 2.3 Final Exit**

Length 1.00 m

Connecting [Corridor](#) to [Safe Place-stair2.3](#) (target node for required path)

Door width 0.93 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)

Connection **L1-L0 stair2.4**

Length 1.00 m

Connecting [L1 Stair2.4 Stair](#) to [Safe Place-stair2.4](#) (target node for required path)

Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

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Connection **L2 Stair2.4 to L1 landing**

Length 1.00 m

Connecting [L2 Stair2.4 Stair](#) to [L1 Stair2.4 Landing](#) (target node for required path)

Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L3 Stair2.4 to L2 landing**

Length 1.00 m

Connecting [L3 Stair2.3 Stair](#) to [L2 Stair2.4 Landing](#) (target node for required path)

Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L4 Stair2.4 to L3 landing**

Length 1.00 m

Connecting [L4 Stair2.4 Stair](#) to [L3 Stair2.4 Landing](#) (target node for required path)

Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L5 Stair2.4 to L4 landing**

Length 1.00 m

Connecting [L5 Stair2.4 stair](#) to [L4 Stair2.4 Landing](#) (target node for required path)

Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L1-L0 Stair2.3**

Length 1.00 m

Connecting [L1 Stair2.3 Stair](#) to [L0 Stair2.3 Landing](#) (target node for required path)

Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L2-L1 Stair2.3**

Length 1.00 m

Connecting [L2 Stair2.3 Stair](#) to [L1 Stair2.3 Landing](#) (target node for required path)

Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L3-L2 Stair2.3**

Length 1.00 m

Connecting [L3 Stair2.3 Stair](#) to [L2 Stair2.3 Landing](#) (target node for required path)

Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L4-L3 Stair2.3**

Length 1.00 m

Connecting [L4 Stair2.3 Stair](#) to [L3 Stair2.3 Landing](#) (target node for required path)

Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L5CS to L5S2.4L**

Length 1.00 m

Connecting [L5 Carpark](#) to [L5 Stair2.4 Landing](#) (target node for required path)

Door width 0.93 m, specific flow 1.33 persons/s per m eff. width

Connection **L5CN to L5S2.3L**

Length 1.00 m

Connecting [L5 Carpark](#) to [L5 Stair2.3 Landing](#) (target node for required path)

Door width 0.93 m, specific flow 1.33 persons/s per m eff. width

Connection **L5-L4 Stair2.3**

Length 1.00 m

Connecting [L5 Stair2.3 Stair](#) to [L4 Stair2.3 Landing](#) (target node for required path)

Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L1CN to L1S2.3L**

Length 1.00 m

Connecting [L1 Carpark](#) to [L1 Stair2.3 Landing](#) (target node for required path)

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Door width 0.93 m, specific flow 1.33 persons/s per m eff. width  
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Connection **L1CS to L1S2.4L**

Length 1.00 m  
Connecting [L1 Carpark](#) to [L1 Stair2.4 Landing](#) (target node for required path)  
Door width 0.93 m, specific flow 1.33 persons/s per m eff. width

Connection **L2CN to L2S2.3L**

Length 1.00 m  
Connecting [L2 Carpark](#) to [L2 Stair2.3 Landing](#) (target node for required path)  
Door width 0.93 m, specific flow 1.33 persons/s per m eff. width

Connection **L2CS to L2S2.4L**

Length 1.00 m  
Connecting [L2 Carpark](#) to [L2 Stair2.4 Landing](#) (target node for required path)  
Door width 0.93 m, specific flow 1.33 persons/s per m eff. width

Connection **L3CN to L3S2.3L**

Length 1.00 m  
Connecting [L3 Carpark](#) to [L3 Stair2.3 Landing](#) (target node for required path)  
Door width 0.93 m, specific flow 1.33 persons/s per m eff. width

Connection **L3CS to L3S2.4L**

Length 1.00 m  
Connecting [L3 Carpark](#) to [L3 Stair2.4 Landing](#) (target node for required path)  
Door width 0.93 m, specific flow 1.33 persons/s per m eff. width

Connection **L4CS to L4S2.4L**

Length 1.00 m  
Connecting [L4 Carpark](#) to [L4 Stair2.4 Landing](#) (target node for required path)  
Door width 0.93 m, specific flow 1.33 persons/s per m eff. width

Connection **L4CN to L4S2.3L**

Length 1.00 m  
Connecting [L4 Carpark](#) to [L4 Stair2.3 Landing](#) (target node for required path)  
Door width 0.93 m, specific flow 1.33 persons/s per m eff. width

Connection **L5 Stair2.4 landing to stair**

Length 1.00 m  
Connecting [L5 Stair2.4 Landing](#) to [L5 Stair2.4 stair](#) (target node for required path)  
Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L5-L4 Stair2.4**

Length 1.00 m  
Connecting [L4 Stair2.4 Landing](#) to [L4 Stair2.4 Stair](#) (target node for required path)  
Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L4-L3 Stair2.4**

Length 1.00 m  
Connecting [L3 Stair2.4 Landing](#) to [L3 Stair2.3 Stair](#) (target node for required path)  
Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L3-L2 Stair2.4**

Length 1.00 m  
Connecting [L2 Stair2.4 Landing](#) to [L2 Stair2.4 Stair](#) (target node for required path)  
Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L2-L1 Stair2.4**

EvacuationNZ model for:  
Non-base Case  
- Challenging Fire 3 (CF3)  
Childcare Fire  
Fire-movement time for GF and  
1L anchor space = 60 sec

Length 1.00 m  
Connecting [L1 Stair2.4 Landing](#) to [L1 Stair2.4 Stair](#) (target node for required path)  
Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L5 Stair2.3 landing to stair**

Length 1.00 m  
Connecting [L5 Stair2.3 Landing](#) to [L5 Stair2.3 Stair](#) (target node for required path)  
Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L4 Stair2.3 landing to stair**

Length 1.00 m  
Connecting [L4 Stair2.3 Landing](#) to [L4 Stair2.3 Stair](#) (target node for required path)  
Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L3 Stair2.3 landing to stair**

Length 1.00 m  
Connecting [L3 Stair2.3 Landing](#) to [L3 Stair2.3 Stair](#) (target node for required path)  
Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L2 Stair2.3 landing to stair**

Length 1.00 m  
Connecting [L2 Stair2.3 Landing](#) to [L2 Stair2.3 Stair](#) (target node for required path)  
Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L1 Stair2.3 landing to stair**

Length 1.00 m  
Connecting [L1 Stair2.3 Landing](#) to [L1 Stair2.3 Stair](#) (target node for required path)  
Stairs width 1.20 m, tread 0.26 m, riser 0.19 m

Connection **L1-L0 Stair3**

Length 1.00 m  
Connecting [L1 Stair3 Landing](#) to [L1 Stair3](#) (target node for required path)  
Stairs width 1.80 m, tread 0.26 m, riser 0.19 m

Connection **L1 S3 landing**

Length 1.00 m  
Connecting [L1 Stair3](#) to [L0 Stair3 Landing](#) (target node for required path)  
Stairs width 1.80 m, tread 0.26 m, riser 0.19 m

Connection **L1 entrance to Stair4**

Length 1.00 m  
Connecting [L1 Anchor-S BoH](#) to [L1 Stair4 Landing](#) (target node for required path)  
Door width 1.55 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)

Connection **L1-L0 Stair4**

Length 1.00 m  
Connecting [L1 Stair4 Landing](#) to [L1 Stair4](#) (target node for required path)  
Stairs width 1.80 m, tread 0.26 m, riser 0.19 m

Connection **L0 S4 landing**

Length 1.00 m  
Connecting [L1 Stair4](#) to [L0 Stair4 landing](#) (target node for required path)  
Stairs width 1.80 m, tread 0.26 m, riser 0.19 m

Connection **Stair 4 Final Exit**

Length 1.00 m  
Connecting [L0 Stair4 landing](#) to [Safe Place-stair4](#) (target node for required path)  
Door width 1.55 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)

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EvacuationNZ model for:  
Non-base Case  
- Challenging Fire 3 (CF3)  
Childcare Fire  
Pre-movement time for GF  
and 1L anchor space = 60 sec

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Connection **Stair 3 Final Exit**  
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Connecting [L0 Stair3 Landing](#) to [Safe Place-stair3](#) (target node for required path)  
Door width 1.55 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)

Connection **L1 Anchor to Carpark**  
Length 1.00 m  
Connecting [L1 Anchor](#) to [L1 Carpark](#) (target node for required path)  
Door width 2.00 m, specific flow 1.33 persons/s per m eff. width

Connection **Z2 to L1 Carpark**  
Length 1.00 m  
Connecting [Z2 Intermediate Floor](#) to [L1 Carpark](#) (target node for required path)  
Door width 1.86 m, specific flow 1.33 persons/s per m eff. width

Connection **L1 Anchor to S BoH**  
Length 1.00 m  
Connecting [L1 Anchor](#) to [L1 Anchor-S BoH](#) (target node for required path)  
Door width 1.55 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)

Connection **L1 entrance to Stair 3**  
Length 1.00 m  
Connecting [L1 Anchor](#) to [L1 Stair3 Landing](#) (target node for required path)  
Door width 1.55 m, specific flow 1.33 persons/s per m eff. width (restricted by closer)

Connection **GF Anchor- Esk St**  
Length 1.00 m  
Connecting [GF Anchor](#) to [GF Anchor Safe Place-Esk St](#) (target node for required path)  
Door width 2.00 m, specific flow 1.33 persons/s per m eff. width

Connection **GF Anchor - Tay St**  
Length 1.00 m  
Connecting [GF Anchor](#) to [GF Anchor Safe Place-Tay St](#) (target node for required path)  
Door width 1.60 m, specific flow 1.33 persons/s per m eff. width

Connection **GF Anchor to mall**  
Length 1.00 m  
Connecting [GF Anchor](#) to [E Circulation](#) (target node for required path)  
Door width 3.00 m, specific flow 1.33 persons/s per m eff. width

Connection **N Cir to NE Esk St**  
Length 1.00 m  
Connecting [N Circulation](#) to [Mall- NE-Safe Place-Esk St](#) (target node for required path)  
Door width 3.90 m, specific flow 1.33 persons/s per m eff. width

Connection **NE retail to E Cir**  
Length 1.00 m  
Connecting [NE Retail](#) to [N Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **E Retail to E cir**  
Length 1.00 m  
Connecting [E Retail](#) to [E Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **S Cir to E Cir**  
Length 1.00 m  
Connecting [S Circulation](#) to [E Circulation](#) (target node for required path)

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Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **S Retail to S Cir**  
Length 1.00 m  
Connecting [S Retail](#) to [S Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **S Retail to Tay st**  
Length 1.00 m  
Connecting [S Retail](#) to [Mall-SE- Safe Place-Tay St](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **S Cent. Retail to S Cir**  
Length 1.00 m  
Connecting [S Central Retail](#) to [S Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **S Cent. Retail to E Cir**  
Length 1.00 m  
Connecting [S Central Retail](#) to [E Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **S Cent. Retail to W Cir**  
Length 1.00 m  
Connecting [S Central Retail](#) to [W Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **N Cent. Retail to N Cir**  
Length 1.00 m  
Connecting [N Central Retail](#) to [N Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **N Cent. retail to E Cir**  
Length 1.00 m  
Connecting [N Central Retail](#) to [E Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **N Cent. Retail to W Cir**  
Length 1.00 m  
Connecting [N Central Retail](#) to [W Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **N Cir to NW Esk St**  
Length 1.00 m  
Connecting [N Circulation](#) to [Mall- NW-Safe Place-Esk St](#) (target node for required path)  
Door width 3.50 m, specific flow 1.33 persons/s per m eff. width

Connection **N Retail to N cir**  
Length 1.00 m  
Connecting [N Retail](#) to [N Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **W Cir to N Cir**  
Length 1.00 m  
Connecting [W Circulation](#) to [N Circulation](#) (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

Connection **S F&B to Tay St**

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Length 1.00 m  
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Door width 2.60 m, specific flow 1.33 persons/s

EvacuationNZ mode for Non-base Case  
- Challenge (see Appendix Childcare Fire)  
Pre-movement time for GF and 1L anchor space = 60 sec

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**Connection S F&B seat to F&B**

Length 1.00 m  
Connecting S F&B Seating to S F&B (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

**Connection S F&B to S Cir**

Length 1.00 m  
Connecting S F&B Seating to S Circulation (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

**Connection W cir to S F&B**

Length 1.00 m  
Connecting W Circulation to S F&B (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

**Connection N HOS-1 to 2**

Length 1.00 m  
Connecting N HOS-1 to N HOS-2 (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

**Connection N HOS-1 to N F&B**

Length 1.00 m  
Connecting N HOS-1 to N F&B (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

**Connection N HOS to F&B Esk St**

Length 1.00 m  
Connecting N HOS-2 to Mall- NW-F&B-Safe Place-Esk St (target node for required path)  
Door width 1.60 m, specific flow 1.33 persons/s per m eff. width

**Connection N HOS to HOS Esk St**

Length 1.00 m  
Connecting N HOS-2 to Mall- NW-HOS-Safe Place-Esk St (target node for required path)  
Door width 2.00 m, specific flow 1.33 persons/s per m eff. width

**Connection N HOS-2 to N F&B**

Length 1.00 m  
Connecting N HOS-2 to N F&B (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

**Connection N F&B to N Cir**

Length 1.00 m  
Connecting N F&B to N Circulation (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

**Connection S cir to W cir**

Length 1.00 m  
Connecting S Circulation to W Circulation (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

**Connection E cir to N cir**

Length 1.00 m  
Connecting E Circulation to N Circulation (target node for required path)  
Door width 4.20 m, specific flow 1.33 persons/s per m eff. width

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**Population**

Name	Number	Density (agents/m <sup>2</sup> )	Density (m <sup>2</sup> /agent)
<a href="#">L1 Anchor</a>	719	2.04	0.49
<a href="#">L1 Carpark</a>	93	0.21	4.84
<a href="#">L2 Carpark</a>	112	0.25	4.02
<a href="#">L3 Carpark</a>	112	0.25	4.02
<a href="#">L4 Carpark</a>	111	0.25	4.05
<a href="#">L5 Carpark</a>	999	0.70	1.44
<a href="#">Z2 Intermediate Floor</a>	378	0.84	1.19
<a href="#">GF Anchor</a>	629	1.79	0.56
<a href="#">E Circulation</a>	123	0.69	1.45
<a href="#">E Retail</a>	97	1.01	0.99
<a href="#">NE Retail</a>	27	0.28	3.57
<a href="#">S Circulation</a>	136	0.80	1.25
<a href="#">S Retail</a>	405	2.10	0.48
<a href="#">S Central Retail</a>	137	0.71	1.41
<a href="#">W Circulation</a>	216	0.97	1.03
<a href="#">N Central Retail</a>	249	1.29	0.77
<a href="#">N Circulation</a>	179	2.06	0.49
<a href="#">N Retail</a>	144	1.11	0.90
<a href="#">S F&amp;B Seating</a>	195	1.01	0.99
<a href="#">S F&amp;B</a>	75	0.39	2.57
<a href="#">N HOS-1</a>	86	0.45	2.24
<a href="#">N HOS-2</a>	185	0.96	1.04
<a href="#">N F&amp;B</a>	210	1.40	0.72

**Results**

Simulation run 1 : Total number of agents = 5617

- Node [N HOS-1](#) clear at 98.5 s
- Node [S Central Retail](#) clear at 103.5 s
- Node [E Retail](#) clear at 109.0 s
- Node [S F&B Seating](#) clear at 109.5 s
- Node [N Central Retail](#) clear at 120.0 s

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- Node [S Retail](#) clear at 132.0 s
- Node [N HOS-2](#) clear at 135.5 s
- Node [NE Retail](#) clear at 138.0 s
- Node [S Circulation](#) clear at 178.5 s
- Node [L3 Carpark](#) clear at 185.5 s
- Node [GF Anchor](#) clear at 187.5 s
- Node [L2 Carpark](#) clear at 201.0 s
- Node [N F&B](#) clear at 223.0 s
- Node [W Circulation](#) clear at 229.0 s
- Node [N Retail](#) clear at 240.0 s
- Node [S F&B](#) clear at 241.0 s
- Node [L1 Anchor](#) clear at 243.0 s
- Node [Z2 Intermediate Floor](#) clear at 272.5 s
- Node [E Circulation](#) clear at 277.5 s
- Node [N Circulation](#) clear at 321.0 s
- Node [L4 Carpark](#) clear at 506.0 s
- Node [L1 Carpark](#) clear at 802.0 s
- Node [L5 Carpark](#) clear at 1049.5 s

Time for last person to leave the ground floor mall space.

- Last agent to leave node [N F&B](#) was 'Agent #5138' at 223.0 s
- Last agent to leave node [N HOS-2](#) was 'Agent #5148' at 135.5 s
- Last agent to leave node [N HOS-1](#) was 'Agent #5137' at 98.5 s
- Last agent to leave node [S F&B](#) was 'Agent #3538' at 241.0 s
- Last agent to leave node [S F&B Seating](#) was 'Agent #4867' at 109.5 s
- Last agent to leave node [N Retail](#) was 'Agent #4723' at 240.0 s
- Last agent to leave node [N Circulation](#) was 'Agent #3544' at 321.0 s
- Last agent to leave node [N Central Retail](#) was 'Agent #4296' at 120.0 s
- Last agent to leave node [W Circulation](#) was 'Agent #4871' at 229.0 s
- Last agent to leave node [S Central Retail](#) was 'Agent #3943' at 103.5 s
- Last agent to leave node [S Retail](#) was 'Agent #3539' at 132.0 s
- Last agent to leave node [S Circulation](#) was 'Agent #3537' at 178.5 s
- Last agent to leave node [NE Retail](#) was 'Agent #3374' at 138.0 s
- Last agent to leave node [E Retail](#) was 'Agent #3277' at 109.0 s
- Last agent to leave node [E Circulation](#) was 'Agent #3537' at 277.5 s
- Last agent to leave node [GF Anchor](#) was 'Agent #2525' at 187.5 s
- Last agent to leave node [Z2 Intermediate Floor](#) was 'Agent #2147' at 272.5 s
- Last agent to leave node [L5 Stair2.4 Stair](#) was 'Agent #1148' at 1103.5 s
- Last agent to leave node [L5 Stair2.4 Landing](#) was 'Agent #1148' at 1060.0 s
- Last agent to leave node [L5 Stair2.3 Stair](#) was 'Agent #1149' at 1033.0 s
- Last agent to leave node [L5 Stair2.3 Landing](#) was 'Agent #1149' at 992.5 s
- Last agent to leave node [L5 Carpark](#) was 'Agent #1148' at 1049.5 s
- Last agent to leave node [L4 Stair2.4 Stair](#) was 'Agent #1148' at 1158.5 s
- Last agent to leave node [L4 Stair2.4 Landing](#) was 'Agent #1148' at 1114.5 s
- Last agent to leave node [L4 Stair2.3 Stair](#) was 'Agent #1149' at 1132.0 s
- Last agent to leave node [L4 Stair2.3 Landing](#) was 'Agent #1149' at 1091.0 s
- Last agent to leave node [L4 Carpark](#) was 'Agent #1040' at 506.0 s
- Last agent to leave node [L3 Stair2.4 Landing](#) was 'Agent #1148' at 1169.0 s
- Last agent to leave node [L3 Stair2.3 Stair](#) was 'Agent #1148' at 1212.5 s
- Last agent to leave node [L3 Stair2.3 Stair](#) was 'Agent #1149' at 1232.0 s
- Last agent to leave node [L3 Stair2.3 Landing](#) was 'Agent #1149' at 1190.5 s
- Last agent to leave node [L3 Carpark](#) was 'Agent #928' at 185.5 s
- Last agent to leave node [L2 Stair2.4 Stair](#) was 'Agent #1148' at 1266.5 s

Time for GF Anchor space to clear.

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- Last agent to leave node [L2 Stair2.4 Landing](#) was 'Agent #1148' at 1223.0 s
- Last agent to leave node [L2 Stair2.3 Stair](#) was 'Agent #1149' at 1328.5 s
- Last agent to leave node [L2 Stair2.3 Landing](#) was 'Agent #1149' at 1289.0 s
- Last agent to leave node [L2 Carpark](#) was 'Agent #813' at 201.0 s
- Last agent to leave node [L1 Stair4 Landing](#) was 'Agent #3' at 215.0 s
- Last agent to leave node [L1 Stair4](#) was 'Agent #3' at 226.0 s
- Last agent to leave node [L1 Stair3 Landing](#) was 'Agent #5' at 228.5 s
- Last agent to leave node [L1 Stair3](#) was 'Agent #5' at 240.0 s
- Last agent to leave node [L1 Stair2.4 Stair](#) was 'Agent #1148' at 1338.0 s
- Last agent to leave node [L1 Stair2.4 Landing](#) was 'Agent #1148' at 1276.0 s
- Last agent to leave node [L1 Stair2.3 Stair](#) was 'Agent #1149' at 1427.0 s
- Last agent to leave node [L1 Stair2.3 Landing](#) was 'Agent #1149' at 1387.5 s
- Last agent to leave node [L1 Carpark](#) was 'Agent #2148' at 802.0 s
- Last agent to leave node [L1 Anchor-S BoH](#) was 'Agent #3' at 198.5 s
- Last agent to leave node [L1 Anchor](#) was 'Agent #1' at 243.0 s
- Last agent to leave node [L0 Stair4 landing](#) was 'Agent #3' at 231.5 s
- Last agent to leave node [L0 Stair3 Landing](#) was 'Agent #5' at 245.5 s
- Last agent to leave node [L0 Stair2.3 Landing](#) was 'Agent #1149' at 1444.5 s
- Last agent to leave node [Corridor](#) was 'Agent #1149' at 1491.5 s

Time for last person to enter into stair 3 (i.e. time to clear the queue in front of stair 3).

Time for last person to enter into stair 4 (i.e. time to clear the queue in front of stair 4).

Time for last person from Level 1 anchor space to leave Stair 4.

Time for last person from Level 1 anchor space to leave Stair 3. This is the designated egress stair for the Childcare Centre on Level 2.

- Total number of agents in safe node [Mall- NW-HOS-Safe Place-Esk St](#) = 75
- Total number of agents in safe node [Mall- NW-F&B-Safe Place-Esk St](#) = 77
- Total number of agents in safe node [Mall-SW- Safe Place-Tay St](#) = 458
- Total number of agents in safe node [Mall- NW-Safe Place-Esk St](#) = 962
- Total number of agents in safe node [Mall-SE- Safe Place-Tay St](#) = 214
- Total number of agents in safe node [Mall- NE-Safe Place-Esk St](#) = 927
- Total number of agents in safe node [GF Anchor Safe Place-Tay St](#) = 161
- Total number of agents in safe node [GF Anchor Safe Place-Esk St](#) = 219
- Total number of agents in safe node [Safe Place-stair4](#) = 174
- Total number of agents in safe node [Safe Place-stair3](#) = 200
- Total number of agents in safe node [Safe Place-stair2.4](#) = 1055
- Total number of agents in safe node [Safe Place-stair2.3](#) = 1095

Total evacuation time = 1492.00 s

Time for L1 Anchor space to clear.

Time for last person to leave the car park building.



## B.5 Hand-calculation Validation of EvacuatioNZ

To validate the presented EvacuatioNZ results, hand-calculation of travel / flow times is undertaken for key areas. Hand-calculations are undertaken as per V/VM2, section 3.2.5.

EvacuatioNZ results from Base case evacuation are utilised in comparison.

Table 14 - Hand-calculation Validation

Location	Total Occupancy Using Egress (ppl)	Hand-calculation			EvacuatioNZ RSET (s)
		Travel Time (s)	Flow Time (s)	RSET (s)	
GF Anchor	629	36	84	144 <sup>1</sup>	168 <sup>1</sup>
L1 Anchor	719	52	142	232 <sup>2</sup>	241 <sup>2</sup>

Explanatory notes:

- 1) The RSET time did not include smoke detection time but does include  $t_n$  (30s) and  $t_{pre}$  (30s).
- 2) The RSET time did not include smoke detection time but does include  $t_n$  (30s) and  $t_{pre}$  (60s).

The RSET times (excluding the smoke detection time) are generally similar between EvacuatioNZ results and hand-calculations. The minor difference may be due to occupant interaction leading to queuing and as such reducing flow through various bottle-necks.

It is considered that the derived EvacuatioNZ modelling results are supported by crude overall building evacuation estimates by hand calculations.

It is also noted from Table 14 above that the travel time from both ground floor and Level 1 are less than the flow time. This is consistent with the assumption that flow time governs due to the large number of occupants presented within the space.

Attached is the following:

- Hand calculation for flow time validation.

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**Holmes**

Travel distance v.s. Flow calculation validation.  
Level 1 Anchor Space

RSET component	Inputs	Value
$t_d$	determined by FDS using C/VM2 input parameters (heat detection)	0 s
$t_n$	As per C/VM2	30 s
$t_{pre}$	Pre-movement time (C/VM2 Table 3.3) for occupants awake, alert, unfamiliar and within the enclosure of origin	60 s
$t_{trav}$	= distance / walking speed (= distance/S) distance (assumed) = 52 m S = 1.2 m/s	43
$t_{flow}$	= #ppl / $F_c$ #ppl = 719 ppl See flow capacity calc - total for 3 exits, $F_c$ = 304 ppl/min $F_c$ = 5.1 ppl/s	142
$t_{move}$	= the larger of $t_{flow}$ and $t_{trav}$	tflow 142 s
<b>RSET</b>	= ( $t_d + t_n + t_{pre}$ ) + $t_{move}$	<b>RSET = 232 s</b>

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Flow capacity of egress route elements

Job No. 136249  
Name: HWCP Zone 1  
By: ACC  
Date: 16/07/2019

Egress route / space: Ground Floor

Summary - inputs and outputs

Doorset clear width: # leaves per doorset: Self-closer fitted?	$W_{(d)} = 2000$ mm = 1 leaves No	134 ppl/min	Automatic sliding door for both ground floor and level 1 carpark entrance.
Doorset clear width: # leaves per doorset: Self-closer fitted?	$W_{(d)} = 3000$ mm = 0 leaves No	213 ppl/min	Opening into mall
Doorset clear width: # leaves per doorset: Self-closer fitted?	$W_{(d)} = 1600$ mm = 2 leaves Yes	100 ppl/min	Double leaf door

Calculations (Reference: C/VM2)

<b>Door flow capacity</b>	$W_{(d)} = 2000$ mm	
Boundary layer (each side)	= 0.15 m	C/VM2 Table 3.5 (Door)
Effective width	$W_{e(d)} = 1.70$ m	
Door flow capacity	$F_{c (door)} = (1-\alpha D)kD W_{e(d)}$	
	$k = 1.40$	C/VM2: $k = 1.4$ for horizontal travel
	$\alpha = 0.266$	C/VM2: $\alpha = 0.266$
	$D = 1.90$ ppl/m <sup>2</sup>	C/VM2 Density at flow constriction
Calculated capacity	$F_{c (door)} = 2.24$ ppl/s	
Calculated $F_{c (door)}$ per leaf	= 134 ppl/min/leaf	
Would closers restrict capacity?	No	"Yes" if $F_c$ (door) per leaf >50ppl/min
Design flow capacity	$F_{c (door)} = 2.24$ ppl/s	
	134 ppl/min	
<b>Door flow capacity</b>	$W_{(d)} = 3000$ mm	
Boundary layer (each side)	= 0.15 m	C/VM2 Table 3.5 (Door)
Effective width	$W_{e(d)} = 2.70$ m	
Door flow capacity	$F_{c (door)} = (1-\alpha D)kD W_{e(d)}$	
	$k = 1.40$	C/VM2: $k = 1.4$ for horizontal travel
	$\alpha = 0.266$	C/VM2: $\alpha = 0.266$
	$D = 1.90$ ppl/m <sup>2</sup>	C/VM2 Density at flow constriction
Calculated capacity	$F_{c (door)} = 3.55$ ppl/s	
Calculated $F_{c (door)}$ per leaf	= #DIV/0! ppl/min/leaf	
Would closers restrict capacity?	No	"Yes" if $F_c$ (door) per leaf >50ppl/min
Design flow capacity	$F_{c (door)} = 3.55$ ppl/s	
	213.1 ppl/min	
<b>Door flow capacity</b>	$W_{(d)} = 1600$ mm	
Boundary layer (each side)	= 0.15 m	C/VM2 Table 3.5 (Door)
Effective width	$W_{e(d)} = 1.30$ m	
Door flow capacity	$F_{c (door)} = (1-\alpha D)kD W_{e(d)}$	
	$k = 1.40$	C/VM2: $k = 1.4$ for horizontal travel
	$\alpha = 0.266$	C/VM2: $\alpha = 0.266$
	$D = 1.90$ ppl/m <sup>2</sup>	C/VM2 Density at flow constriction
Calculated capacity	$F_{c (door)} = 1.71$ ppl/s	
Calculated $F_{c (door)}$ per leaf	= 51 ppl/min/leaf	
Would closers restrict capacity?	Yes	"Yes" if $F_c$ (door) per leaf >50ppl/min
Design flow capacity	$F_{c (door)} = 1.67$ ppl/s	
	100 ppl/min	

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Flow capacity of egress route elements

Job No. 136249  
Name: HWCP Zone 1  
By: ACC  
Date: 16/07/2019

Egress route / space: Level one

Summary - inputs and outputs

Corridor width:  $W_{(c)} = 2000$  mm 126 ppl/min

Stair width:  $W_{(s)} = 1800$  mm 85 ppl/min

Stair geometry: Stair tread = 254 mm  
Stair riser = 191 mm

Doorset clear width:  $W_{(d)} = 1600$  mm 100 ppl/min

# leaves per doorset: = 2 leaves

Self-closer fitted? Yes

Double leaf door into stairwells

Calculations [Reference: C/VM2]

a) Corridor flow capacity

Boundary layer (each side) =	0.2 m	C/VM2 Table 3.5 (corridor/ramp wall)
Effective width $W_{e(c)} =$	1.60 m	
Corridor flow capacity $F_{c(\text{corridor})} =$	$(1-\alpha D)kDW_{e(c)}$	
	$k = 1.40$	C/VM2: $k = 1.4$ for horizontal travel
	$\alpha = 0.266$	C/VM2: $\alpha = 0.266$
	$D = 1.90$ ppl/m <sup>2</sup>	C/VM2 Density at flow constriction
Corridor flow capacity $F_{c(\text{corridor})} =$	<u>2.11 ppl/s</u>	

b) Stair flow capacity

Boundary layer (each side) =	0.15 m	C/VM2 Table 3.5 (stair walls/side tread)
Effective width $W_{e(s)} =$	1.50 m	
Stair flow capacity $F_{c(\text{stair})} =$	$(1-\alpha D)k_sDW_{e(s)}$	
	$k_s = 1$	C/VM2 Table 3.4 (closest riser/tread)
	$\alpha = 0.266$	C/VM2: $\alpha = 0.266$
	$D = 1.90$	C/VM2 Density at flow constriction
Stair flow capacity $F_{c(\text{stair})} =$	<u>1.41 ppl/s</u>	
Travel speed in full stair $S = \zeta_s - \alpha k_s D$ m/s		$S = k - \alpha k D$ ( $k$ from Table 3-14.5)
	$S = 0.49$ m/s	C/VM2 Table 3.4 (closest riser/tread)
Travel speed, unimpeded $S_{\text{max}} =$	<u>0.85 m/s</u>	i.e. for very low occupant density

c) Door flow capacity

Boundary layer (each side) =	0.15 m	C/VM2 Table 3.5 (Door)
Effective width $W_{e(d)} =$	1.30 m	
Door flow capacity $F_{c(\text{door})} =$	$(1-\alpha D)kDW_{e(d)}$	
	$k = 1.40$	C/VM2: $k = 1.4$ for horizontal travel
	$\alpha = 0.266$	C/VM2: $\alpha = 0.266$
	$D = 1.90$ ppl/m <sup>2</sup>	C/VM2 Density at flow constriction
	$F_{c(\text{door})} = 1.71$ ppl/s	Based only on width
	= 51 ppl/min/leaf	
Would closers restrict capacity? =	Yes	
Design flow capacity $F_{c(\text{door})} =$	<u>1.67 ppl/s</u>	Accounting for closers and # leaves
	= 100 ppl/min	"Yes" if $F_c$ (door) per leaf >50ppl/min

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**Holmes**

Travel distance v.s. Flow calculation validation.  
Ground Floor Anchor Space

RSET component	Inputs	Value
$t_d$	determined by FDS using C/VM2 input parameters (smoke detection)	s
$t_n$	As per C/VM2	30 s
$t_{pre}$	Pre-movement time (C/VM2 Table 3.3) for occupants awake, alert, unfamiliar and within the enclosure of origin	30 s
$t_{trav}$	= distance / walking speed (= distance/S) $distance (assumed) = 43 m$ $S = 1.2 m/s$	36
$t_{flow}$	= #ppl / $F_c$ $\#ppl = 629 ppl$ See flow capacity calc - total for 3 exits, $F_c = 447 ppl/min$ $F_c = 7.5 ppl/s$	84
$t_{move}$	= the larger of $t_{flow}$ and $t_{trav}$	<b>tflow</b> 84 s
<b>RSET</b>	= $(t_d + t_n + t_{pre}) + t_{move}$	<b>RSET = 144 s</b>

= 134 ppl/min (Auto. sliding door)  
+ 213 ppl/min (opening into mall)  
+ 100 ppl/min (1600 mm double leaf door)

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Travel distance v.s. Flow calculation validation.  
Level 1 Anchor Space

RSET component	Inputs	Value
$t_d$	determined by FDS using C/VM2 input parameters (heat detection)	0 s
$t_n$	As per C/VM2	30 s
$t_{pre}$	Pre-movement time (C/VM2 Table 3.3) for occupants awake, alert, unfamiliar and within the enclosure of origin	60 s
$t_{trav}$	= distance / walking speed (= distance/S) distance (assumed) = 52 m S = 1.2 m/s	43
$t_{flow}$	= #ppl / $F_c$ #ppl = 719 ppl See flow capacity calc - total for 3 exits, $F_c$ = 304 ppl/min $F_c$ = 5.1 ppl/s	142
$t_{move}$	= the larger of $t_{flow}$ and $t_{trav}$	tflow
<b>RSET</b>	= ( $t_d + t_n + t_{pre}$ ) + $t_{move}$	<b>RSET = 232 s</b>

= 85 ppl/min (Stair 3)  
+ 85 ppl/min (Stair 4)  
+ 134 ppl/min (Auto. sliding door)

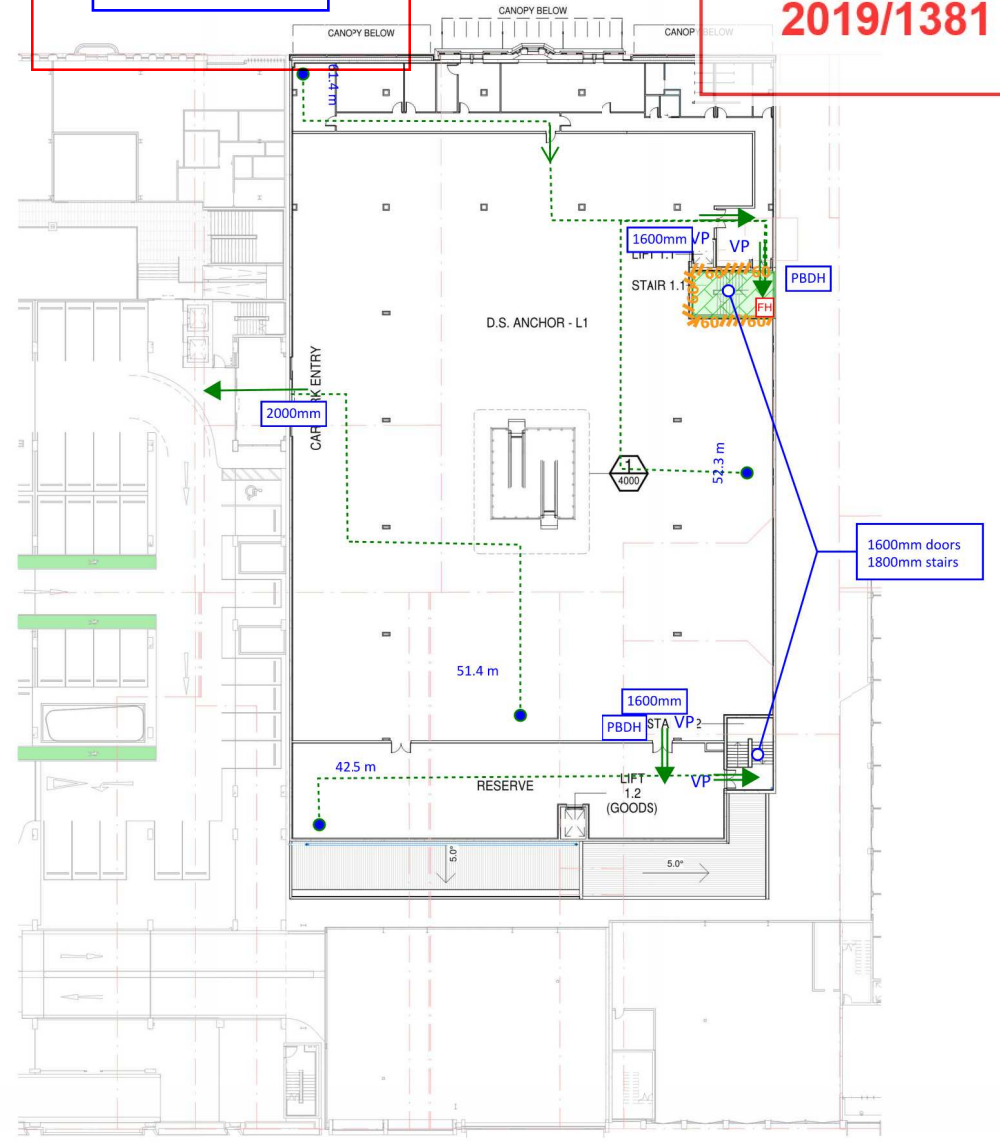
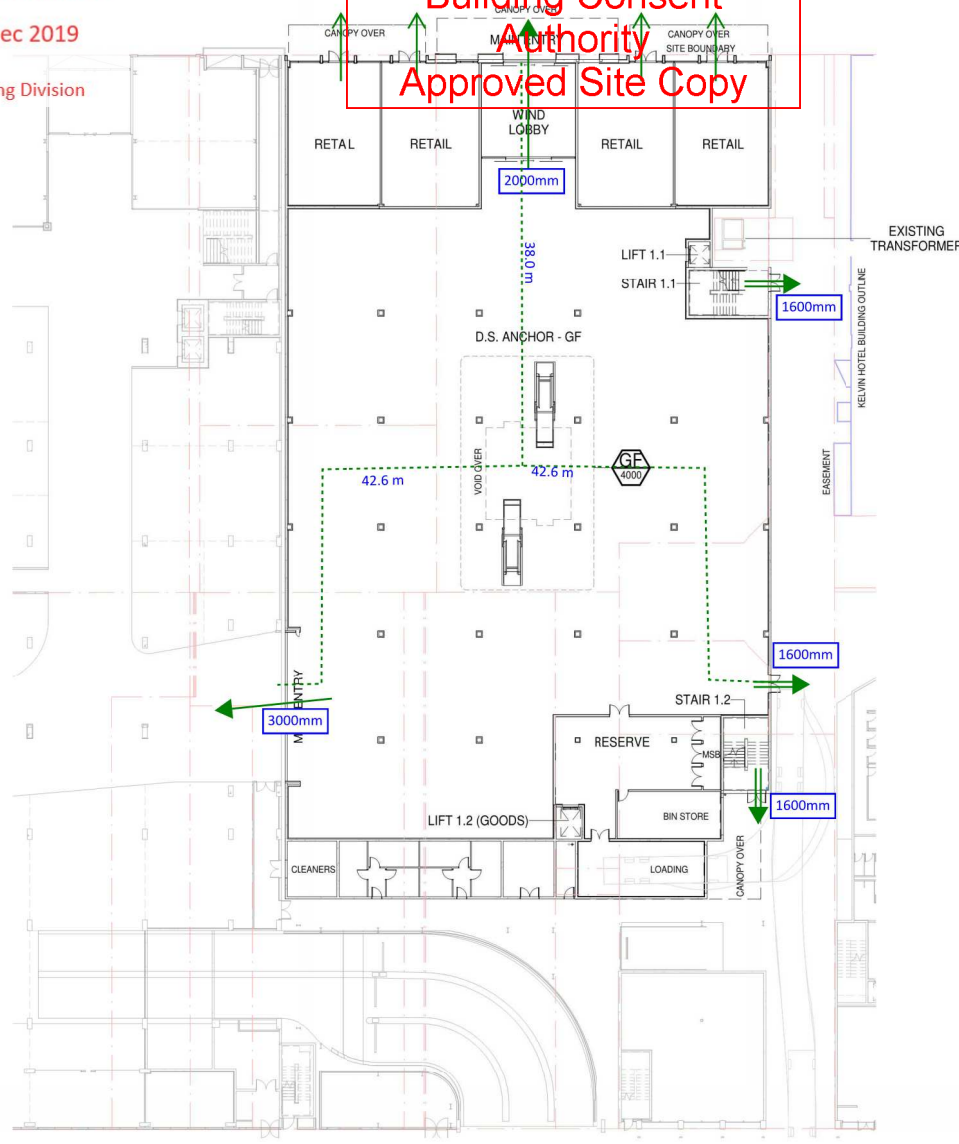
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GF Z1 - GROUND FLOOR - OVERALL  
1:250

1 Z1 - LEVEL 1 - OVERALL  
1:250

This sketch does not constitute a complete fire engineering design or detail. Detailed construction drawings are provided by others. Best viewed in colour. Not all fire separations around ducts and shafts are shown.



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Project Title	Sketch Title	Drawn: ACC	Date: 30 / 07 / 2019
HWCP - Invercargill Central	Zone 1 GF & L1 Travel Distance Measurement	Project No.	Sheet No.
		136249	Z1 B.5
		Rev	A

Rev.	Date	Description	Iss.	Appr.	Keyplan
A	27.11.18	FOR COMMENT	BH	JB	
B	19.03.19	PRELIMINARY DESIGN	BH	JB	
C	21.03.19	PRELIMINARY DESIGN	BH	DA	
D	17.04.19	FOR INFORMATION	JT	DA	



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File: C:\BGM - Revit Projects\917077 - AR-PD - INVERCARGILL - ZONE 1 - ANCHOR - 2019\_Jessica Tubo\Revit\buchan.rvt



Project  
**INVERCARGILL CENTRAL - ZONE 1**  
TAY STREET & DEE STREET CORNER  
INVERCARGILL

Project Number  
917077

Status  
PRELIMINARY DESIGN

Date Issued  
17/04/2019 14:42:26 PM

Date Issued  
21.03.19

Scale  
1:250 @A1

Drawing Title  
**ZONE 1 OVERALL FLOOR PLANS**

Drawing Number  
**Z1-PD-A-1100**

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## Appendix C ASET Assessment

### C.1 ASET for Challenging Fire CF1

Challenging Fire CF1 locates a fire centrally within the atrium on the ground floor, modelled within FDS. The fire is subject to (quick response) sprinkler control.

Table 15 - Sprinkler Activation time for CF1

(Quick Response) Sprinkler activation in FDS (s)	Sprinkler activation modelled for HRR control (s)
265	265

The graph below shows the comparison between the HRR output of the FDS burner modelled in Challenging Fire CF1 against that specified in C/VM2 ( $0.0469t^2$ ).

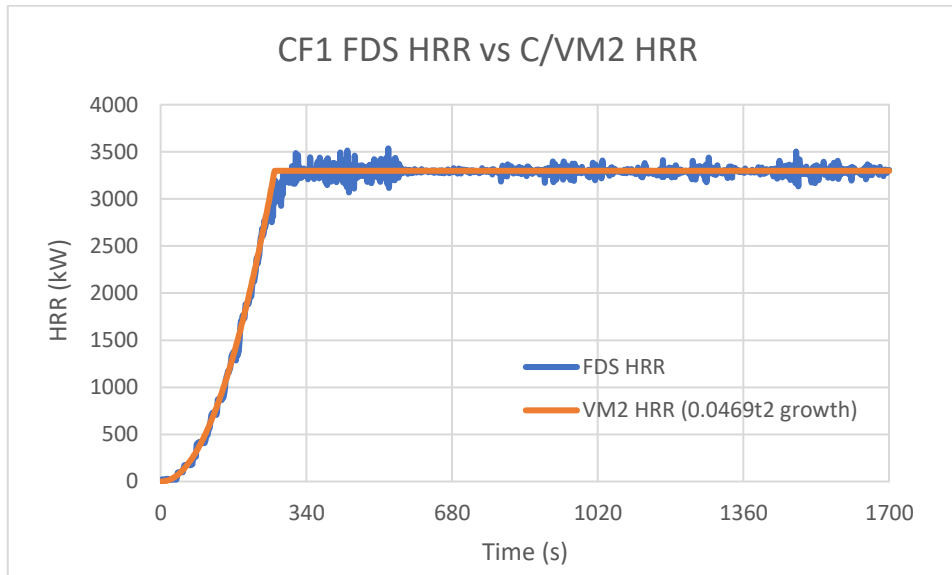


Figure 5 - CF1 FDS HRR vs VM2 HRR

#### C.1.1 CF1 ASET Summary

Tenability was assessed by FEDco slice files located 2m above each floor. The table below showed the tenability for each floor.

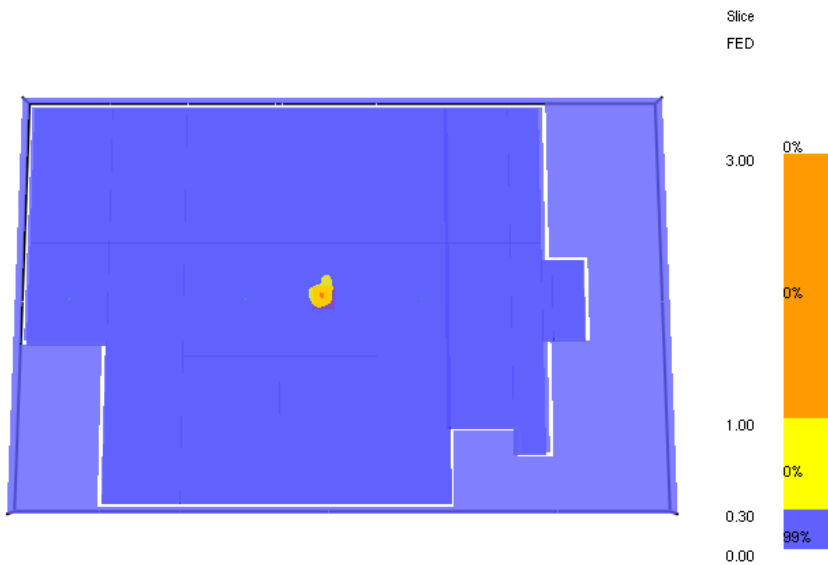
Table 16 - CF1 ASET

Floor Level	Location	Time at Tenability (s)			ASET (s)
		Visibility = 10m	FED <sub>thermal</sub> = 0.3 (temp. @ 50°C)	FED <sub>CO</sub> = 0.3	
GF	Retail	N/A	N/A	>1700	>1700
	SW Entry to Mall	N/A	N/A	>1700	>1700
	Main Entry (Esk St)	N/A	N/A	>1700	>1700
	SE Exit to Tay St	N/A	N/A	>1700	>1700



Floor Level	Location	Time at Tenability (s)			ASET (s)
		Visibility = 10m	FED <sub>thermal</sub> = 0.3 (temp. @ 50°C)	FED <sub>CO</sub> = 0.3	
L1	Retail	213	>1700	>1700	213
	Entry to Carpark	328	>1700	>1700	328
	Entry to Stair 3	386	>1700	>1700	386
	Entry to Stair 4	311	>1700	>1700	311
	Stair 3	N/A	N/A	>1700	>1700
	Stair 4	N/A	N/A	>1700	>1700

The results are shown below in FDS slice files and graphs.



Time: 1700.0

Figure 6 - CF1 FEDco slice file at 2.0 m above Ground Floor at 1700 s

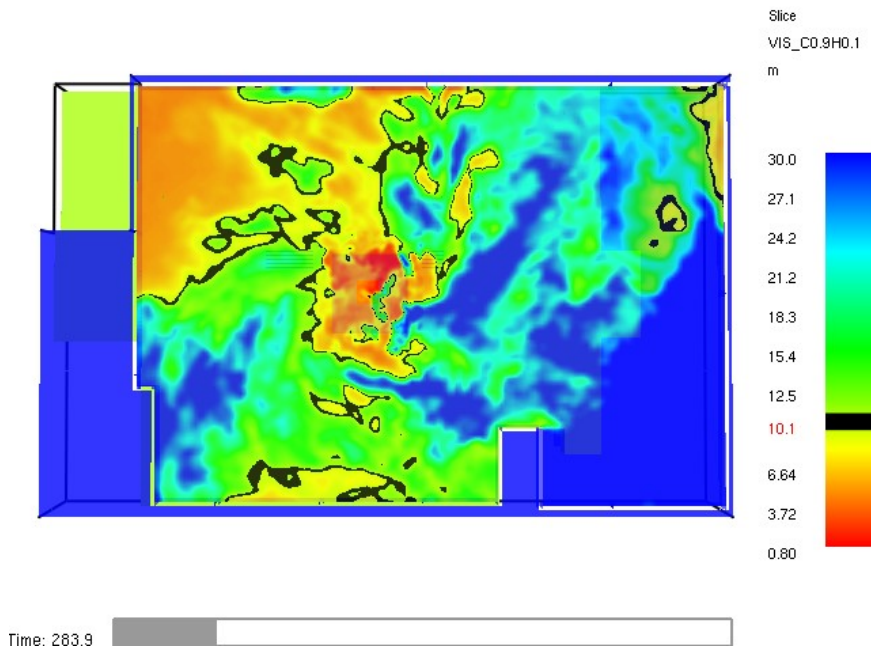


Figure 7 - CF1 Visibility slice file at 2.0 m above Level 1 floor at 284 s

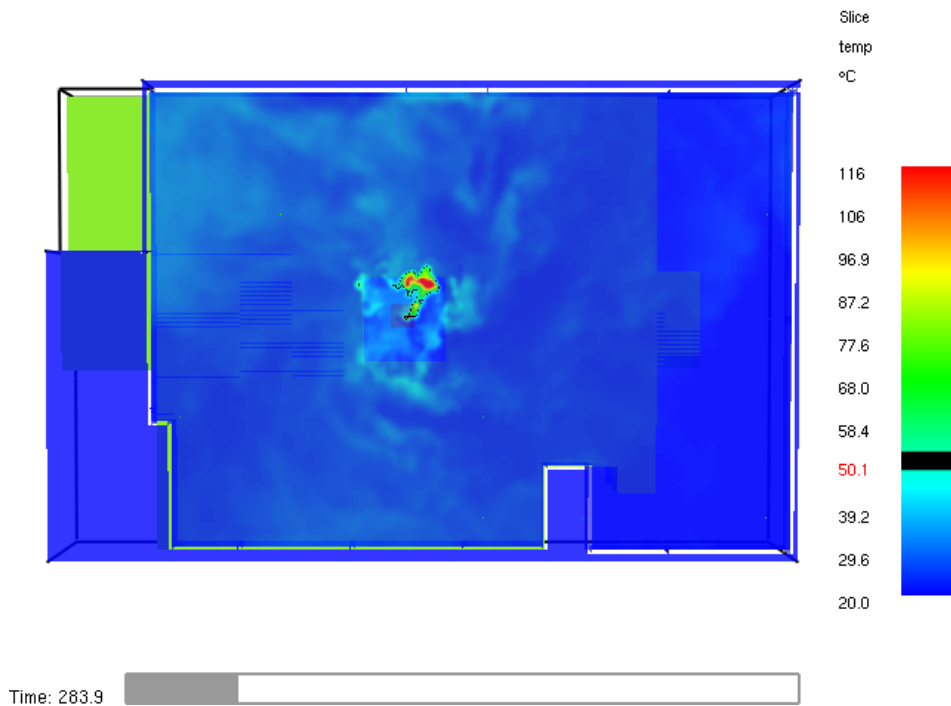
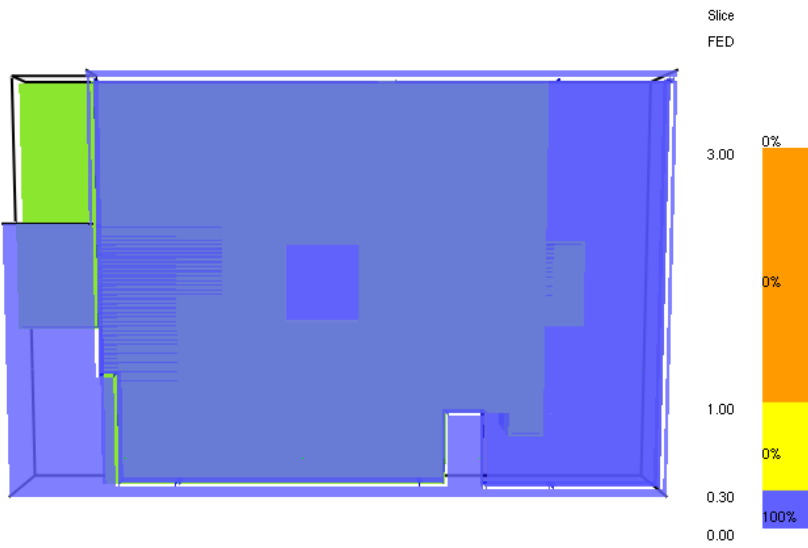


Figure 8 - CF1 Temperature slice file at 2.0 m above Level 1 floor at 284 s



Time: 1700.0

Figure 9 - CF1 FEDco slice file at 2.0 m above Level 1 floor at 1700 s

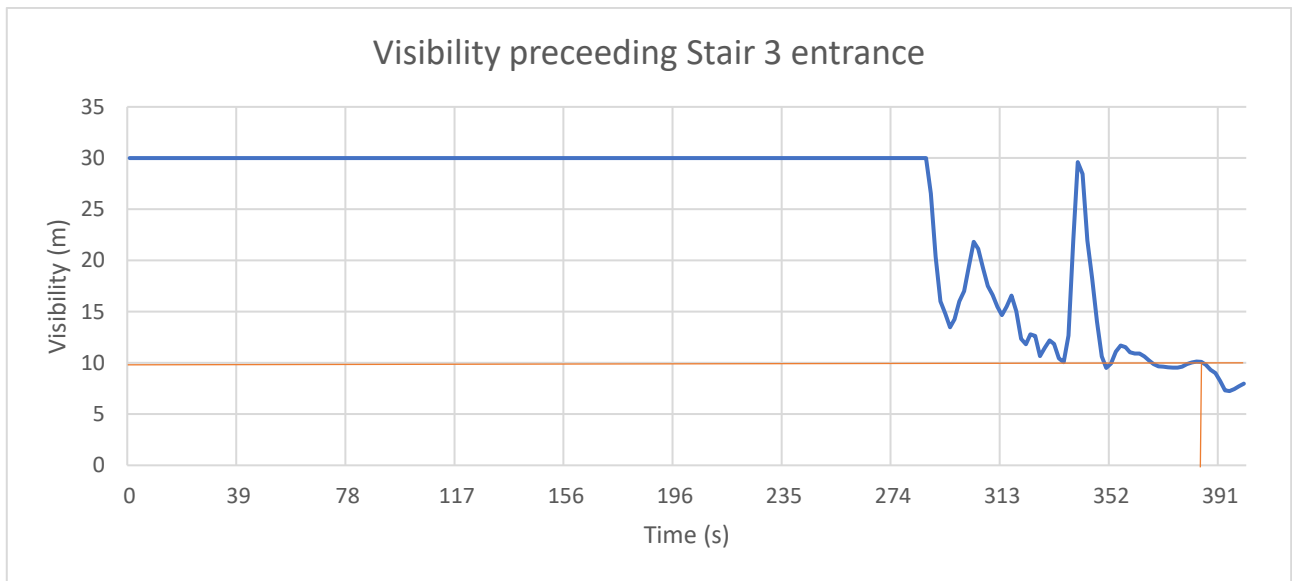


Figure 10 - CF1 Visibility preceding stair 3 entrance

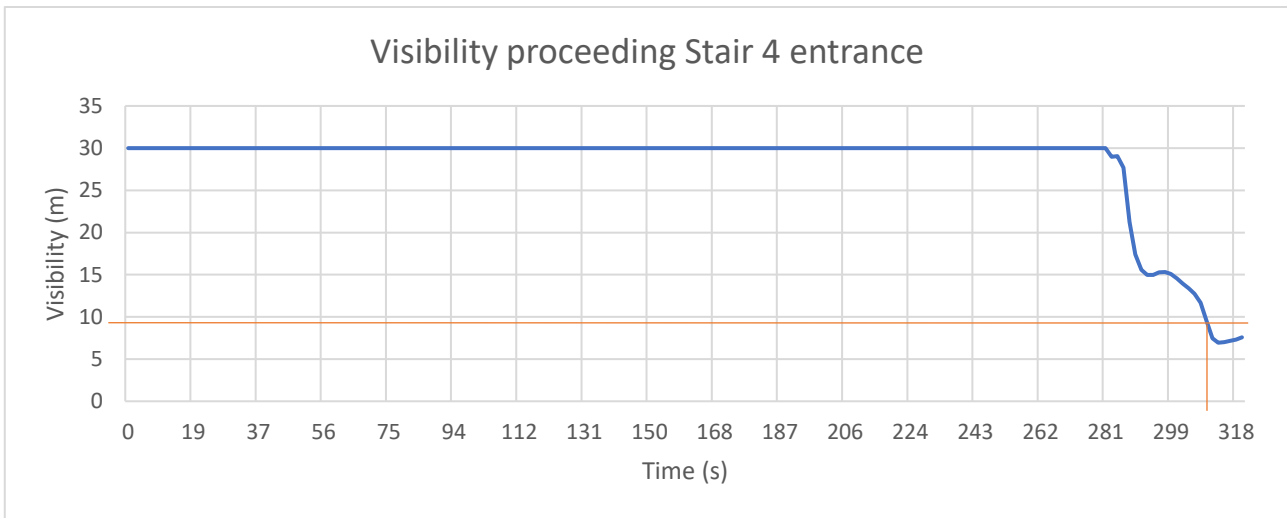


Figure 11 - CF1 Visibility proceeding stair 4 entrance

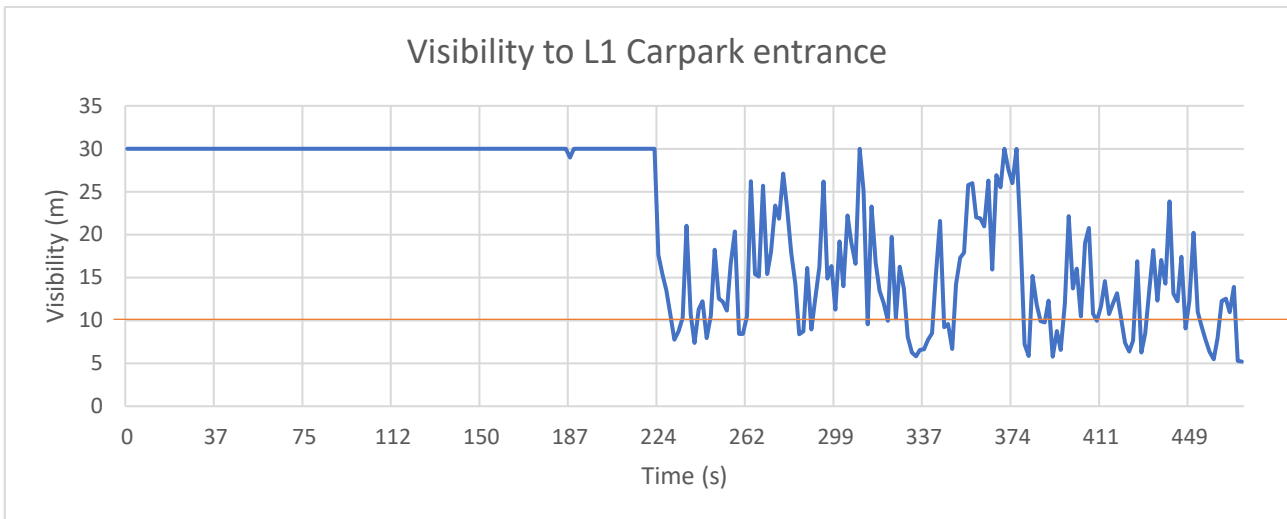


Figure 12 - CF1 Visibility proceeding Level 1 Carpark entrance

### C.1.2 CF1 ASET vs RSET Assessment

Table 17 - CF1 ASET vs RSET Summary

Floor Level	Location <sup>1</sup>	ASET (s)	RSET (s)		ASET > RSET
			Base Case	Non-Base Case	
GF	GF Anchor	>1700	209	199	Yes
	N Circulation <sup>2</sup>	>1700	-	348	Yes
L1	L1 Anchor	213 <sup>8</sup>	161 <sup>9</sup>		Yes
	Entry to Carpark	328 <sup>10</sup>	282	284	Yes
	L1 Stair 3 Landing <sup>3</sup>	386	278	270	Yes

Rev B

Floor Level	Location <sup>1</sup>	ASET (s)	RSET (s)		ASET > RSET
			Base Case	Non-Base Case	
	L1 Anchor-S BoH <sup>4</sup>	311	282	240	Yes
	L0 Stair 3 Landing <sup>5</sup>	>1700	295	287	Yes
	L0 Stair 4 Landing <sup>6</sup>	>1700	267	273	Yes
	Corridor <sup>7</sup>	>1700	-	1537	Yes
L2	Childcare Centre	>1700	783		Yes

Rev B

Explanatory Notes:

- Location is the space represented as nodes in EvacuationNZ.
- 'N Circulation' is the node that corresponds to the space precede the final exit from the Zone 2 ground floor mall space and is taken as the node where the last person leaves GF Anchor.
- 'L1 Stair 3 Landing' is the node that corresponds to the lobby space before entering into Stair 3 which indicates the queuing clear time preceding stair 3.
- 'L1 Anchor-S BoH' is the node that corresponds to the lobby space before entering into Stair 4 which indicate the queuing clear time preceding stair 4.
- 'L0 Stair3 Landing' is the node that corresponds to the space precede the final exit from Stair 3 (i.e. time to clear L1 Anchor north stairwell) which is shared by the occupants from L2 Childcare space.
- 'L0 Stair4 Landing' is the node that corresponds to the space precede the final exit from Stair 4 (i.e. time to clear L1 Anchor south stairwell).
- 'Corridor' is the node that corresponds to the space precede the final exit from Zone 3 Carpark building.
- Visibility in the south west corner starts to fail around 213 seconds as shown above in Figure 7. This is due to the smoke hitting the walls and roll down reducing the visibility at 2.0 m above level 1 floor. The RSET for occupants to move away from the south west corner and queue at the exit is approximately 161 seconds as calculated below. Therefore, the ASET vs RSET passes in this location.
- RSET to start queuing at exit is approximately 161 seconds as calculated below.

$t_d$ (s)	$t_n$ (s)	$t_{pre}$ (s)	$t_{travel}$ (s)	RSET (s)
41	30	60	35m at 1.2m/s = 30	161

- Visibility (10 m) in the near vicinity of entry to L1 carpark starts to fail intermittently around 231 seconds. The intermittent failure was:
  - Short in duration (approximately 2 seconds at a time),
  - Location being within 2m of door (further is clear),
  - Level of visibility in short duration loss is only approximately 8m visibility.

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The intermittent failure of visibility at 10 m continued until 328 seconds when the visibility (10m) failed for 10 seconds and is considered as the time to visibility failure. It is also noted that:

- Visibility (10m) to stair 3 and stair 4 entrance remained clear for the duration of evacuation of L1 Anchor space providing occupants with alternative egress routes.
- $FED_{thermal}$  and  $FED_{co}$  were maintained for the duration of L1 evacuation (284 seconds).

Therefore, given the above reasoning, it is considered that intermittent failure from 231 sec to 328 sec will not negatively impede occupant egress thus not considered as a failure of visibility.

As shown above in Table 17, ASET is greater than RSET for all locations.

**C.2 ASET for Challenging Fire CF2**

Challenging Fire CF2 locates a fire in the SW corner of ground floor Anchor to simulate a spill plume fire, modelled within FDS. The SW corner of the ground floor Anchor has the highest ceiling throughout the ground floor Anchor. The fire is subject to sprinkler control. As agreed in the Zone 1 FEB, B-Risk model has been used to find the sprinkler activation time for Challenging Fire 2 with number used as the sprinkler activation time in the FDS model.

Figure 13 below showed the B-Risk model that simulate the part of ground floor Anchor with the highest ceiling. Openings simulated within the B-Risk model has been taken directly from the floor plan measurement as shown in Appendix C.2.

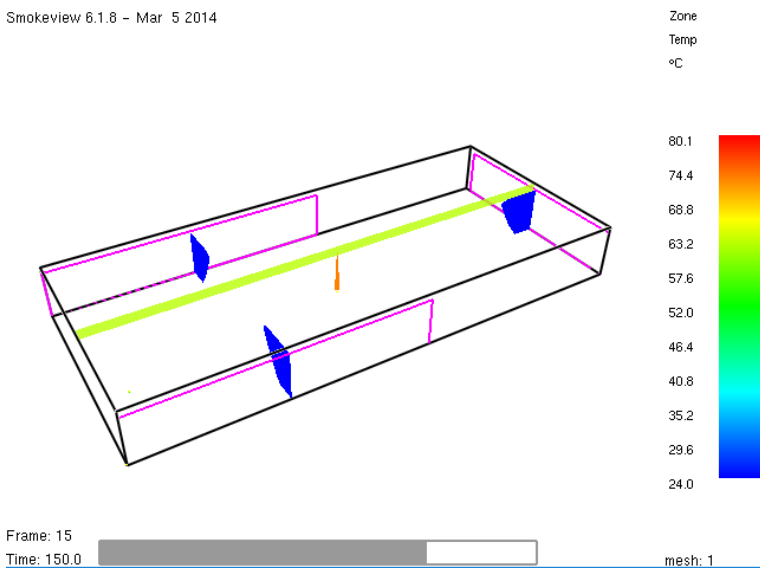


Figure 13 - CF2 Visual representation of B-Risk simulation

Table 18 - Sprinkler Activation time for CF2

[Quick Response] Sprinkler activation in B-Risk (s)	Sprinkler activation modelled for HRR control (s)
180	180

The graph below shows the comparison between the HRR output of the FDS burner modelled in Challenging Fire CF2 against that specified in C/VM2 (0.0469t<sup>2</sup>)

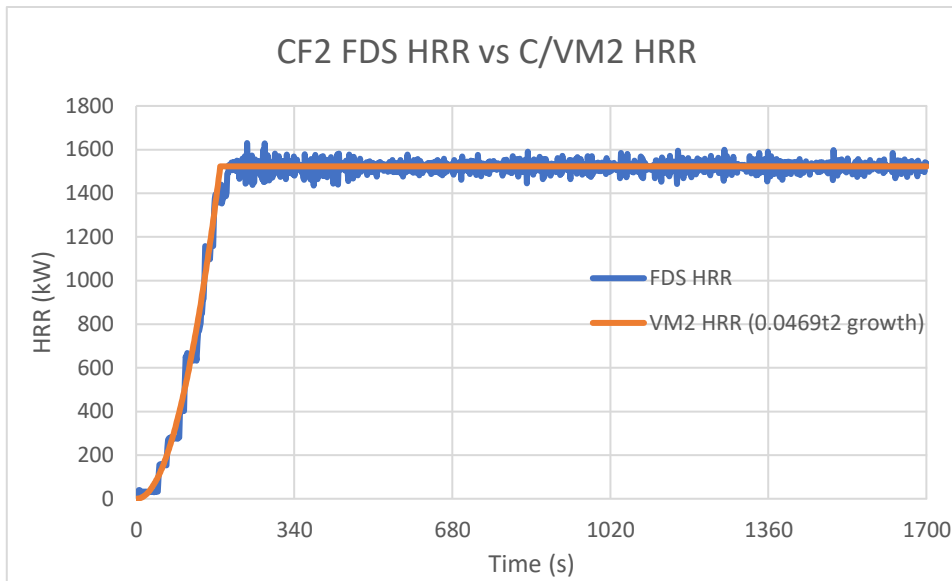


Figure 14 - CF2 FDS HRR v.s. VM2 HRR

### C.2.1 CF2 ASET Summary

Tenability was assessed by FEDco slice files located 2m above ground floor and level 1. The table below showed the tenability for each floor.

Table 19 - CF2 ASET

Floor Level	Location	Time at Tenability (s)			ASET (s)
		Visibility = 10m	FED <sub>thermal</sub> = 0.3 (temp. at 50°C)	FED <sub>co</sub> = 0.3	
GF	Retail	N/A	N/A	>1700	>1700
	SW Entry to Mall	N/A	N/A	>1700	>1700
	Main Entry (Esk St)	N/A	N/A	>1700	>1700
	SE Exit to Tay St	N/A	N/A	>1700	>1700
1L	Retail	362	>1700	>1700	362
	Entry to Carpark	1360	>1700	>1700	1360
	Entry to Stair 3	469	>1700	>1700	469
	Entry to Stair 4	362	>1700	>1700	362
	Stair 3	N/A	N/A	>1700	>1700
	Stair 4	N/A	N/A	>1700	>1700



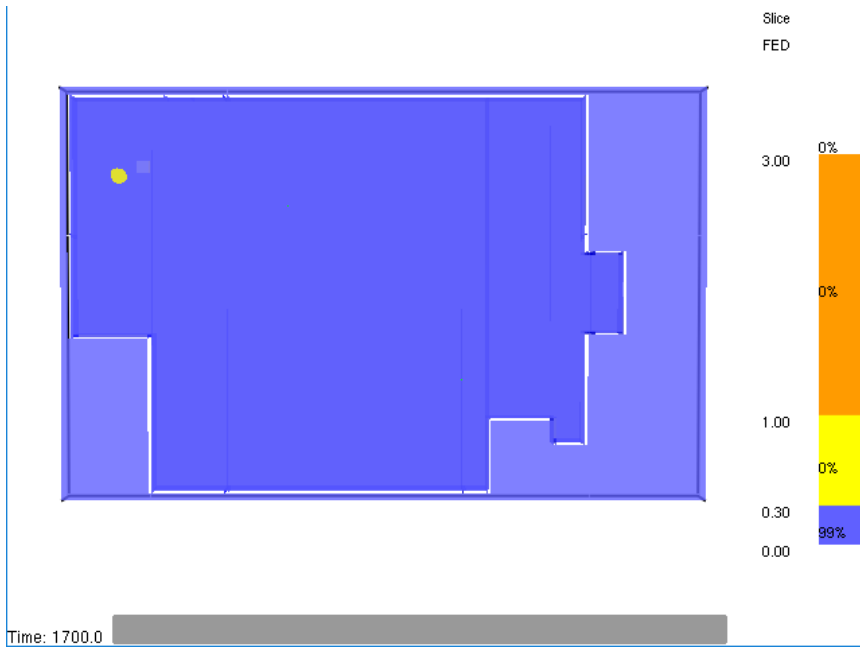


Figure 15 - CF2 FEDco slice file at 2.0 m above Ground Floor at 1700 s

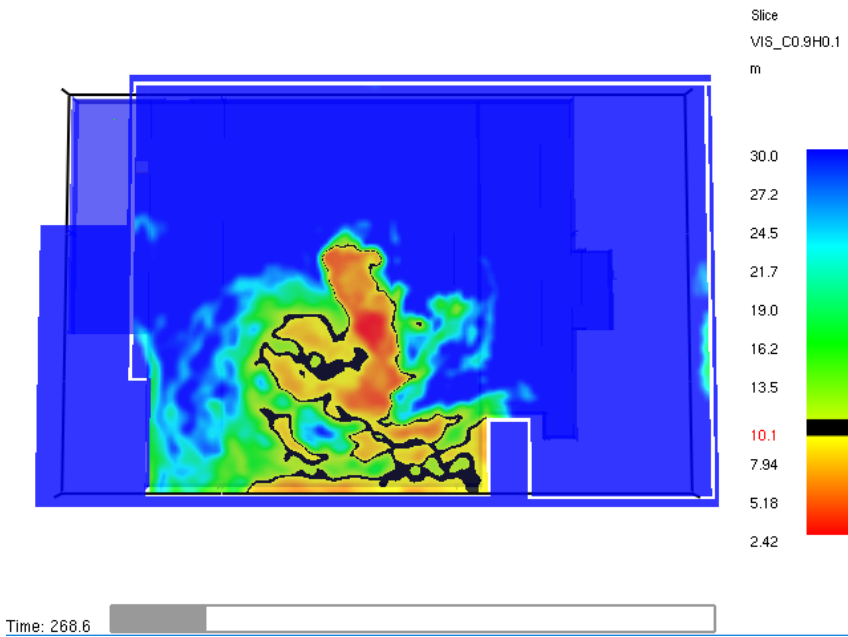


Figure 16 - CF2 Visibility slice file on Level 1 Anchor at 268 s

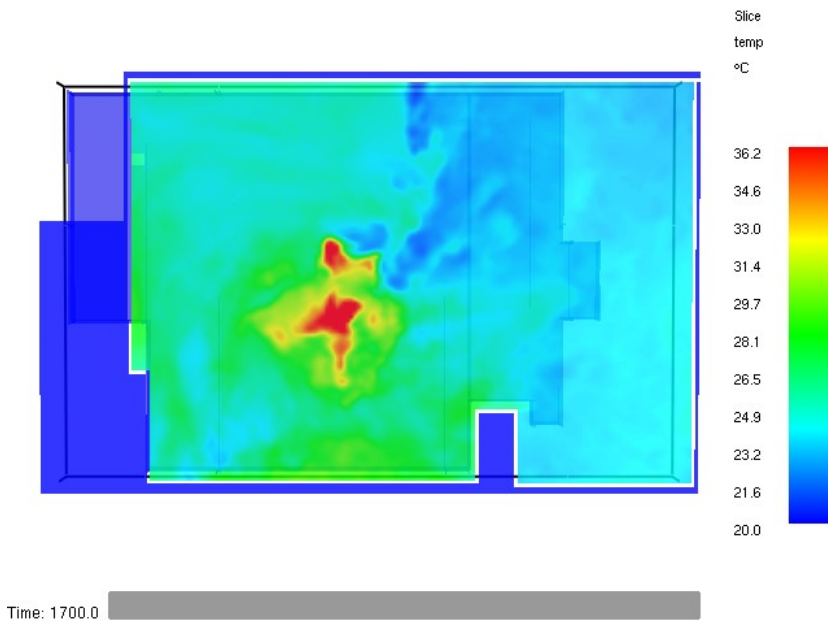


Figure 17 - CF2 Temperature slice file on Level 1 Anchor at 1700 s

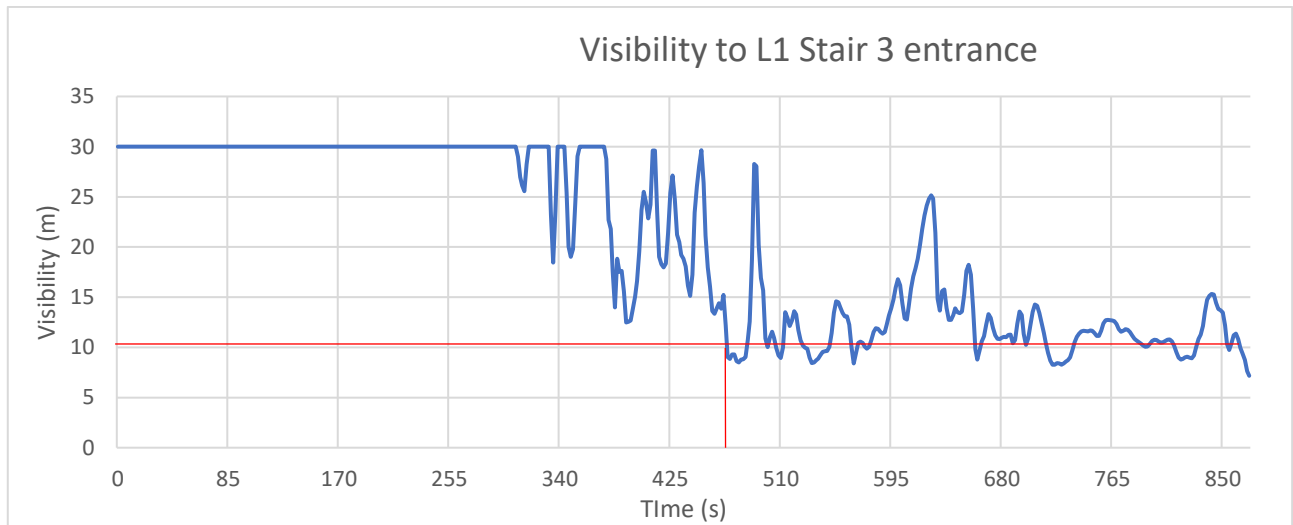


Figure 18 - CF2 Visibility at 2.0 m above Level 1 floor Stair 3 entrance

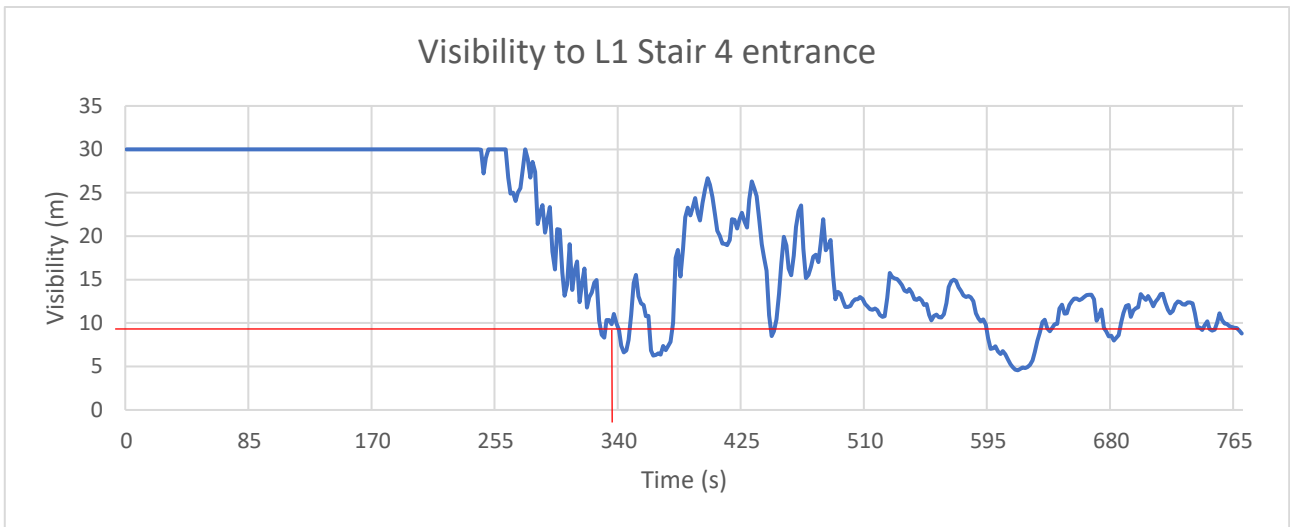


Figure 19 - CF2 Visibility at 2.0 m above Level 1 floor Stair 4 entrance

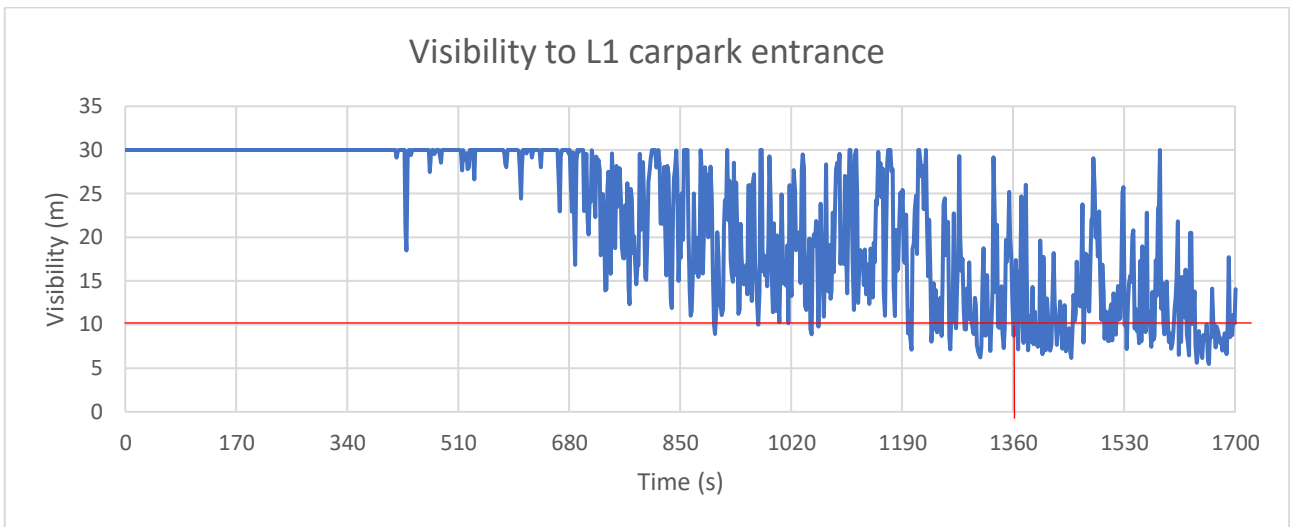


Figure 20 - CF2 Visibility at 2.0 m above Level 1 floor to L1 Carpark entrance

As shown above in Figure 16 and Figure 19, the visibility first starts to fail on the east side of atrium at 281 seconds followed by the failure of visibility on the south side of the atrium around 340 seconds before slowing moving towards the south wall (BoH wall) with intermittent failure starting around 600 seconds as shown in Figure 20.

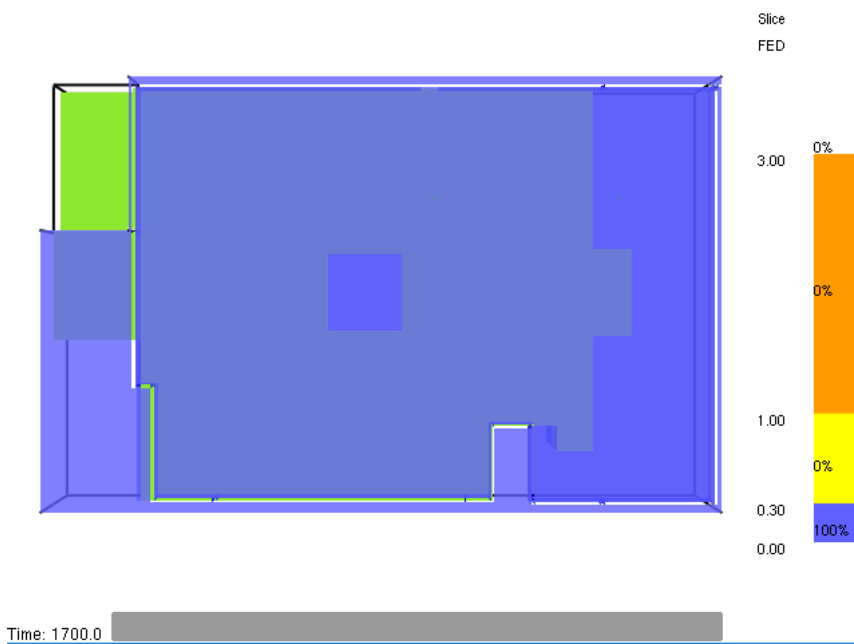


Figure 21 - CF2 FEDco slice file at 2.0 m above Level 1 floor at 1700 s

### C.2.2 CF2 ASET vs RSET Assessment

Table 20 - CF2 ASET vs RSET Summary

Floor Level	Location <sup>1</sup>	ASET (s)	RSET (s)		ASET > RSET
			Base Case	Non-Base Case	
GF	GF Anchor	>1700	193	183	Yes
	N Circulation <sup>2</sup>	>1700	-	332	Yes
L1	L1 Anchor	362	266	268	Yes
	Entry to Carpark	1360	266	268	Yes
	L1 Stair 3 Landing <sup>3</sup>	469	262	254	Yes
	L1 Anchor-S BoH <sup>4</sup>	362	266	224	Yes
	L0 Stair 3 Landing <sup>5</sup>	>1700	279	271	Yes
	L0 Stair 4 Landing <sup>6</sup>	>1700	251	257	Yes
	Corridor <sup>7</sup>	>1700	-	1521	Yes
L2	Childcare Centre	>1700	767		Yes

Explanatory Notes:

- 1) Location is the space represented as nodes in EvacuationNZ.
- 2) 'N Circulation' is the node that corresponds to the space precede the final exit from the Zone 2 ground floor mall space and is taken as the node where the last person leaves GF Anchor.

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- 3) 'L1 Stair 3 Landing' is the node that corresponds to the lobby space before entering into Stair 3 which indicates the queuing clear time preceding stair 3.
- 4) 'L1 Anchor-S BoH' is the node that corresponds to the lobby space before entering into Stair 4 which indicate the queuing clear time preceding stair 4.
- 5) 'L0 Stair3 Landing' is the node that corresponds to the space precede the final exit from Stair 3 (i.e. time to clear L1 Anchor north stairwell) which is shared by the occupants from L2 Childcare space.
- 6) 'L0 Stair4 Landing' is the node that corresponds to the space precede the final exit from Stair 4 (i.e. time to clear L1 Anchor south stairwell).
- 7) 'Corridor' is the node that corresponds to the space precede the final exit from Zone 3 Carpark building.

As shown above in Table 20, ASET is greater than RSET for all locations.

Attached is the following:

- B-Risk results for sprinkler activation time
- FSK C.2.01 – C.2.03

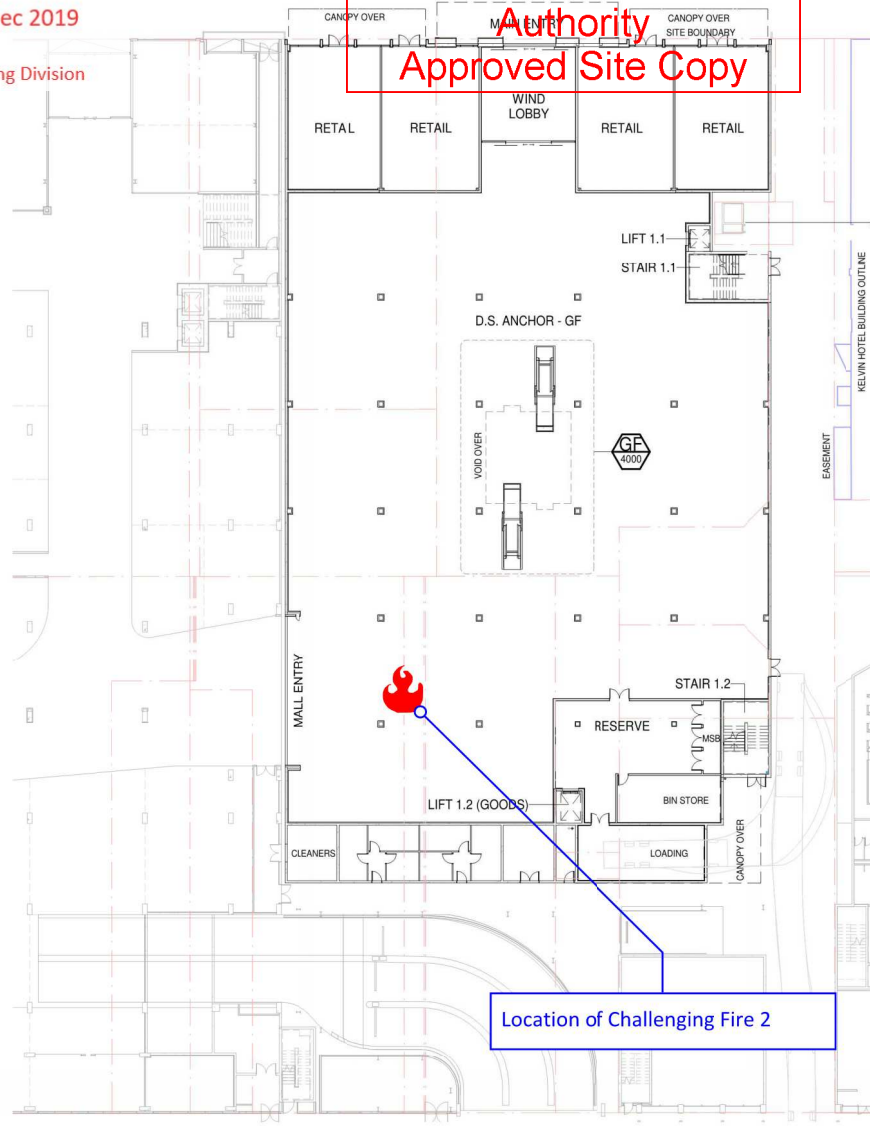
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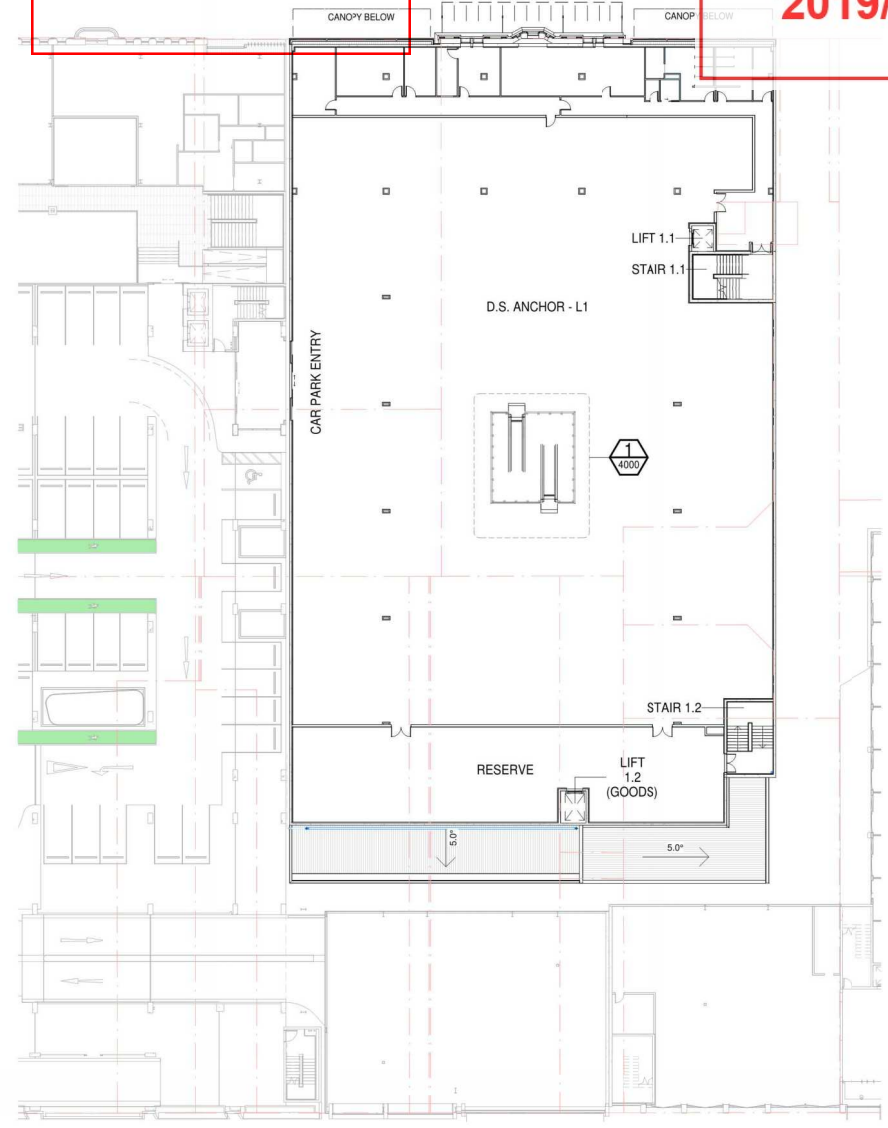
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Appendix C.2 - B-Risk  
Sprinkler Activation time for CF2  
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**2019/1381**



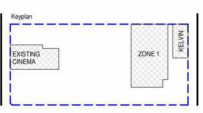
**GF** Z1 - GROUND FLOOR - OVERALL  
1:250



**1** Z1 - LEVEL 1 - OVERALL

<p>Holmes Fire LP L2, 254 Montreal St Christchurch New Zealand T: +64 3 365 3855 holmesfire.com</p>	Project Title	Sketch Title	Drawn: Author	Date: 31 / 07 / 2019
	HWCP Zone 1	B-Risk Geometry for CF2 Fire location	Project No. <b>136249</b>	Sheet No. <b>FSK C.2.01</b>

Rev.	Date	Description	Iss. Appr.	Keyplan
A	27/11/18	FOR COMMENT	BH JB	
B	19/01/19	PRELIMINARY DESIGN	BH JB	
C	21/03/19	PRELIMINARY DESIGN	BH DA	
D	17/04/19	FOR INFORMATION	JT DA	



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Project  
**INVERCARGILL CENTRAL - ZONE 1**  
TAY STREET & DEE STREET CORNER  
INVERCARGILL

Project Number  
917077

Status  
PRELIMINARY DESIGN

Date Issued  
17/04/2019 2:44:26 PM

Date Issued  
21/03/19

Scale  
1:250 @A1

Drawing Title  
**ZONE 1**  
**OVERALL FLOOR PLANS**

Drawing Number  
**Z1-PD-A-1100**

**BUCHAN**

Christchurch Studio  
+64 3 377 2973 / buchanguroup.co.nz

Revision  
**D**

Environmental & Planning Services I.C.C.		Document Received	
REF.	CEILING DESCRIPTION	LEVEL	STOPPED TO
C.01	CEILING BY TENANT - RETAIL AT 3300mm ABOVE FFL	FL	
C.05	15mm GIB PLASTERBOARD CEILING ABOVE ESCALATOR ON CONCEALED 2-WAY SUSPENDED GRID SYSTEM	LATOR ON	STOPPED TO
17 Dec 2019			
C.06	CEILING BY TENANT - RETAIL AT 3300mm ABOVE FFL	FL	

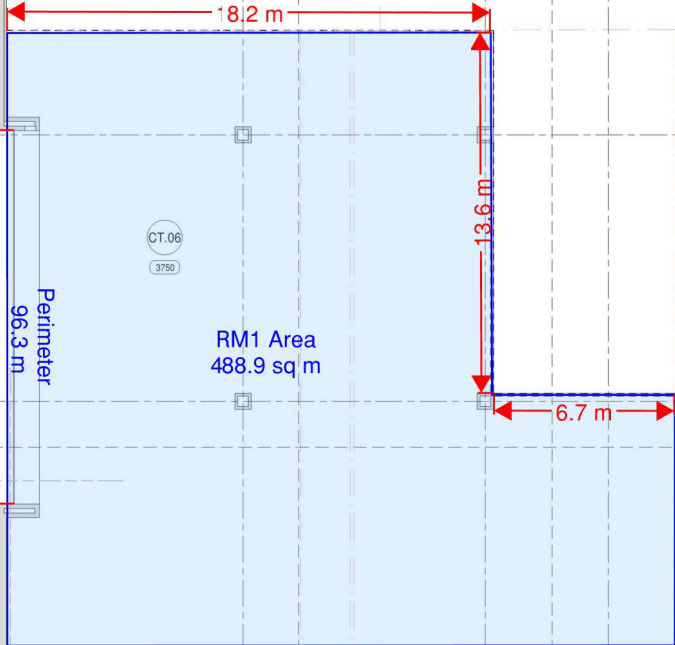
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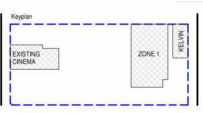
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27/02/2020

Appendix C.2 - B-Risk Sprinkler Activation time for CF2  
**2019/1381**

Total vertical opening (Length) = 14.1 + 18.2 + 13.6 + 6.7 = 52.6 m  
Opening Height = 3.3 m



Rev.	Date	Description	Iss.	Appr.	Keyplan
A	27.11.18	FOR COMMENT	BH	JB	
B	19.03.19	PRELIMINARY DESIGN	BH	JB	
C	21.03.19	PRELIMINARY DESIGN	BH	DA	



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Project  
**INVERCARGILL CENTRAL - ZONE 1**  
TAY STREET & DEE STREET CORNER  
INVERCARGILL

Project Number  
917077

Holmes Fire LP  
L2, 254 Montreal St  
Christchurch  
New Zealand  
T: +64 3 365 8855  
holmesfire.com

Project Title  
**HWCP Zone 1**

Sketch Title  
**B-Risk Geometry for CF2 Space modelled in B-Risk**

Drawn: Author	Date: 31 / 07 / 2019
Project No. <b>136249</b>	Sheet No. <b>FSK C.2.02</b>
Rev <b>A</b>	

Status  
**PRELIMINARY DESIGN**

Date Issued: 25-Apr-19 2:18:27 PM  
Date Issued: 21.03.19  
Scale: 1:100 @A

Drawing Title  
**ZONE 1 GROUND FLOOR REFLECTED CEILING PLAN - PART 2**

Drawing Number  
**Z1-PD-A-1402**

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Christchurch Studio  
+ 64 3 377 2973 / buchangroup.co.nz

WALL CODE	Document Received
WT.E01	PRECAST CONCRETE PANELS TO STRUCTURAL ENGINEERS DETAILS
WT.I01	70x13mm H1.2 TIMBER STRAPPING ON DPC WITH 13mm MDF ONE SIDE. ONE COAT OF CLEAR POLYURETHANE. 75mm LOFTED TO 70mm SEGMENTS BETWEEN STRAPPING UP TO UNDERSIDE OF CONCRETE SLAB. MINIMUM VALUE OF R1.9
WT.I02	400x45 H1.2 TIMBER STUDS @ 400cs & DWANGS @ 800cs. 13mm GIB PLASTERBOARD, STOPPED TO LEVEL 4. PAINT FINISH ON 17mm FULL HEIGHT PLYWOOD TO DS ANCHOR SIDE. 12mm MR MDF TO RESERVE SIDE. 4600mm HIGH. EARTHWOOL INSULATION WITHIN FRAME. SMOKE SEPARATION REQUIRED
WT.I04T	70mm H1.2 TIMBER STRAPPING ON DPC WITH 12mm MDF ONE SIDE. ONE COAT OF CLEAR POLYURETHANE. 75mm LOFTED TO 70mm SEGMENTS BETWEEN STRAPPING UP TO UNDERSIDE OF CONCRETE SLAB. MINIMUM VALUE OF R1.9
WT.I05T	190x45 H1.2 TIMBER STUDS @ 400cs & DWANGS @ 800cs. 13mm GIB PLASTERBOARD, STOPPED TO LEVEL 4. PAINT FINISH ON 17mm FULL HEIGHT PLYWOOD TO DS ANCHOR SIDE. 12mm MR MDF TO RESERVE SIDE. 4600mm HIGH. EARTHWOOL INSULATION WITHIN FRAME. SMOKE SEPARATION REQUIRED
WT.I11	9mm VILLAGOARD LINING FIXED BACK TO 140x45 H1.2 TREATED TIMBER FRAMING @ MAX 600 CRS TAKEN 100mm PASSED CEILING HEIGHT. CLAD WITH 400x400x15mm "CREAME MARPHIL" MARBLE TILES.

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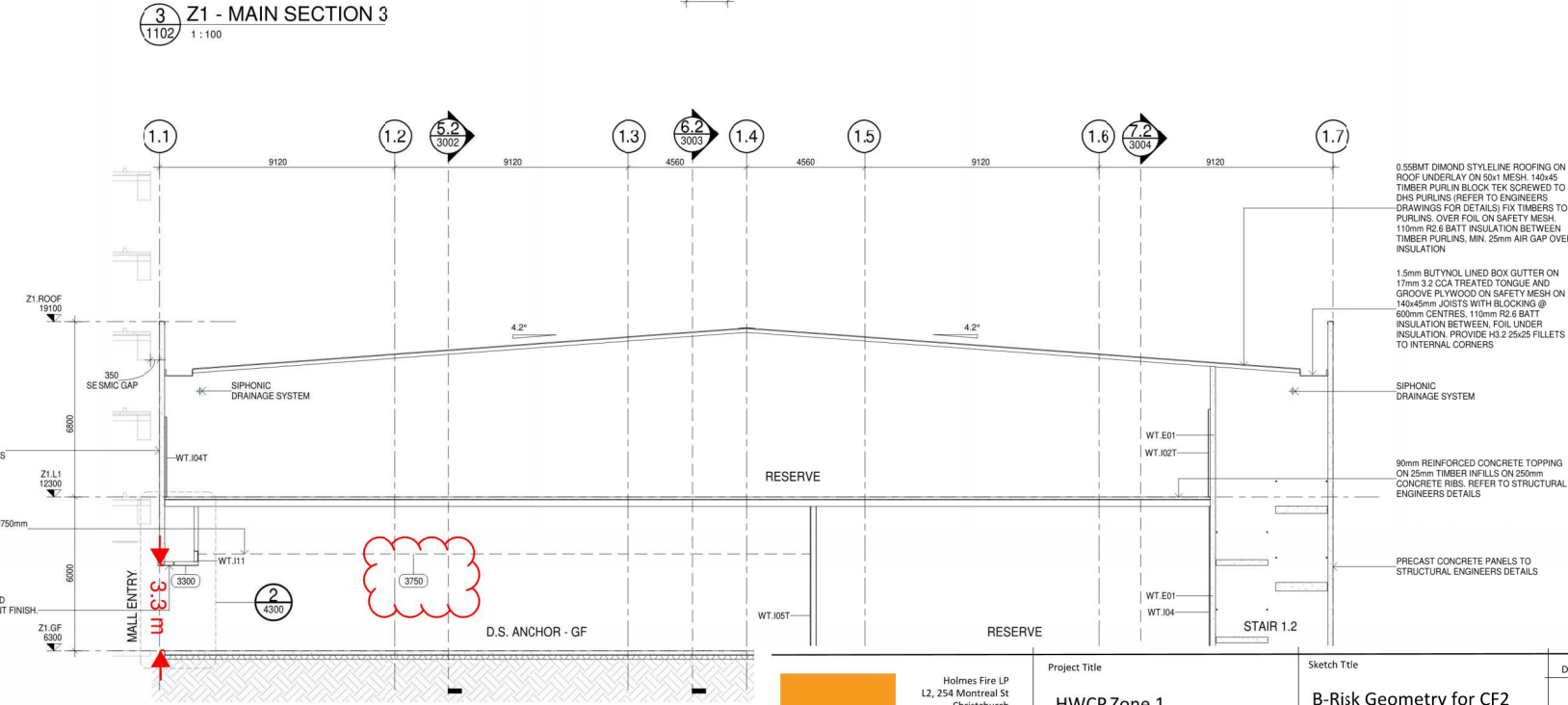
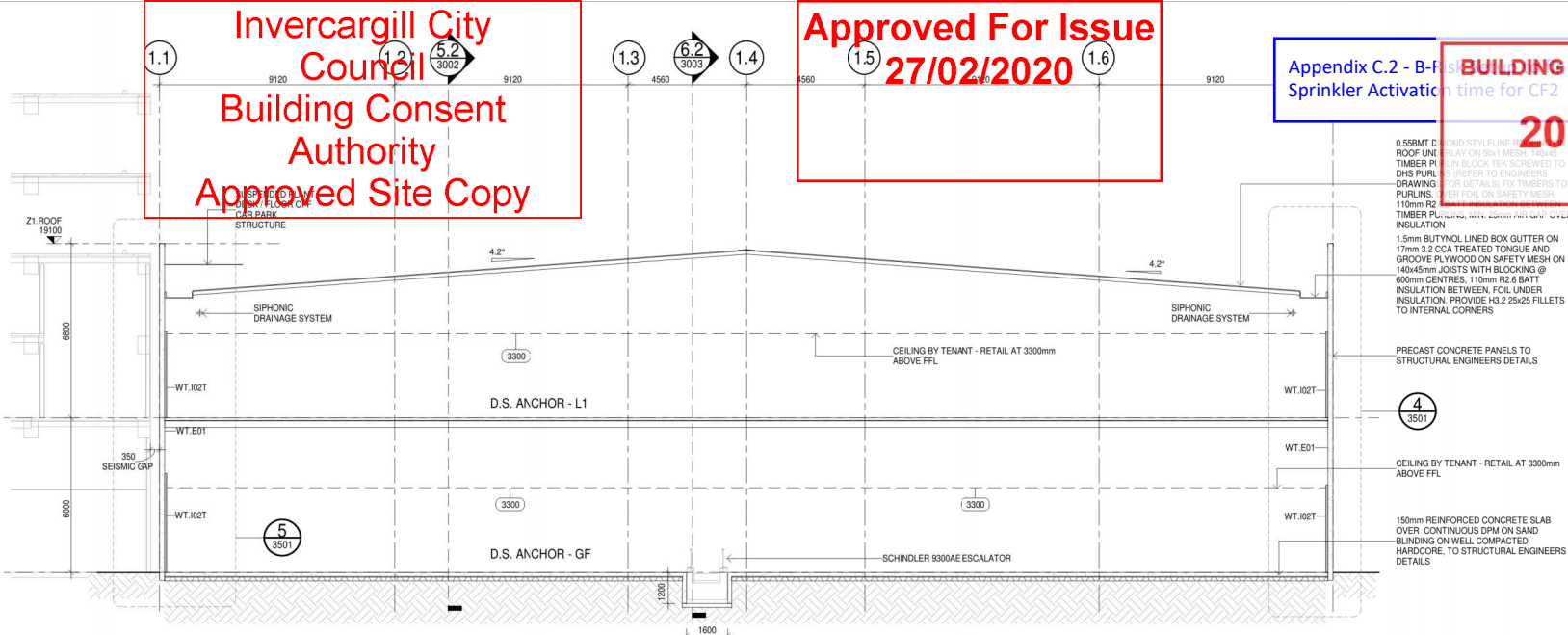
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Appendix C.2 - B-Risk Sprinkler Activation time for CF2

**2019/1381**



Holmes Fire LP  
 L2, 254 Montreal St  
 Christchurch  
 New Zealand  
 T: +64 3 365 8855  
 holmesfire.com

Project Title	HWCP Zone 1
Sketch Title	B-Risk Geometry for CF2 Opening modelled

Draws: Author	Date: 31 / 07 / 2019	
Project No.	Sheet No.	Rev
136249	FSK C.2.03	A

Rev.	Date	Description	Iss.	Appr.	Keyplan
A	27.11.18	FOR COMMENT	BH	JB	
B	19.01.19	PRELIMINARY DESIGN	BH	JB	
C	21.03.19	PRELIMINARY DESIGN	BH	DA	

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Project  
**INVERCARGILL CENTRAL - ZONE 1**  
 TAY STREET & DEE STREET CORNER  
 INVERCARGILL

Project Number  
 917077

Status  
 PRELIMINARY DESIGN

Date Issued  
 25-Apr-19 2:18:52 PM

Date Issued  
 21.03.19

Scale  
 1 : 100 @A

Drawing Title  
**ZONE 1**  
**MAIN SECTION 3 & 4**

Drawing Number  
**Z1-PD-A-3001**

Revision  
**C**





17 Dec 2019

July 31, 2019 11:17:29

Building Division

B-RISK Fire Simulator and Design Fire Tool Ver. 2019-03

Input Filename : input1.xml  
Base File : C:\Users\amy.chao\Documents\B-  
RISK\riskdata\basemodel\_default\basemodel\_default.xml

User Mode : C/VM2  
Simulation Time = 200.00 seconds.  
Initial Time-Step = 1.00 seconds.

=====  
Description of Rooms  
=====

Room 1 : GF Anchor  
Room Length (m) = 33.60  
Room Width (m) = 14.60  
Maximum Room Height (m) = 3.75  
Minimum Room Height (m) = 3.75  
Floor Elevation (m) = 0.000  
Absolute X Position (m) = 0.000  
Absolute Y Position (m) = 0.000  
Room 1 has a flat ceiling.  
Shape Factor (Af/H^2) = 34.9  
  
Wall Surface is plasterboard  
Wall Density (kg/m3) = 810.0  
Wall Conductivity (W/m.K) = 0.160  
Wall Specific Heat (J/kg.K) = 900  
Wall Emissivity = 0.88  
Wall Thickness (mm) = 13.0  
SQROOT Thermal Inertia (J.m-2.s-1/2.K-1) = 342  
  
Ceiling Surface is plasterboard  
Ceiling Density (kg/m3) = 810.0  
Ceiling Conductivity (W/m.K) = 0.160  
Ceiling Specific Heat (J/kg.K) = 900  
Ceiling Emissivity = 0.88  
Ceiling Thickness (mm) = 13.0  
SQROOT Thermal Inertia (J.m-2.s-1/2.K-1) = 342  
  
Floor Surface is concrete  
Floor Density (kg/m3) = 2300.0  
Floor Conductivity (W/m.K) = 1.200  
Floor Specific Heat (J/kg.K) = 880  
Floor Emissivity = 0.50  
Floor Thickness (mm) = 100.0  
SQROOT Thermal Inertia (J.m-2.s-1/2.K-1) = 1558

=====  
Wall Vents  
=====

Vent 1 : Mall Opening  
From room 1 to 2  
Right face of room 1  
Offset (m) = 0.000  
Vent Width (m) = 14.100  
Vent Height (m) = 3.300  
Vent Sill Height (m) = 0.000  
Vent Soffit Height (m) = 3.300  
Opening Time (sec) = 0  
Closing Time (sec) = 0  
Discharge Coefficient (-) = 0.680  
  
Vent 2 : opening2  
From room 1 to 2  
Front face of room 1  
Offset (m) = 0.000  
Vent Width (m) = 19.000  
Vent Height (m) = 3.300  
Vent Sill Height (m) = 0.000

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Appendix C.2 - B-Fris  
Sprinkler Activation time for CF2

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Vent Soffit Height (m) = 3.300  
Opening Time (sec) = 0  
Closing Time (sec) = 0  
Discharge Coefficient (-) = 0.680

Vent 3 : Opening1  
From room 1 to 2  
Rear face of room 1  
Offset (m) = 0.000  
Vent Width (m) = 19.500  
Vent Height (m) = 3.300  
Vent Sill Height (m) = 0.000  
Vent Soffit Height (m) = 3.300  
Opening Time (sec) = 0  
Closing Time (sec) = 0  
Discharge Coefficient (-) = 0.680

=====  
Ceiling/Floor Vents  
=====

=====  
Ambient Conditions  
=====

Interior Temp (C) = 24.0  
Exterior Temp (C) = 15.0  
Relative Humidity (%) = 50

=====  
Tenability Parameters  
=====

Monitoring Height for Visibility and FED (m) = 2.00  
Asphyxiant gas model = FED(CO) C/VM2  
Visibility calculations assume: reflective signs  
Egress path segments for FED calculations  
1. Start Time (sec) 0  
1. End Time (sec) 600  
1. Room 1  
2. Start Time (sec) 0  
2. End Time (sec) 0  
2. Room 0  
3. Start Time (sec) 0  
3. End Time (sec) 0  
3. Room 0

=====  
Sprinkler / Detector Parameters  
=====

Ceiling Jet model used is NIST JET.  
Sprinkler System Reliability 1.000  
Sprinkler Probability of Suppression 0.000  
Sprinkler Cooling Coefficient 1.000

Sprinkler ID 1  
Room 1  
Response Time Index (m.s)^1/2 = 50  
Sprinkler C-Factor (m/s)^1/2 = 0.65  
Water Spray Density (mm/min) = 4.20  
Radial Distance (m) = 3.250  
Distance below ceiling (m) = 0.025  
Actuation Temperature (deg C) = 68.0

=====  
Smoke Detector Parameters  
=====

Smoke Detection System Reliability 1.000  
  
Smoke Detector ID 1  
Room 1  
Radial Distance from Plume (m) = 7.00  
Distance below Ceiling (m) = 0.025  
Smoke Optical Density for Alarm (1/m) 0.097  
Detector Characteristic Length Number (m) = 15.00  
Detector response is based on OD outside the detector chamber.

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Appendix C.2 - B-F  
Sprinkler Activation time for CF2  
**BUILDING CONSENT NUMBER  
2019/1381**

Mechanical Ventilation (to/from outside)  
Ventilation not installed.  
Mech ventilation system reliability 1.000

=====  
Description of the Fire  
=====

CO Yield pre-flashover (g/g) = 0.040  
CO Yield post-flashover (g/g) = 0.400  
Soot Yield pre-flashover (g/g) = 0.070  
Soot Yield post-flashover (g/g) = 0.140  
Flame Emission Coefficient (1/m) = 1.00  
Fuel - Carbon Moles 1.00  
Fuel - Hydrogen Moles 2.00  
Fuel - Oxygen Moles 0.50  
Fuel - Nitrogen Moles 0.00  
Stoichiometric air/fuel ratio 0.0

Burning objects are manually positioned in room.  
Enhanced burning submodel is OFF

Burning Object No 1  
description

Located in Room 1  
Energy Yield (kJ/g) = 20.0  
CO2 Yield (kg/kg fuel) = 1.500  
HCN Yield (kg/kg fuel) = 0.000  
H2O Yield (kg/kg fuel) = 0.818  
Heat Release Rate Per Unit Area (kW/m2) = 250.0  
Radiant Loss Fraction = 0.35  
Fire Elevation (m) = 0.300  
Location, X-coordinate (m) = 17.000  
Location, Y-coordinate (m) = 7.200  
Fire Location (for entrainment) = CENTRE  
Plume behaviour is UNDISTURBED  
  
Alpha T2 growth coefficient = 0.0469  
Peak HRR (kW) = 20000

=====  
Postflashover Inputs  
=====

Postflashover model is OFF.

=====  
Flame Spread Inputs  
=====

This simulation includes flame spread on linings.  
Cone Calorimeter Ignition data is correlated using the Flux Time Product method.

=====  
Results from Fire Simulation  
=====

0 min 00 sec (0 sec) Room 1 Outside  
  
Layer (m) 3.750  
Upper Temp (C) 24.0  
Lower Temp (C) 24.0  
Unconstrained HRR (kW) 0.0  
HRR (kW) 0.0  
Q\* = 0.0000  
Visibility (m) at 2m 20+  
FED gases on egress path = 0.000  
FED thermal on egress path = 0.000  
  
0 min 10 sec (10 sec) Room 1 Outside  
  
Layer (m) 3.741

Upper Temp (C) 24.6  
Lower Temp (C) 22.3  
Unconstrained HRR (kW) 4.7  
HRR (kW) 4.7  
Q\* = 0.0002  
Visibility (m) at 2m 20+  
FED gases on egress path = 0.000  
FED thermal on egress path = 0.000  
  
0 min 20 sec (20 sec) Room 1 Outside  
  
Layer (m) 3.722  
Upper Temp (C) 26.2  
Lower Temp (C) 21.1  
Unconstrained HRR (kW) 18.8  
HRR (kW) 18.8  
Q\* = 0.0006  
Visibility (m) at 2m 20+  
FED gases on egress path = 0.000  
FED thermal on egress path = 0.000  
  
0 min 30 sec (30 sec) Room 1 Outside  
  
Layer (m) 3.695  
Upper Temp (C) 27.9  
Lower Temp (C) 20.1  
Unconstrained HRR (kW) 42.2  
HRR (kW) 42.2  
Q\* = 0.0014  
Visibility (m) at 2m 20+  
FED gases on egress path = 0.000  
FED thermal on egress path = 0.000  
  
0 min 40 sec (40 sec) Room 1 Outside  
  
Layer (m) 3.659  
Upper Temp (C) 30.0  
Lower Temp (C) 19.4  
Unconstrained HRR (kW) 75.0  
HRR (kW) 75.0  
Q\* = 0.0025  
Visibility (m) at 2m 20+  
FED gases on egress path = 0.000  
FED thermal on egress path = 0.000  
  
0 min 50 sec (50 sec) Room 1 Outside  
  
Layer (m) 3.615  
Upper Temp (C) 32.3  
Lower Temp (C) 18.9  
Unconstrained HRR (kW) 117.3  
HRR (kW) 117.3  
Q\* = 0.0039  
Visibility (m) at 2m 20+  
FED gases on egress path = 0.000  
FED thermal on egress path = 0.000  
  
1 min 00 sec (60 sec) Room 1 Outside  
  
Layer (m) 3.562  
Upper Temp (C) 34.7  
Lower Temp (C) 18.4  
Unconstrained HRR (kW) 168.8  
HRR (kW) 168.8  
Q\* = 0.0056  
Visibility (m) at 2m 20+  
FED gases on egress path = 0.000  
FED thermal on egress path = 0.000

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Appendix C.2 - B-Fire  
Sprinkler Activation time for CF2  
**BUILDING CONSENT NUMBER  
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Time	Room	Location	Layer (m)	Upper Temp (C)	Lower Temp (C)	Unconstrained HRR (kW)	HRR (kW)	Q* =	Visibility (m) at 2m	FED gases on egress path =	FED thermal on egress path =	
1 min	Room 1	Outside	10 sec (70 sec)	3.502	37.1	18.1	229.8	229.8	0.0076	20+	0.000	0.000
			20 sec (80 sec)	3.433	39.5	17.9	300.2	300.2	0.0099	20+	0.000	0.000
			30 sec (90 sec)	3.356	42.1	17.7	379.9	379.9	0.0126	20+	0.000	0.000
			40 sec (100 sec)	3.273	44.8	17.6	469.0	469.0	0.0155	20+	0.000	0.000
			50 sec (110 sec)	3.206	47.8	17.5	567.5	567.5	0.0188	20+	0.000	0.000
			00 sec (120 sec)	3.159	51.0	17.5	675.4	675.4	0.0223	20+	0.000	0.000

Time	Room	Location	Layer (m)	Upper Temp (C)	Lower Temp (C)	Unconstrained HRR (kW)	HRR (kW)	Q* =	Visibility (m) at 2m	FED gases on egress path =	FED thermal on egress path =	
2 min	Room 1	Outside	10 sec (130 sec)	3.125	54.5	17.5	792.6	792.6	0.0262	20+	0.000	0.000
			20 sec (140 sec)	3.099	58.3	17.6	919.2	919.2	0.0304	20+	0.000	0.000
			30 sec (150 sec)	3.079	62.4	17.7	1055.3	1055.3	0.0349	20+	0.000	0.000
			40 sec (160 sec)	3.062	66.6	17.9	1200.6	1200.6	0.0397	20+	0.000	0.000
			50 sec (170 sec)	3.048	70.9	18.0	1355.4	1355.4	0.0448	20+	0.000	0.000
			00 sec (180 sec)	3.035	75.3	18.0	1500.0	1500.0	0.0500	20+	0.000	0.000

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Lower Temp (C) 18.2  
Unconstrained HRR (kW) 1519.6  
HRR (kW) 1519.6  
Q\* = 0.0503  
Visibility (m) at 2m 20+  
FED gases on egress path = 0.000  
FED thermal on egress path = 0.000

3 min 10 sec  
(190 sec) Room 1 Outside

Layer (m) 3.030  
Upper Temp (C) 78.4  
Lower Temp (C) 18.4  
Unconstrained HRR (kW) 1519.6  
HRR (kW) 1519.6  
Q\* = 0.0503  
Visibility (m) at 2m 20+  
FED gases on egress path = 0.000  
FED thermal on egress path = 0.000

3 min 20 sec  
(200 sec) Room 1 Outside

Layer (m) 3.032  
Upper Temp (C) 80.1  
Lower Temp (C) 18.6  
Unconstrained HRR (kW) 1519.6  
HRR (kW) 1519.6  
Q\* = 0.0503  
Visibility (m) at 2m 20+  
FED gases on egress path = 0.000  
FED thermal on egress path = 0.000

=====  
Event Log  
=====

Simulation Finished.  
Sprinkler Effectiveness 1  
Fire HRR is controlled by sprinkler  
180 Sec. Sprinkler 1 responded.  
32 sec. Smoke detector 1 operates in room 1  
0 sec. Item 1 description ignited.  
Iteration 1

=====  
Computer Run-Time = 1.6 seconds.  
=====

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Appendix C.2 - B-Fire  
Sprinkler Activation time for CF2

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### C.3 ASET for Challenging Fire CF3

Challenging Fire CF3 locates a fire in the kitchen of the Level 2 Childcare centre, modelled in B-Risk. The fire is subject to (quick response) sprinkler control. All internal doors assumed to be open for the duration of the model while the external doors are modelled for the duration of egress. Figure 22 below showed the B-Risk model.

Smokeyview 6.1.8 - Mar 5 2014

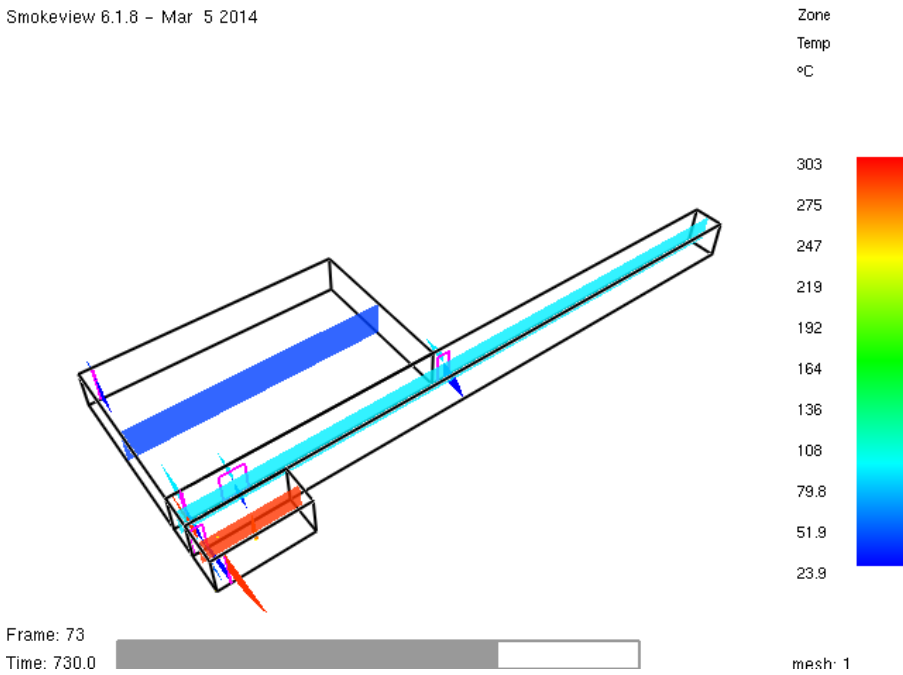


Figure 22 - CF3 Visual representation of B-Risk simulation

The heat release rate for CF3 is shown below in Figure 23.

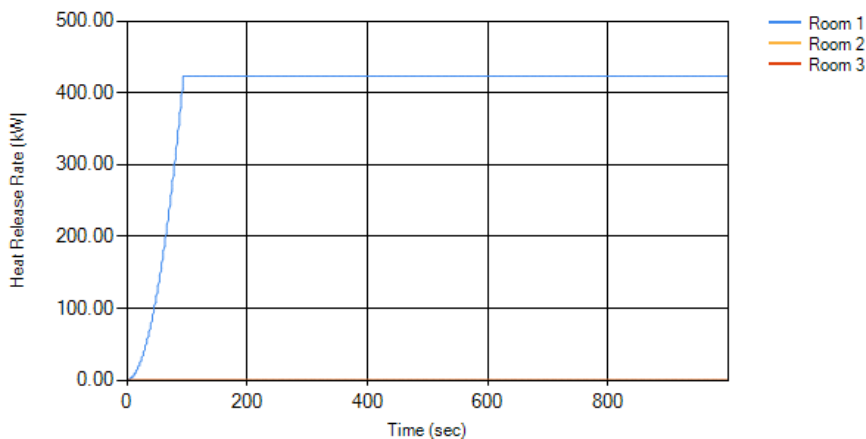


Figure 23 - CF3 FDS HRR v.s. VM2 HRR

#### C.3.1 CF3 ASET Summary

Tenability is limited to the FEDco outputs in spaces remote from fire origin as shown below in Figure 24 and Figure 25. The FEDco failed at 915 seconds in the Corridor (Room 2).

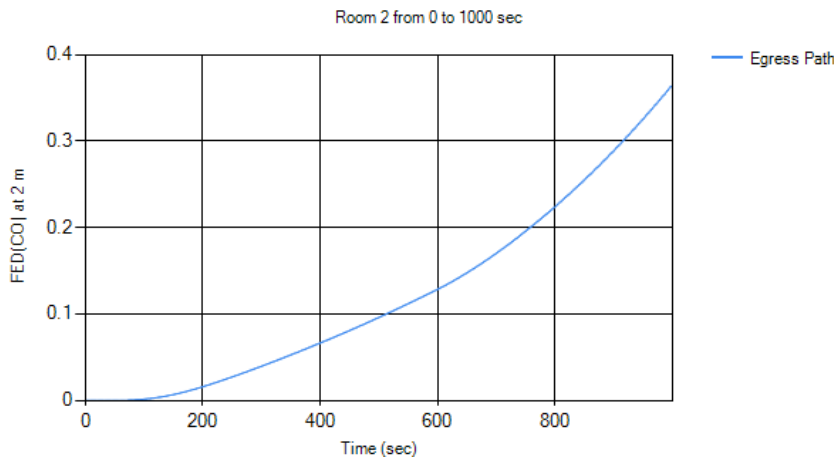


Figure 24 - CF3 FEDco in Room 2 (corridor)

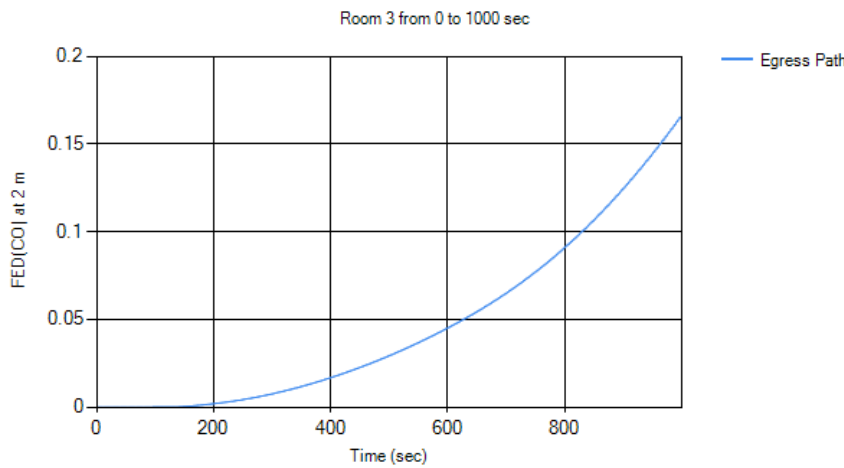


Figure 25 - CF3 FEDco in Room 3 (Childcare)

A summary of the ASET for Challenging Fire 3 is shown below in Table 21.

Table 21 - CF3 ASET Summary

Room	Time @ FED <sub>CO</sub> = 0.3 (s)	ASET (s)
Corridor (RM2)	917	917
Childcare space (RM3)	>1000	

### C.3.2 CF3 ASET vs RSET Assessment

Table 22 - CF3 ASET vs RSET Summary

Floor Level	Location <sup>1</sup>	ASET (s)	RSET (s)		ASET > RSET
			Base Case	Non-Base Case	
GF	GF Anchor	>1700	227	217	Yes

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Floor Level	Location <sup>1</sup>	ASET (s)	RSET (s)		ASET > RSET
			Base Case	Non-Base Case	
	N Circulation <sup>2</sup>	>1700	-	350	Yes
L1	L1 Anchor	>1700	270	272	Yes
	Entry to Carpark	>1700	270	272	Yes
	L1 Stair 3 Landing <sup>3</sup>	>1700	266	258	Yes
	L1 Anchor-S BoH <sup>4</sup>	>1700	270	228	Yes
	L0 Stair 3 Landing <sup>5</sup>	>1700	283	275	Yes
	L0 Stair 4 Landing <sup>6</sup>	>1700	255	261	Yes
	Corridor <sup>7</sup>	>1700	-	1521	Yes
L2	Childcare Centre	917	711		Yes

Rev B

Rev B

Rev B

Explanatory Notes:

- 1) Location is the space represented as nodes in EvacuationNZ.
- 2) 'N Circulation' is the node that corresponds to the space precede the final exit from the Zone 2 ground floor mall space and is taken as the node where the last person leaves GF Anchor.
- 3) 'L1 Stair 3 Landing' is the node that corresponds to the lobby space before entering into Stair 3 which indicates the queuing clear time preceding stair 3.
- 4) 'L1 Anchor-S BoH' is the node that corresponds to the lobby space before entering into Stair 4 which indicate the queuing clear time preceding stair 4.
- 5) 'L0 Stair3 Landing' is the node that corresponds to the space precede the final exit from Stair 3 (i.e. time to clear L1 Anchor north stairwell) which is shared by the occupants from L2 Childcare space.
- 6) 'L0 Stair4 Landing' is the node that corresponds to the space precede the final exit from Stair 4 (i.e. time to clear L1 Anchor south stairwell).
- 7) 'Corridor' is the node that corresponds to the space precede the final exit from Zone 3 Carpark building.
- 8) As shown above in Table 22, ASET is greater than RSET for all locations.

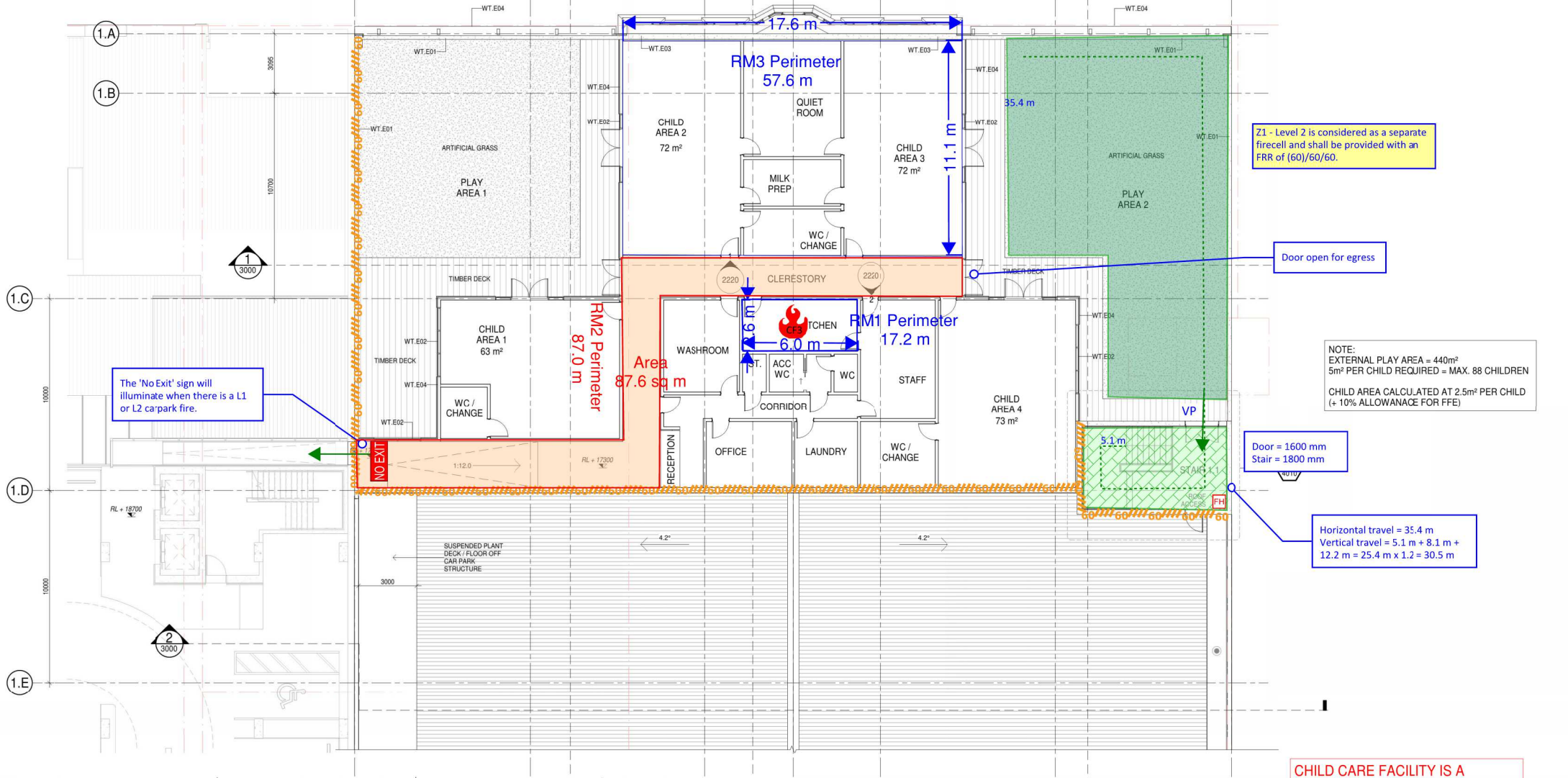
Attached is the following:

- B-Risk results
- FSK C.3.01 - C.3.02

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 Appendix C.3

BUILDING CONSENT NUMBER  
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 Appendix C.3 Childcare Centre B-Risk Setup and Results



Z1 - Level 2 is considered as a separate firecell and shall be provided with an FFR of (60)/60/60.

Door open for egress

NOTE:  
 EXTERNAL PLAY AREA = 440m²  
 5m² PER CHILD REQUIRED = MAX. 88 CHILDREN  
 CHILD AREA CALCULATED AT 2.5m² PER CHILD (+ 10% ALLOWANCE FOR FFE)

The 'No Exit' sign will illuminate when there is a L1 or L2 car park fire.

Door = 1600 mm  
 Stair = 1800 mm

Horizontal travel = 35.4 m  
 Vertical travel = 5.1 m + 8.1 m + 12.2 m = 25.4 m x 1.2 = 30.5 m

CHILD CARE FACILITY IS A PRELIMINARY CONCEPT AND IS PENDING OPERATORS REQUIREMENTS. LAYOUTS WILL LIKELY CHANGE ONCE THESE REQUIREMENTS ARE CONFIRMED.

	Project Title	Sketch Title	Drawn: ACC	Date: 02 / 05 / 2019
	Holmes Fire LP L2, 254 Montreal St Christchurch New Zealand T: +44 3 365 8855 hdmsfire.com	HWCP - Invercargill Central	Zone 1 L2 B-Risk Geometry - Floor Plan	Project No. 136249
			Rev	A

Rev.	Date	Description	Iss. Appr.	Keyplan
A	27.11.18	FOR COMMENT	BH JB	
B	19.02.19	PRELIMINARY DESIGN	BH JB	
C	05.02.19	FOR PRELIMINARY COSTING	TH JB	
D	14.02.19	FOR INFORMATION	BH BM	
E	21.03.19	PRELIMINARY DESIGN	BH DA	

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Project  
**INVERCARGILL CENTRAL - ZONE 1**  
 TAY STREET & DEE STREET CORNER  
 INVERCARGILL  
 Project Number  
 917077

Status  
 PRELIMINARY DESIGN  
 Date Issued: 25-Apr-19 2:18:12 PM  
 Date Issued: 21.03.19  
 Scale: As Indicated  
 @A1

Drawing Title  
**ZONE 1  
 LEVEL 2 FLOOR PLAN**  
 Drawing Number  
 Z1-PD-A-1105

**BUCHAN**  
 Christchurch Studio  
 + 64 3 377 2973 | buchanguroup.co.nz

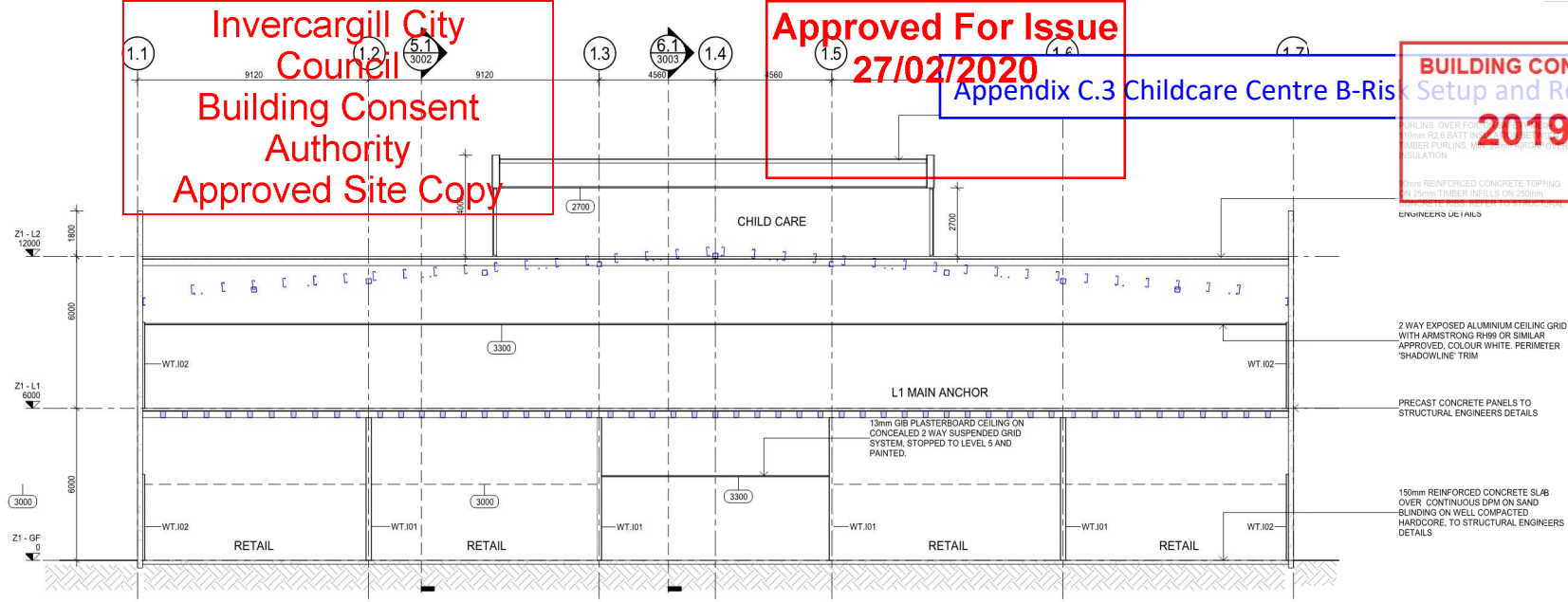


WALL TYPE	Document Received
WT.EI	PRECAST CONCRETE PANELS TO STRUCTURAL ENGINEERS DETAILS
WT.I0	13mm GIB PLASTERBOARD TO BOTH SIDES OF WALL STOPPED TO LEVEL 4. PAINT FINISH
WT.I0	70mm H1.2 TIMBER STRAPPING ON DPC WITH 3mm PAINT FINISH TO CEILING LEVEL ONE
WT.I03	90x45 H1.2 TIMBER FRAMING, DWANGS & 600cra WITH 13mm PLASTERBOARD ONE SIDE TAKEN 100mm ABOVE CEILING LEVEL ONE SIDE. LINING STEPS BACK AT BASE. REFER TO SPECIFICATION FOR DETAILS.

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 Appendix C.3 Childcare Centre B-Risk

BUILDING CONSENT NUMBER  
 Setup and Results  
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1 MAIN SECTION 1  
 1: 100

<p>Holmes Fire LP          L2, 254 Montreal St          Christchurch          New Zealand          T: +64 3 365 8855          homesfire.com</p>	Project Title	Sketch Title	Drawn: ACC	Date: 02 / 05 / 2019	
	HWCP - Invercargill Central	Zone 1 L2 B-Risk Geometry - Section	Project No.	Sheet No.	Rev
			136249	FSK C.3.02	A



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File: C:\TSG - Revit Projects\917077 - PD - INVERCARGILL - ZONE 1 - ANCHOR - 2019\_buchangroup.nz



Project  
**INVERCARGILL CENTRAL - ZONE 1**  
 TAY STREET & DEE STREET CORNER  
 INVERCARGILL

Project Number  
 917077

Status  
**PRELIMINARY DESIGN**

Date Plotted  
 11/02/2019 11:39:46 AM

Date Issued  
 \_\_\_\_\_

Scale  
 1:100 @A

Drawing Title  
**ZONE 1  
 MAIN SECTION 1 & 2**

Drawing Number  
**Z1-PD-3000**

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Appendix C.5 Childcare Centre B-

BUILDING CONSENT NUMBER

2019/1381

Job Name	HWCP Zone 1 Childcare
Job Number	136249
Name	ACC
Date	19-Jul-19

**B-Risk Checklist**

CF3 RM 1 - kitchen

**Building Parameters**

Volume, $V_R$ =		$m^3$
Floor area, $A_F$ =	15.6	$m^2$
Perimeter, $P$ =	17.2	m

**Model Inputs**

Length, $L$ =	6.0	m
Width, $W$ =	2.6	m
Height, $H$ =	2.7	m

**Shape Factor**

Average enclosure height =	2.7	m
SF =	2	

Single room OK

**Non-dimensional HRR Parameter**

HRR (peak or value at RSET) =	459.7	kW
Non-dimensional HRR =	0.03	

Within recommended limit

Note: Applies to room of fire origin only and only during the period of interest

**Leakage**

Leakage wall area ( $m^2$ ) =	46.4
Leakage area ( $\times 0.001m^2/m^2$ )	0.0464
Leakage width (m)	0.017

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Appendix C.3 Childcare Centre B-

BUILDING CONSENT NUMBER

2019/1381

Job Name HWCP Zone 1 Childcare  
Job Number 136249  
Name ACC  
Date 19-Jul-19

B-Risk Checklist

CF1 RM 2 - Corridor

Building Parameters

Volume,  $V_R$  =   $m^3$   
Floor area,  $A_F$  =   $m^2$   
Perimeter,  $P$  =   $m$

Model Inputs

Length,  $L$  =   $m$   
Width,  $W$  =   $m$   
Height,  $H$  =   $m$

Shape Factor

Average enclosure height =   $m$   
SF =

Single room OK

Non-dimensional HRR Parameter

HRR (peak or value at RSET) =   $kW$   
Non-dimensional HRR =

Within recommended limit

Note: Applies to room of fire origin only and only during the period of interest

Leakage

Leakage wall area ( $m^2$ )=   
Leakage area ( $\times 0.001m^2/m^2$ )   
Leakage width( $m$ )

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Appendix C.3 Childcare Centre B-Risk Setup and Results

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Job Name	HWCP Zone 1 Childcare
Job Number	136249
Name	ACC
Date	19-Jul-19

**B-Risk Checklist** CF3 RM3 - Child carea

<b>Building Parameters</b>		
Volume, $V_R$ =		$m^3$
Floor area, $A_F$ =	195.36	$m^2$
Perimeter, $P$ =	57.6	m
<b>Model Inputs</b>		
Length, $L$ =	17.6	m
Width, $W$ =	11.1	m
Height, $H$ =	2.7	m

<b>Shape Factor</b>		
Average enclosure height =	2.7	m
SF =	27	
Single room OK		

<b>Non-dimensional HRR Parameter</b>		
HRR (peak or value at RSET) =	0	kW
Non-dimensional HRR =	0.00	
Within recommended limit		
Note: Applies to room of fire origin only and only during the period of interest		

<b>Leakage</b>		
Leakage wall area ( $m^2$ )=	155.5	
Leakage area ( $\times 0.001m^2/m^2$ )	0.1555	
Leakage width (m)	0.058	

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July 31, 2019 12:15:00

Building Division

B-RISK Fire Simulator and Design Fire Tool Ver. 2019-03

Input Filename : input1.xml  
Base File : C:\Users\amy.chao\Documents\B-RISK\riskdata\basemodel\_136249\_Zone1\_CF3  
\basemodel\_136249\_Zone1\_CF3.xml

User Mode : C/VM2  
Simulation Time = 1000.00 seconds.  
Initial Time-Step = 1.00 seconds.

=====  
Description of Rooms  
=====

Room 1 : Kitchen

Room Length (m) = 6.00  
Room Width (m) = 2.60  
Maximum Room Height (m) = 2.70  
Minimum Room Height (m) = 2.70  
Floor Elevation (m) = 0.000  
Absolute X Position (m) = 0.000  
Absolute Y Position (m) = 0.000  
Room 1 has a flat ceiling.  
Shape Factor (Af/H^2) = 2.1

Wall Surface is plasterboard  
Wall Density (kg/m3) = 810.0  
Wall Conductivity (W/m.K) = 0.160  
Wall Specific Heat (J/kg.K) = 900  
Wall Emissivity = 0.88  
Wall Thickness (mm) = 13.0  
SQROOT Thermal Inertia (J.m-2.s-1/2.K-1) = 342

Ceiling Surface is plasterboard  
Ceiling Density (kg/m3) = 810.0  
Ceiling Conductivity (W/m.K) = 0.160  
Ceiling Specific Heat (J/kg.K) = 900  
Ceiling Emissivity = 0.88  
Ceiling Thickness (mm) = 13.0  
SQROOT Thermal Inertia (J.m-2.s-1/2.K-1) = 342

Floor Surface is concrete  
Floor Density (kg/m3) = 2300.0  
Floor Conductivity (W/m.K) = 1.200  
Floor Specific Heat (J/kg.K) = 880  
Floor Emissivity = 0.50  
Floor Thickness = (mm) 100.0  
SQROOT Thermal Inertia (J.m-2.s-1/2.K-1) = 1558

Room 2 : Corridor

Room Length (m) = 41.40  
Room Width (m) = 2.10  
Maximum Room Height (m) = 2.70  
Minimum Room Height (m) = 2.70  
Floor Elevation (m) = 0.000  
Absolute X Position (m) = 0.000  
Absolute Y Position (m) = 2.600  
Room 2 has a flat ceiling.  
Shape Factor (Af/H^2) = 11.9

Wall Surface is plasterboard  
Wall Density (kg/m3) = 810.0  
Wall Conductivity (W/m.K) = 0.160  
Wall Specific Heat (J/kg.K) = 900  
Wall Emissivity = 0.88  
Wall Thickness (mm) = 13.0  
SQROOT Thermal Inertia (J.m-2.s-1/2.K-1) = 342

Ceiling Surface is plasterboard  
Ceiling Density (kg/m3) = 810.0  
Ceiling Conductivity (W/m.K) = 0.160

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Ceiling Specific Heat (J/kg.K) = 900  
Ceiling Emissivity = 0.88  
Ceiling Thickness (mm) = 13.0  
SQROOT Thermal Inertia (J.m-2.s-1/2.K-1) = 342

Floor Surface is concrete  
Floor Density (kg/m3) = 2300.0  
Floor Conductivity (W/m.K) = 1.200  
Floor Specific Heat (J/kg.K) = 880  
Floor Emissivity = 0.50  
Floor Thickness = (mm) 100.0  
SQROOT Thermal Inertia (J.m-2.s-1/2.K-1) = 1558

Room 3 : Child Area

Room Length (m) = 17.60  
Room Width (m) = 11.10  
Maximum Room Height (m) = 2.70  
Minimum Room Height (m) = 2.70  
Floor Elevation (m) = 0.000  
Absolute X Position (m) = 0.000  
Absolute Y Position (m) = 4.700  
Room 3 has a flat ceiling.  
Shape Factor (Af/H^2) = 26.8

Wall Surface is plasterboard  
Wall Density (kg/m3) = 810.0  
Wall Conductivity (W/m.K) = 0.160  
Wall Specific Heat (J/kg.K) = 900  
Wall Emissivity = 0.88  
Wall Thickness (mm) = 13.0  
SQROOT Thermal Inertia (J.m-2.s-1/2.K-1) = 342

Ceiling Surface is plasterboard  
Ceiling Density (kg/m3) = 810.0  
Ceiling Conductivity (W/m.K) = 0.160  
Ceiling Specific Heat (J/kg.K) = 900  
Ceiling Emissivity = 0.88  
Ceiling Thickness (mm) = 13.0  
SQROOT Thermal Inertia (J.m-2.s-1/2.K-1) = 342

Floor Surface is concrete  
Floor Density (kg/m3) = 2300.0  
Floor Conductivity (W/m.K) = 1.200  
Floor Specific Heat (J/kg.K) = 880  
Floor Emissivity = 0.50  
Floor Thickness = (mm) 100.0  
SQROOT Thermal Inertia (J.m-2.s-1/2.K-1) = 1558

=====  
Wall Vents  
=====

Vent 1 : RM1 Leak

From room 1 to 4  
Front face of room 1  
Offset (m) = 0.800  
Vent Width (m) = 0.017  
Vent Height (m) = 2.700  
Vent Sill Height (m) = 0.000  
Vent Soffit Height (m) = 2.700  
Opening Time (sec) = 0  
Closing Time (sec) = 0  
Discharge Coefficient (-) = 1.000

Vent 2 : RM2 Leak

From room 2 to 4  
Rear face of room 2  
Offset (m) = 0.800  
Vent Width (m) = 0.087  
Vent Height (m) = 2.700  
Vent Sill Height (m) = 0.000  
Vent Soffit Height (m) = 2.700  
Opening Time (sec) = 0  
Closing Time (sec) = 0  
Discharge Coefficient (-) = 1.000

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Vent 3 : Door - RM1-RM2

From room 1 to 2  
Rear face of room 1  
Offset (m) = 0.100  
Vent Width (m) = 0.800  
Vent Height (m) = 2.100  
Vent Sill Height (m) = 0.000  
Vent Soffit Height (m) = 2.100  
Opening Time (sec) = 0  
Closing Time (sec) = 0  
Discharge Coefficient (-) = 0.680

Vent 4 : Final Exit - RM2

From room 2 to 4  
Rear face of room 2  
Offset (m) = 18.000  
Vent Width (m) = 0.900  
Vent Height (m) = 2.100  
Vent Sill Height (m) = 0.000  
Vent Soffit Height (m) = 2.100  
Opening Time (sec) = 120  
Closing Time (sec) = 600  
Discharge Coefficient (-) = 0.680

Vent 5 : RM3 Leak

From room 3 to 4  
Rear face of room 3  
Offset (m) = 0.800  
Vent Width (m) = 0.058  
Vent Height (m) = 2.700  
Vent Sill Height (m) = 0.000  
Vent Soffit Height (m) = 2.700  
Opening Time (sec) = 0  
Closing Time (sec) = 0  
Discharge Coefficient (-) = 1.000

Vent 6 : Door - RM2-RM3

From room 2 to 3  
Rear face of room 2  
Offset (m) = 3.000  
Vent Width (m) = 1.600  
Vent Height (m) = 2.100  
Vent Sill Height (m) = 0.000  
Vent Soffit Height (m) = 2.100  
Opening Time (sec) = 0  
Closing Time (sec) = 0  
Discharge Coefficient (-) = 0.680

=====  
Ceiling/Floor Vents  
=====

Ambient Conditions  
=====

Interior Temp (C) = 24.0  
Exterior Temp (C) = 15.0  
Relative Humidity (%) = 50

=====  
Tenability Parameters  
=====

Monitoring Height for Visibility and FED (m) = 2.00  
Asphyxiant gas model = FED(CO) C/VM2  
Visibility calculations assume: reflective signs  
Egress path segments for FED calculations  
1. Start Time (sec) 0  
1. End Time (sec) 1000  
1. Room 2  
2. Start Time (sec) 0  
2. End Time (sec) 0  
2. Room 0  
3. Start Time (sec) 0  
3. End Time (sec) 0

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3. Room 0

=====  
Sprinkler / Detector Parameters  
=====

Ceiling Jet model used is NIST JET.  
Sprinkler System Reliability 1.000  
Sprinkler Probability of Suppression 0.000  
Sprinkler Cooling Coefficient 1.000  
  
Sprinkler ID 1  
Room 1  
Response Time Index (m.s)<sup>1/2</sup> = 50  
Sprinkler C-Factor (m/s)<sup>1/2</sup> = 0.65  
Water Spray Density (mm/min) = 4.20  
Radial Distance (m) = 3.250  
Distance below ceiling (m) = 0.025  
Actuation Temperature (deg C) = 68.0

=====  
Smoke Detector Parameters  
=====

Smoke Detection System Reliability 1.000  
  
Smoke Detector ID 1  
Room 1  
Radial Distance from Plume (m) = 7.00  
Distance below Ceiling (m) = 0.025  
Smoke Optical Density for Alarm (1/m) 0.097  
Detector Characteristic Length Number (m) = 15.00  
Detector response is based on OD outside the detector chamber.

=====  
Mechanical Ventilation (to/from outside)  
=====

Mechanical Ventilation not installed.  
Mech ventilation system reliability 1.000

=====  
Description of the Fire  
=====

CO Yield pre-flashover (g/g) = 0.040  
CO Yield post-flashover (g/g) = 0.400  
Soot Yield pre-flashover (g/g) = 0.070  
Soot Yield post-flashover (g/g) = 0.140  
Flame Emission Coefficient (1/m) = 1.00  
Fuel - Carbon Moles 1.00  
Fuel - Hydrogen Moles 2.00  
Fuel - Oxygen Moles 0.50  
Fuel - Nitrogen Moles 0.00  
Stoichiometric air/fuel ratio 0.0

Burning objects are manually positioned in room.  
Enhanced burning submodel is OFF

Burning Object No 1

description Located in Room 1  
Energy Yield (kJ/g) = 20.0  
CO2 Yield (kg/kg fuel) = 1.500  
HCN Yield (kg/kg fuel) = 0.000  
H2O Yield (kg/kg fuel) = 0.818  
Heat Release Rate Per Unit Area (kW/m2) = 250.0  
Radiant Loss Fraction = 0.35  
Fire Elevation (m) = 0.300  
Location, X-coordinate (m) = 3.000  
Location, Y-coordinate (m) = 1.300  
Fire Location (for entrainment) = CENTRE  
Plume behaviour is UNDISTURBED  
  
Alpha T2 growth coefficient = 0.0469  
Peak HRR (kW) = 20000

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Postflashover model is OFF.

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Results from Fire Simulation

0 min	00 sec (0 sec)	Room 1	Room 2	Room 3	Outside
	Layer (m)	2.700	2.700	2.700	
	Upper Temp (C)	24.0	24.0	24.0	
	Lower Temp (C)	24.0	24.0	24.0	
	Unconstrained HRR (kW)	0.0	0.0	0.0	
	HRR (kW)	0.0	0.0	0.0	
	Q* =	0.0000	-	-	
	Visibility (m) at 2m	20+	20+	20+	

FED gases on egress path = 0.000  
FED thermal on egress path = 0.000

0 min	10 sec (10 sec)	Room 1	Room 2	Room 3	Outside
	Layer (m)	2.560	2.700	2.700	
	Upper Temp (C)	28.0	23.9	24.0	
	Lower Temp (C)	24.0	23.9	24.0	
	Unconstrained HRR (kW)	4.7	0.0	0.0	
	HRR (kW)	4.7	0.0	0.0	
	Q* =	0.0004	-	-	
	Visibility (m) at 2m	20+	20+	20+	

FED gases on egress path = 0.000  
FED thermal on egress path = 0.000

0 min	20 sec (20 sec)	Room 1	Room 2	Room 3	Outside
	Layer (m)	2.280	2.700	2.700	
	Upper Temp (C)	34.9	23.9	24.0	
	Lower Temp (C)	24.1	23.9	24.0	
	Unconstrained HRR (kW)	18.8	0.0	0.0	
	HRR (kW)	18.8	0.0	0.0	
	Q* =	0.0014	-	-	
	Visibility (m) at 2m	20+	20+	20+	

FED gases on egress path = 0.000  
FED thermal on egress path = 0.000

0 min	30 sec (30 sec)	Room 1	Room 2	Room 3	Outside
	Layer (m)	1.938	2.694	2.700	
	Upper Temp (C)	44.6	25.2	24.0	
	Lower Temp (C)	24.4	23.9	24.0	
	Unconstrained HRR (kW)	42.2	0.0	0.0	
	HRR (kW)	42.2	0.0	0.0	
	Q* =	0.0032	-	-	
	Visibility (m) at 2m	2.77	20+	20+	

FED gases on egress path = 0.000  
FED thermal on egress path = 0.000

0 min	40 sec (40 sec)	Room 1	Room 2	Room 3	Outside
	Layer (m)	1.624	2.638	2.700	

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Upper Temp (C)	57.6	27.7	24.0	
Lower Temp (C)	25.1	23.9	24.0	
Unconstrained HRR (kW)	75.0	0.0	0.0	
HRR (kW)	75.0	0.0	0.0	
Q* =	0.0056	-	-	
Visibility (m) at 2m	1.74	20+	20+	

FED gases on egress path = 0.000  
FED thermal on egress path = 0.000

0 min	50 sec (50 sec)	Room 1	Room 2	Room 3	Outside
	Layer (m)	1.389	2.502	2.700	
	Upper Temp (C)	76.1	30.4	24.0	
	Lower Temp (C)	26.4	23.9	24.0	
	Unconstrained HRR (kW)	117.3	0.0	0.0	
	HRR (kW)	117.3	0.0	0.0	
	Q* =	0.0088	-	-	
	Visibility (m) at 2m	1.19	20+	20+	

FED gases on egress path = 0.000  
FED thermal on egress path = 0.000

1 min	00 sec (60 sec)	Room 1	Room 2	Room 3	Outside
	Layer (m)	1.232	2.292	2.700	
	Upper Temp (C)	98.4	33.7	24.0	
	Lower Temp (C)	28.5	23.9	23.9	
	Unconstrained HRR (kW)	168.8	0.0	0.0	
	HRR (kW)	168.8	0.0	0.0	
	Q* =	0.0127	-	-	
	Visibility (m) at 2m	0.88	20+	20+	

FED gases on egress path = 0.000  
FED thermal on egress path = 0.000

1 min	10 sec (70 sec)	Room 1	Room 2	Room 3	Outside
	Layer (m)	1.151	2.041	2.699	
	Upper Temp (C)	123.5	37.7	24.2	
	Lower Temp (C)	33.1	23.9	23.9	
	Unconstrained HRR (kW)	229.8	0.0	0.0	
	HRR (kW)	229.8	0.0	0.0	
	Q* =	0.0173	-	-	
	Visibility (m) at 2m	0.67	20+	20+	

FED gases on egress path = 0.000  
FED thermal on egress path = 0.000

1 min	20 sec (80 sec)	Room 1	Room 2	Room 3	Outside
	Layer (m)	1.105	1.798	2.684	
	Upper Temp (C)	152.2	41.9	25.7	
	Lower Temp (C)	41.6	23.9	23.9	
	Unconstrained HRR (kW)	300.2	0.0	0.0	
	HRR (kW)	300.2	0.0	0.0	
	Q* =	0.0226	-	-	
	Visibility (m) at 2m	0.53	2.49	20+	

FED gases on egress path = 0.000  
FED thermal on egress path = 0.001

1 min	30 sec (90 sec)	Room 1	Room 2	Room 3	Outside
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Layer (m)	1.053	1.55	2.18
Upper Temp (C)	181.7	46.5	26.8
Lower Temp (C)	53.7	31.6	28.5
Unconstrained HRR (kW)	379.9	0.0	0.0
HRR (kW)	379.9	0.0	0.0
Q* =	0.0286	-	-
Visibility (m) at 2m	0.45	1.90	20+

FED gases on egress path = 0.001  
FED thermal on egress path = 0.002

1 min	40 sec (100 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)	1.005	1.341	2.545		
Upper Temp (C)	208.7	51.2	27.9		
Lower Temp (C)	69.2	24.2	23.9		
Unconstrained HRR (kW)	423.3	0.0	0.0		
HRR (kW)	423.3	0.0	0.0		
Q* =	0.0318	-	-		
Visibility (m) at 2m	0.39	1.51	20+		

FED gases on egress path = 0.001  
FED thermal on egress path = 0.004

1 min	50 sec (110 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)	1.010	1.191	2.422		
Upper Temp (C)	221.7	55.5	28.7		
Lower Temp (C)	83.5	24.5	24.0		
Unconstrained HRR (kW)	423.3	0.0	0.0		
HRR (kW)	423.3	0.0	0.0		
Q* =	0.0318	-	-		
Visibility (m) at 2m	0.36	1.24	20+		

FED gases on egress path = 0.002  
FED thermal on egress path = 0.006

2 min	00 sec (120 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)	1.007	1.086	2.280		
Upper Temp (C)	229.0	58.7	29.3		
Lower Temp (C)	91.6	25.1	24.0		
Unconstrained HRR (kW)	423.3	0.0	0.0		
HRR (kW)	423.3	0.0	0.0		
Q* =	0.0318	-	-		
Visibility (m) at 2m	0.34	1.06	20+		

FED gases on egress path = 0.003  
FED thermal on egress path = 0.010

2 min	10 sec (130 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)	1.018	1.084	2.141		
Upper Temp (C)	233.4	61.2	29.7		
Lower Temp (C)	98.8	26.0	24.0		
Unconstrained HRR (kW)	423.3	0.0	0.0		
HRR (kW)	423.3	0.0	0.0		
Q* =	0.0318	-	-		
Visibility (m) at 2m	0.33	0.93	20+		

FED gases on egress path = 0.004  
FED thermal on egress path = 0.013

2 min	20 sec (140 sec)	Room 1	Room 2	Room 3	Outside
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Layer (m)	1.022	1.096	2.003
Upper Temp (C)	237.3	63.3	30.1
Lower Temp (C)	104.7	26.9	24.0
Unconstrained HRR (kW)	423.3	0.0	0.0
HRR (kW)	423.3	0.0	0.0
Q* =	0.0318	-	-
Visibility (m) at 2m	0.33	0.83	20+

FED gases on egress path = 0.005  
FED thermal on egress path = 0.018

2 min	30 sec (150 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)	1.023	1.109	1.873		
Upper Temp (C)	240.1	65.1	30.5		
Lower Temp (C)	109.3	27.8	24.0		
Unconstrained HRR (kW)	423.3	0.0	0.0		
HRR (kW)	423.3	0.0	0.0		
Q* =	0.0318	-	-		
Visibility (m) at 2m	0.33	0.76	3.42		

FED gases on egress path = 0.006  
FED thermal on egress path = 0.022

2 min	40 sec (160 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)	1.024	1.120	1.749		
Upper Temp (C)	242.5	66.6	30.8		
Lower Temp (C)	112.8	28.6	24.0		
Unconstrained HRR (kW)	423.3	0.0	0.0		
HRR (kW)	423.3	0.0	0.0		
Q* =	0.0318	-	-		
Visibility (m) at 2m	0.32	0.71	3.09		

FED gases on egress path = 0.008  
FED thermal on egress path = 0.027

2 min	50 sec (170 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)	1.025	1.129	1.633		
Upper Temp (C)	244.5	67.9	31.1		
Lower Temp (C)	115.8	29.3	24.0		
Unconstrained HRR (kW)	423.3	0.0	0.0		
HRR (kW)	423.3	0.0	0.0		
Q* =	0.0318	-	-		
Visibility (m) at 2m	0.32	0.66	2.82		

FED gases on egress path = 0.010  
FED thermal on egress path = 0.033

3 min	00 sec (180 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)	1.026	1.136	1.524		
Upper Temp (C)	246.4	69.0	31.3		
Lower Temp (C)	118.3	29.9	24.1		
Unconstrained HRR (kW)	423.3	0.0	0.0		
HRR (kW)	423.3	0.0	0.0		
Q* =	0.0318	-	-		
Visibility (m) at 2m	0.32	0.63	2.59		

FED gases on egress path = 0.012  
FED thermal on egress path = 0.039

3 min	10 sec
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190 sec

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.026	1.145	1.232	
Upper Temp (C)	248.4	70.9	31.8	
Lower Temp (C)	120.4	30.4	24.1	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.32	0.60	2.40	

FED gases on egress path = 0.013  
FED thermal on egress path = 0.045

3 min 20 sec (200 sec)

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.027	1.144	1.323	
Upper Temp (C)	249.7	70.9	31.8	
Lower Temp (C)	122.2	30.9	24.2	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.32	0.58	2.23	

FED gases on egress path = 0.016  
FED thermal on egress path = 0.051

3 min 30 sec (210 sec)

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.027	1.145	1.232	
Upper Temp (C)	251.2	71.6	32.0	
Lower Temp (C)	123.8	31.2	24.2	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.32	0.56	2.10	

FED gases on egress path = 0.018  
FED thermal on egress path = 0.058

3 min 40 sec (220 sec)

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.027	1.136	1.146	
Upper Temp (C)	252.5	72.2	32.2	
Lower Temp (C)	125.2	31.3	24.2	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.32	0.55	1.97	

FED gases on egress path = 0.020  
FED thermal on egress path = 0.065

3 min 50 sec (230 sec)

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.027	1.126	1.101	
Upper Temp (C)	253.9	72.7	32.6	
Lower Temp (C)	126.3	31.4	24.3	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.32	0.54	1.83	

FED gases on egress path = 0.022  
FED thermal on egress path = 0.072

4 min 00 sec (240 sec)

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.027	1.118	1.055	
Upper Temp (C)	255.1	73.1	32.9	
Lower Temp (C)	127.4	31.6	24.3	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.32	0.53	1.70	

FED gases on egress path = 0.024  
FED thermal on egress path = 0.079

4 min 10 sec (250 sec)

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.026	1.111	1.030	
Upper Temp (C)	256.3	73.5	33.3	
Lower Temp (C)	128.6	31.8	24.4	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.33	0.52	1.59	

FED gases on egress path = 0.027  
FED thermal on egress path = 0.086

4 min 20 sec (260 sec)

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.026	1.105	0.996	
Upper Temp (C)	257.5	73.9	33.5	
Lower Temp (C)	129.8	32.1	24.5	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.33	0.51	1.50	

FED gases on egress path = 0.029  
FED thermal on egress path = 0.094

4 min 30 sec (270 sec)

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.026	1.099	0.964	
Upper Temp (C)	258.6	74.2	33.8	
Lower Temp (C)	131.1	32.4	24.5	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.33	0.51	1.42	

FED gases on egress path = 0.032  
FED thermal on egress path = 0.101

4 min 40 sec (280 sec)

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.025	1.094	0.932	
Upper Temp (C)	259.7	74.5	34.0	
Lower Temp (C)	132.5	32.8	24.6	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.33	0.50	1.35	

FED gases on egress path = 0.034  
FED thermal on egress path = 0.109

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4 min 50 sec  
(290 sec)

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	Room 1	Room 2	Room 3	Outside
Layer (m)	1.023	1.088	0.902	
Upper Temp (C)	260.8	74.7	34.2	
Lower Temp (C)	133.9	33.2	24.7	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.33	0.50	1.29	

FED gases on egress path = 0.037  
FED thermal on egress path = 0.117

5 min 00 sec  
(300 sec)

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.025	1.083	0.872	
Upper Temp (C)	261.8	75.0	34.4	
Lower Temp (C)	135.4	33.5	24.8	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.33	0.50	1.23	

FED gases on egress path = 0.039  
FED thermal on egress path = 0.124

5 min 10 sec  
(310 sec)

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.024	1.078	0.844	
Upper Temp (C)	262.8	75.3	34.6	
Lower Temp (C)	136.9	33.9	25.0	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.33	0.50	1.18	

FED gases on egress path = 0.042  
FED thermal on egress path = 0.132

5 min 20 sec  
(320 sec)

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.024	1.073	0.816	
Upper Temp (C)	263.9	75.5	34.8	
Lower Temp (C)	138.4	34.3	25.1	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.33	0.49	1.14	

FED gases on egress path = 0.044  
FED thermal on egress path = 0.140

5 min 30 sec  
(330 sec)

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.024	1.068	0.789	
Upper Temp (C)	264.9	75.8	34.9	
Lower Temp (C)	139.9	34.7	25.2	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.33	0.49	1.10	

FED gases on egress path = 0.047

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FED thermal on egress path = 0.149

5 min 40 sec  
(340 sec)

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.023	1.063	0.763	
Upper Temp (C)	265.8	76.0	35.1	
Lower Temp (C)	141.4	35.1	25.3	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.33	0.49	1.06	

FED gases on egress path = 0.050  
FED thermal on egress path = 0.157

5 min 50 sec  
(350 sec)

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.023	1.058	0.738	
Upper Temp (C)	266.8	76.3	35.2	
Lower Temp (C)	142.9	35.5	25.5	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.33	0.49	1.03	

FED gases on egress path = 0.052  
FED thermal on egress path = 0.165

6 min 00 sec  
(360 sec)

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.023	1.054	0.714	
Upper Temp (C)	267.7	76.5	35.4	
Lower Temp (C)	144.4	35.9	25.6	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.33	0.49	1.00	

FED gases on egress path = 0.055  
FED thermal on egress path = 0.174

6 min 10 sec  
(370 sec)

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.022	1.049	0.690	
Upper Temp (C)	268.7	76.7	35.5	
Lower Temp (C)	145.8	36.2	25.8	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.33	0.49	0.97	

FED gases on egress path = 0.058  
FED thermal on egress path = 0.182

6 min 20 sec  
(380 sec)

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.022	1.045	0.667	
Upper Temp (C)	269.6	76.9	35.6	
Lower Temp (C)	147.2	36.6	25.9	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.32	0.48	0.94	

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FED gases on egress path = 0.061  
FED thermal on egress path = 0.191

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.022	1.040	0.645	
Upper Temp (C)	270.5	77.0	35.7	
Lower Temp (C)	148.7	37.0	26.1	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.32	0.48	0.92	

FED gases on egress path = 0.063  
FED thermal on egress path = 0.199

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.022	1.036	0.624	
Upper Temp (C)	271.3	77.0	35.9	
Lower Temp (C)	150.0	37.3	26.2	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.32	0.48	0.90	

FED gases on egress path = 0.066  
FED thermal on egress path = 0.208

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.022	1.031	0.604	
Upper Temp (C)	272.2	77.0	36.0	
Lower Temp (C)	151.3	37.6	26.4	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.32	0.48	0.88	

FED gases on egress path = 0.069  
FED thermal on egress path = 0.217

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.021	1.025	0.584	
Upper Temp (C)	273.0	77.0	36.2	
Lower Temp (C)	152.6	37.9	26.6	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.32	0.48	0.86	

FED gases on egress path = 0.072  
FED thermal on egress path = 0.225

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.021	1.023	0.565	
Upper Temp (C)	273.8	77.2	36.3	
Lower Temp (C)	153.8	38.2	26.7	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.32	0.48	0.84	

FED gases on egress path = 0.075  
FED thermal on egress path = 0.234

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.021	1.024	0.546	
Upper Temp (C)	274.6	77.4	36.4	
Lower Temp (C)	154.9	38.5	26.9	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.32	0.47	0.82	

FED gases on egress path = 0.078  
FED thermal on egress path = 0.243

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.021	1.022	0.529	
Upper Temp (C)	275.4	77.6	36.5	
Lower Temp (C)	155.9	38.8	27.1	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.32	0.47	0.81	

FED gases on egress path = 0.081  
FED thermal on egress path = 0.252

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.021	1.021	0.512	
Upper Temp (C)	276.1	77.8	36.6	
Lower Temp (C)	156.9	39.0	27.3	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.32	0.47	0.79	

FED gases on egress path = 0.083  
FED thermal on egress path = 0.260

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.021	1.024	0.496	
Upper Temp (C)	276.8	78.2	36.7	
Lower Temp (C)	157.8	39.3	27.4	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.32	0.46	0.78	

FED gases on egress path = 0.086  
FED thermal on egress path = 0.270

	Room 1	Room 2	Room 3	Outside
Layer (m)	1.022	1.026	0.481	
Upper Temp (C)	276.8	78.5	36.8	
Lower Temp (C)	158.6	39.5	27.6	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.32	0.46	0.76	

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FED thermal on egress path = 0.279

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8 min	10 sec (490 sec)	Room 1	Room 2	Room 3	Outside
	Layer (m)	1.021	1.021	0.466	
	Upper Temp (C)	276.9	78.7	36.9	
	Lower Temp (C)	159.4	39.7	27.8	
	Unconstrained HRR (kW)	423.3	0.0	0.0	
	HRR (kW)	423.3	0.0	0.0	
	Q* =	0.0318	-	-	
	Visibility (m) at 2m	0.32	0.46	0.75	

FED gases on egress path = 0.093  
FED thermal on egress path = 0.288

8 min	20 sec (500 sec)	Room 1	Room 2	Room 3	Outside
	Layer (m)	1.021	1.025	0.452	
	Upper Temp (C)	277.0	79.2	37.0	
	Lower Temp (C)	160.1	40.0	27.9	
	Unconstrained HRR (kW)	423.3	0.0	0.0	
	HRR (kW)	423.3	0.0	0.0	
	Q* =	0.0318	-	-	
	Visibility (m) at 2m	0.32	0.46	0.74	

FED gases on egress path = 0.096  
FED thermal on egress path = 0.297

8 min	30 sec (510 sec)	Room 1	Room 2	Room 3	Outside
	Layer (m)	1.021	1.025	0.438	
	Upper Temp (C)	277.2	79.5	37.1	
	Lower Temp (C)	160.8	40.2	28.1	
	Unconstrained HRR (kW)	423.3	0.0	0.0	
	HRR (kW)	423.3	0.0	0.0	
	Q* =	0.0318	-	-	
	Visibility (m) at 2m	0.32	0.45	0.72	

FED gases on egress path = 0.099  
FED thermal on egress path = 0.307

8 min	40 sec (520 sec)	Room 1	Room 2	Room 3	Outside
	Layer (m)	1.021	1.021	0.425	
	Upper Temp (C)	277.0	79.8	37.3	
	Lower Temp (C)	161.5	40.4	28.2	
	Unconstrained HRR (kW)	423.3	0.0	0.0	
	HRR (kW)	423.3	0.0	0.0	
	Q* =	0.0318	-	-	
	Visibility (m) at 2m	0.32	0.45	0.71	

FED gases on egress path = 0.102  
FED thermal on egress path = 0.317

8 min	50 sec (530 sec)	Room 1	Room 2	Room 3	Outside
	Layer (m)	1.020	1.021	0.412	
	Upper Temp (C)	277.1	80.1	37.4	
	Lower Temp (C)	162.2	40.7	28.4	
	Unconstrained HRR (kW)	423.3	0.0	0.0	
	HRR (kW)	423.3	0.0	0.0	
	Q* =	0.0318	-	-	

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Visibility (m) at 2m 0.32 0.45 0.69

FED gases on egress path = 0.105  
FED thermal on egress path = 0.327

9 min	00 sec (540 sec)	Room 1	Room 2	Room 3	Outside
	Layer (m)	1.020	1.024	0.400	
	Upper Temp (C)	277.2	80.5	37.5	
	Lower Temp (C)	162.9	40.9	28.5	
	Unconstrained HRR (kW)	423.3	0.0	0.0	
	HRR (kW)	423.3	0.0	0.0	
	Q* =	0.0318	-	-	
	Visibility (m) at 2m	0.32	0.45	0.69	

FED gases on egress path = 0.108  
FED thermal on egress path = 0.336

9 min	10 sec (550 sec)	Room 1	Room 2	Room 3	Outside
	Layer (m)	1.019	1.020	0.389	
	Upper Temp (C)	277.5	80.7	37.6	
	Lower Temp (C)	163.6	41.1	28.7	
	Unconstrained HRR (kW)	423.3	0.0	0.0	
	HRR (kW)	423.3	0.0	0.0	
	Q* =	0.0318	-	-	
	Visibility (m) at 2m	0.32	0.45	0.68	

FED gases on egress path = 0.112  
FED thermal on egress path = 0.347

9 min	20 sec (560 sec)	Room 1	Room 2	Room 3	Outside
	Layer (m)	1.019	1.023	0.377	
	Upper Temp (C)	278.0	81.0	37.7	
	Lower Temp (C)	164.4	41.3	28.8	
	Unconstrained HRR (kW)	423.3	0.0	0.0	
	HRR (kW)	423.3	0.0	0.0	
	Q* =	0.0318	-	-	
	Visibility (m) at 2m	0.32	0.44	0.67	

FED gases on egress path = 0.115  
FED thermal on egress path = 0.357

9 min	30 sec (570 sec)	Room 1	Room 2	Room 3	Outside
	Layer (m)	1.019	1.021	0.367	
	Upper Temp (C)	278.5	81.2	37.8	
	Lower Temp (C)	165.1	41.5	28.9	
	Unconstrained HRR (kW)	423.3	0.0	0.0	
	HRR (kW)	423.3	0.0	0.0	
	Q* =	0.0318	-	-	
	Visibility (m) at 2m	0.32	0.44	0.66	

FED gases on egress path = 0.118  
FED thermal on egress path = 0.367

9 min	40 sec (580 sec)	Room 1	Room 2	Room 3	Outside
	Layer (m)	1.018	1.021	0.357	
	Upper Temp (C)	279.0	81.5	37.9	
	Lower Temp (C)	165.8	41.7	29.1	
	Unconstrained HRR (kW)	423.3	0.0	0.0	
	HRR (kW)	423.3	0.0	0.0	

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Q* =	0.0318	-	-	-
Visibility (m) at 2m	0.32	0.44	0.65	-

FED gases on egress path = 0.122  
FED thermal on egress path = 0.378

9 min	50 sec (590 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)		1.018	1.020	0.347	
Upper Temp (C)		279.5	81.6	38.0	
Lower Temp (C)		166.5	41.9	29.2	
Unconstrained HRR (kW)		423.3	0.0	0.0	
HRR (kW)		423.3	0.0	0.0	
Q* =		0.0318	-	-	
Visibility (m) at 2m		0.32	0.44	0.64	

FED gases on egress path = 0.125  
FED thermal on egress path = 0.388

10 min	00 sec (600 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)		1.018	1.019	0.337	
Upper Temp (C)		280.0	81.8	38.0	
Lower Temp (C)		167.2	42.1	29.3	
Unconstrained HRR (kW)		423.3	0.0	0.0	
HRR (kW)		423.3	0.0	0.0	
Q* =		0.0318	-	-	
Visibility (m) at 2m		0.32	0.44	0.63	

FED gases on egress path = 0.128  
FED thermal on egress path = 0.399

10 min	10 sec (610 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)		1.010	0.997	0.326	
Upper Temp (C)		280.7	83.9	38.2	
Lower Temp (C)		167.9	43.6	29.4	
Unconstrained HRR (kW)		423.3	0.0	0.0	
HRR (kW)		423.3	0.0	0.0	
Q* =		0.0318	-	-	
Visibility (m) at 2m		0.32	0.42	0.63	

FED gases on egress path = 0.132  
FED thermal on egress path = 0.410

10 min	20 sec (620 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)		1.004	0.977	0.316	
Upper Temp (C)		281.8	85.5	38.4	
Lower Temp (C)		169.7	45.0	29.5	
Unconstrained HRR (kW)		423.3	0.0	0.0	
HRR (kW)		423.3	0.0	0.0	
Q* =		0.0318	-	-	
Visibility (m) at 2m		0.32	0.40	0.62	

FED gases on egress path = 0.135  
FED thermal on egress path = 0.422

10 min	30 sec (630 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)		1.003	0.960	0.306	
Upper Temp (C)		282.9	86.5	38.6	
Lower Temp (C)		172.3	46.3	29.7	
Unconstrained HRR (kW)		423.3	0.0	0.0	

HRR (kW)	423.3	0.0	0.0
Q* =	0.0318	-	-
Visibility (m) at 2m	0.32	0.39	0.61

FED gases on egress path = 0.139  
FED thermal on egress path = 0.434

10 min	40 sec (640 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)		1.005	0.944	0.296	
Upper Temp (C)		283.9	87.1	38.8	
Lower Temp (C)		175.3	47.3	29.8	
Unconstrained HRR (kW)		423.3	0.0	0.0	
HRR (kW)		423.3	0.0	0.0	
Q* =		0.0318	-	-	
Visibility (m) at 2m		0.31	0.38	0.60	

FED gases on egress path = 0.143  
FED thermal on egress path = 0.447

10 min	50 sec (650 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)		1.005	0.928	0.287	
Upper Temp (C)		284.8	87.6	39.1	
Lower Temp (C)		178.1	48.2	29.9	
Unconstrained HRR (kW)		423.3	0.0	0.0	
HRR (kW)		423.3	0.0	0.0	
Q* =		0.0318	-	-	
Visibility (m) at 2m		0.31	0.37	0.59	

FED gases on egress path = 0.147  
FED thermal on egress path = 0.461

11 min	00 sec (660 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)		1.002	0.914	0.278	
Upper Temp (C)		285.7	87.9	39.3	
Lower Temp (C)		180.4	49.0	30.1	
Unconstrained HRR (kW)		423.3	0.0	0.0	
HRR (kW)		423.3	0.0	0.0	
Q* =		0.0318	-	-	
Visibility (m) at 2m		0.31	0.36	0.58	

FED gases on egress path = 0.152  
FED thermal on egress path = 0.474

11 min	10 sec (670 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)		0.998	0.900	0.270	
Upper Temp (C)		286.4	88.2	39.3	
Lower Temp (C)		182.3	49.6	30.2	
Unconstrained HRR (kW)		423.3	0.0	0.0	
HRR (kW)		423.3	0.0	0.0	
Q* =		0.0318	-	-	
Visibility (m) at 2m		0.31	0.36	0.57	

FED gases on egress path = 0.156  
FED thermal on egress path = 0.488

11 min	20 sec (680 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)		0.992	0.886	0.263	
Upper Temp (C)		287.0	88.5	39.7	
Lower Temp (C)		184.1	50.2	30.4	

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Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.31	0.34	0.55	

FED gases on egress path = 0.160  
FED thermal on egress path = 0.502

11 min	30 sec (690 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)		0.987	0.872	0.255	
Upper Temp (C)		287.5	88.7	40.0	
Lower Temp (C)		185.7	50.7	30.5	
Unconstrained HRR (kW)		423.3	0.0	0.0	
HRR (kW)		423.3	0.0	0.0	
Q* =		0.0318	-	-	
Visibility (m) at 2m		0.31	0.34	0.55	

FED gases on egress path = 0.165  
FED thermal on egress path = 0.515

11 min	40 sec (700 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)		0.980	0.858	0.248	
Upper Temp (C)		288.0	88.8	40.2	
Lower Temp (C)		187.2	51.1	30.7	
Unconstrained HRR (kW)		423.3	0.0	0.0	
HRR (kW)		423.3	0.0	0.0	
Q* =		0.0318	-	-	
Visibility (m) at 2m		0.30	0.34	0.54	

FED gases on egress path = 0.170  
FED thermal on egress path = 0.529

11 min	50 sec (710 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)		0.973	0.845	0.242	
Upper Temp (C)		288.4	89.0	40.4	
Lower Temp (C)		188.7	51.5	30.8	
Unconstrained HRR (kW)		423.3	0.0	0.0	
HRR (kW)		423.3	0.0	0.0	
Q* =		0.0318	-	-	
Visibility (m) at 2m		0.30	0.33	0.53	

FED gases on egress path = 0.175  
FED thermal on egress path = 0.544

12 min	00 sec (720 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)		0.966	0.832	0.236	
Upper Temp (C)		288.9	89.1	40.5	
Lower Temp (C)		190.1	51.9	31.0	
Unconstrained HRR (kW)		423.3	0.0	0.0	
HRR (kW)		423.3	0.0	0.0	
Q* =		0.0318	-	-	
Visibility (m) at 2m		0.30	0.33	0.52	

FED gases on egress path = 0.180  
FED thermal on egress path = 0.558

12 min	10 sec (730 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)		0.959	0.820	0.230	
Upper Temp (C)		289.3	89.3	40.7	

Lower Temp (C)	191.5	52.2	31.1	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.30	0.33	0.51	

FED gases on egress path = 0.185  
FED thermal on egress path = 0.572

12 min	20 sec (740 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)		0.952	0.808	0.225	
Upper Temp (C)		289.6	89.4	40.9	
Lower Temp (C)		192.8	52.5	31.3	
Unconstrained HRR (kW)		423.3	0.0	0.0	
HRR (kW)		423.3	0.0	0.0	
Q* =		0.0318	-	-	
Visibility (m) at 2m		0.30	0.32	0.50	

FED gases on egress path = 0.190  
FED thermal on egress path = 0.586

12 min	30 sec (750 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)		0.944	0.796	0.220	
Upper Temp (C)		290.0	89.5	41.1	
Lower Temp (C)		194.1	52.9	31.4	
Unconstrained HRR (kW)		423.3	0.0	0.0	
HRR (kW)		423.3	0.0	0.0	
Q* =		0.0318	-	-	
Visibility (m) at 2m		0.29	0.32	0.49	

FED gases on egress path = 0.195  
FED thermal on egress path = 0.601

12 min	40 sec (760 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)		0.937	0.784	0.215	
Upper Temp (C)		290.3	89.6	41.2	
Lower Temp (C)		195.4	53.2	31.6	
Unconstrained HRR (kW)		423.3	0.0	0.0	
HRR (kW)		423.3	0.0	0.0	
Q* =		0.0318	-	-	
Visibility (m) at 2m		0.29	0.31	0.48	

FED gases on egress path = 0.201  
FED thermal on egress path = 0.615

12 min	50 sec (770 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)		0.929	0.773	0.210	
Upper Temp (C)		290.7	89.8	41.4	
Lower Temp (C)		196.7	53.4	31.7	
Unconstrained HRR (kW)		423.3	0.0	0.0	
HRR (kW)		423.3	0.0	0.0	
Q* =		0.0318	-	-	
Visibility (m) at 2m		0.29	0.31	0.48	

FED gases on egress path = 0.206  
FED thermal on egress path = 0.630

13 min	00 sec (780 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)		0.922	0.762	0.206	

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Upper Temp (C)	291.0	89.9	41.8
Lower Temp (C)	197.9	53.7	31.8
Unconstrained HRR (kW)	423.3	0.0	0.0
HRR (kW)	423.3	0.0	0.0
Q* =	0.0318	-	-
Visibility (m) at 2m	0.29	0.31	0.47

FED gases on egress path = 0.212  
FED thermal on egress path = 0.644

13 min	10 sec (790 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)	0.915	0.752	0.202		
Upper Temp (C)	291.3	90.0	41.7		
Lower Temp (C)	199.1	54.0	32.0		
Unconstrained HRR (kW)	423.3	0.0	0.0		
HRR (kW)	423.3	0.0	0.0		
Q* =	0.0318	-	-		
Visibility (m) at 2m	0.29	0.30	0.46		

FED gases on egress path = 0.218  
FED thermal on egress path = 0.659

13 min	20 sec (800 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)	0.907	0.742	0.199		
Upper Temp (C)	291.6	90.1	41.8		
Lower Temp (C)	200.3	54.2	32.1		
Unconstrained HRR (kW)	423.3	0.0	0.0		
HRR (kW)	423.3	0.0	0.0		
Q* =	0.0318	-	-		
Visibility (m) at 2m	0.28	0.30	0.45		

FED gases on egress path = 0.224  
FED thermal on egress path = 0.674

13 min	30 sec (810 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)	0.900	0.732	0.195		
Upper Temp (C)	291.9	90.2	42.0		
Lower Temp (C)	201.4	54.5	32.2		
Unconstrained HRR (kW)	423.3	0.0	0.0		
HRR (kW)	423.3	0.0	0.0		
Q* =	0.0318	-	-		
Visibility (m) at 2m	0.28	0.30	0.45		

FED gases on egress path = 0.230  
FED thermal on egress path = 0.689

13 min	40 sec (820 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)	0.893	0.723	0.192		
Upper Temp (C)	292.2	90.3	42.1		
Lower Temp (C)	202.5	54.7	32.4		
Unconstrained HRR (kW)	423.3	0.0	0.0		
HRR (kW)	423.3	0.0	0.0		
Q* =	0.0318	-	-		
Visibility (m) at 2m	0.28	0.30	0.44		

FED gases on egress path = 0.236  
FED thermal on egress path = 0.703

13 min	50 sec (830 sec)	Room 1	Room 2	Room 3	Outside
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Layer (m)	0.887	0.714	0.189
Upper Temp (C)	292.5	90.5	42.2
Lower Temp (C)	203.6	55.0	32.5
Unconstrained HRR (kW)	423.3	0.0	0.0
HRR (kW)	423.3	0.0	0.0
Q* =	0.0318	-	-
Visibility (m) at 2m	0.28	0.29	0.43

FED gases on egress path = 0.242  
FED thermal on egress path = 0.718

14 min	00 sec (840 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)	0.880	0.705	0.186		
Upper Temp (C)	292.7	90.6	42.4		
Lower Temp (C)	204.6	55.2	32.6		
Unconstrained HRR (kW)	423.3	0.0	0.0		
HRR (kW)	423.3	0.0	0.0		
Q* =	0.0318	-	-		
Visibility (m) at 2m	0.28	0.29	0.43		

FED gases on egress path = 0.248  
FED thermal on egress path = 0.733

14 min	10 sec (850 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)	0.874	0.697	0.183		
Upper Temp (C)	293.0	90.7	42.5		
Lower Temp (C)	205.6	55.4	32.7		
Unconstrained HRR (kW)	423.3	0.0	0.0		
HRR (kW)	423.3	0.0	0.0		
Q* =	0.0318	-	-		
Visibility (m) at 2m	0.27	0.29	0.42		

FED gases on egress path = 0.255  
FED thermal on egress path = 0.748

14 min	20 sec (860 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)	0.811	0.692	0.182		
Upper Temp (C)	303.3	90.7	42.6		
Lower Temp (C)	168.4	55.6	32.8		
Unconstrained HRR (kW)	423.3	0.0	0.0		
HRR (kW)	423.3	0.0	0.0		
Q* =	0.0318	-	-		
Visibility (m) at 2m	0.28	0.29	0.41		

FED gases on egress path = 0.261  
FED thermal on egress path = 0.763

14 min	30 sec (870 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)	0.803	0.690	0.181		
Upper Temp (C)	302.3	90.9	42.7		
Lower Temp (C)	156.2	55.8	32.9		
Unconstrained HRR (kW)	423.3	0.0	0.0		
HRR (kW)	423.3	0.0	0.0		
Q* =	0.0318	-	-		
Visibility (m) at 2m	0.27	0.28	0.41		

FED gases on egress path = 0.268  
FED thermal on egress path = 0.779

14 min	40 sec (880 sec)	Room 1	Room 2	Room 3	Outside
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Layer (m)	0.803	0.688	0.179
Upper Temp (C)	301.2	91.2	43.4
Lower Temp (C)	154.1	56.2	33.1
Unconstrained HRR (kW)	423.3	0.0	0.0
HRR (kW)	423.3	0.0	0.0
Q* =	0.0318	-	-
Visibility (m) at 2m	0.27	0.28	0.40

FED gases on egress path = 0.275  
FED thermal on egress path = 0.794

14 min 50 sec  
(890 sec) Room 1 Room 2 Room 3 Outside

Layer (m)	0.803	0.687	0.177
Upper Temp (C)	300.9	91.2	42.9
Lower Temp (C)	153.7	56.2	33.1
Unconstrained HRR (kW)	423.3	0.0	0.0
HRR (kW)	423.3	0.0	0.0
Q* =	0.0318	-	-
Visibility (m) at 2m	0.26	0.28	0.40

FED gases on egress path = 0.281  
FED thermal on egress path = 0.809

15 min 00 sec  
(900 sec) Room 1 Room 2 Room 3 Outside

Layer (m)	0.802	0.685	0.175
Upper Temp (C)	300.9	91.4	43.0
Lower Temp (C)	153.8	56.4	33.2
Unconstrained HRR (kW)	423.3	0.0	0.0
HRR (kW)	423.3	0.0	0.0
Q* =	0.0318	-	-
Visibility (m) at 2m	0.26	0.27	0.39

FED gases on egress path = 0.288  
FED thermal on egress path = 0.825

15 min 10 sec  
(910 sec) Room 1 Room 2 Room 3 Outside

Layer (m)	0.800	0.683	0.173
Upper Temp (C)	301.0	91.5	43.1
Lower Temp (C)	154.0	56.5	33.3
Unconstrained HRR (kW)	423.3	0.0	0.0
HRR (kW)	423.3	0.0	0.0
Q* =	0.0318	-	-
Visibility (m) at 2m	0.26	0.27	0.39

FED gases on egress path = 0.296  
FED thermal on egress path = 0.840

15 min 20 sec  
(920 sec) Room 1 Room 2 Room 3 Outside

Layer (m)	0.799	0.681	0.172
Upper Temp (C)	301.1	91.6	43.2
Lower Temp (C)	154.3	56.7	33.4
Unconstrained HRR (kW)	423.3	0.0	0.0
HRR (kW)	423.3	0.0	0.0
Q* =	0.0318	-	-
Visibility (m) at 2m	0.26	0.27	0.38

FED gases on egress path = 0.303  
FED thermal on egress path = 0.856

15 min 30 sec

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(930 sec)	Room 1	Room 2	Room 3	Outside
Layer (m)	0.797	0.679	0.170	
Upper Temp (C)	301.3	91.8	43.4	
Lower Temp (C)	154.6	56.9	33.5	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.26	0.27	0.37	

FED gases on egress path = 0.310  
FED thermal on egress path = 0.871

15 min 40 sec  
(940 sec) Room 1 Room 2 Room 3 Outside

Layer (m)	0.796	0.678	0.169
Upper Temp (C)	301.5	91.9	43.4
Lower Temp (C)	154.9	57.0	33.6
Unconstrained HRR (kW)	423.3	0.0	0.0
HRR (kW)	423.3	0.0	0.0
Q* =	0.0318	-	-
Visibility (m) at 2m	0.25	0.26	0.37

FED gases on egress path = 0.318  
FED thermal on egress path = 0.887

15 min 50 sec  
(950 sec) Room 1 Room 2 Room 3 Outside

Layer (m)	0.795	0.676	0.168
Upper Temp (C)	301.7	92.0	43.4
Lower Temp (C)	155.3	57.2	33.7
Unconstrained HRR (kW)	423.3	0.0	0.0
HRR (kW)	423.3	0.0	0.0
Q* =	0.0318	-	-
Visibility (m) at 2m	0.25	0.26	0.36

FED gases on egress path = 0.325  
FED thermal on egress path = 0.903

16 min 00 sec  
(960 sec) Room 1 Room 2 Room 3 Outside

Layer (m)	0.793	0.674	0.167
Upper Temp (C)	301.9	92.1	43.6
Lower Temp (C)	155.6	57.3	33.8
Unconstrained HRR (kW)	423.3	0.0	0.0
HRR (kW)	423.3	0.0	0.0
Q* =	0.0318	-	-
Visibility (m) at 2m	0.25	0.26	0.36

FED gases on egress path = 0.333  
FED thermal on egress path = 0.919

16 min 10 sec  
(970 sec) Room 1 Room 2 Room 3 Outside

Layer (m)	0.792	0.672	0.166
Upper Temp (C)	302.2	92.3	43.7
Lower Temp (C)	156.0	57.5	33.9
Unconstrained HRR (kW)	423.3	0.0	0.0
HRR (kW)	423.3	0.0	0.0
Q* =	0.0318	-	-
Visibility (m) at 2m	0.25	0.26	0.36

FED gases on egress path = 0.341  
FED thermal on egress path = 0.935



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20 min (720 sec)

	Room 1	Room 2	Room 3	Outside
Layer (m)	0.791	0.669	0.164	
Upper Temp (C)	302.4	92.4	43.8	
Lower Temp (C)	156.3	57.6	34.0	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.25	0.26	0.35	

FED gases on egress path = 0.349  
FED thermal on egress path = 0.951

16 min 30 sec (990 sec)

	Room 1	Room 2	Room 3	Outside
Layer (m)	0.789	0.669	0.164	
Upper Temp (C)	302.6	92.5	43.9	
Lower Temp (C)	156.7	57.8	34.0	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.25	0.25	0.35	

FED gases on egress path = 0.357  
FED thermal on egress path = 0.967

16 min 40 sec (1000 sec)

	Room 1	Room 2	Room 3	Outside
Layer (m)	0.788	0.667	0.163	
Upper Temp (C)	302.8	92.6	44.0	
Lower Temp (C)	157.0	57.9	34.1	
Unconstrained HRR (kW)	423.3	0.0	0.0	
HRR (kW)	423.3	0.0	0.0	
Q* =	0.0318	-	-	
Visibility (m) at 2m	0.25	0.25	0.34	

FED gases on egress path = 0.365  
FED thermal on egress path = 0.983

=====  
Event Log  
=====  
FED(CO) Exceeded 0.3 at 917.0 Seconds.  
FED(thermal) Exceeded 0.3 at 503.0 Seconds.  
FED(thermal) Exceeded 0.3 at 503.0 Seconds.  
Simulation Finished.  
Sprinkler Effectiveness 1  
600 sec. Vent 2-4-2 closed by user.  
120 sec. Vent 2-4-2 opened by user.  
Fire HRR is controlled by sprinkler  
95 Sec. Sprinkler 1 responded.  
29 sec. Visibility at 2m above floor reduced to 10 m in room 1  
30 sec. Smoke detector 1 operates in room 1  
0 sec. Item 1 description ignited.  
Iteration 1  
  
=====  
Computer Run-Time = 10.4 seconds.  
=====

#### C.4 ASET for Robustness Check RC1

Robustness Check RC1 utilise Challenging Fire CF1 with the failure of the smoke exhaust system. The fire is subject to (quick response) sprinkler control.

Table 23 - Sprinkler Activation time for CF1

(Quick Response) Sprinkler activation in FDS (s)	Sprinkler activation modelled for HRR control (s)
265	265

The graph below shows the comparison between the HRR output of the FDS burner modelled in RC1 against that specified in C/VM2 (0.0469t<sup>2</sup>).

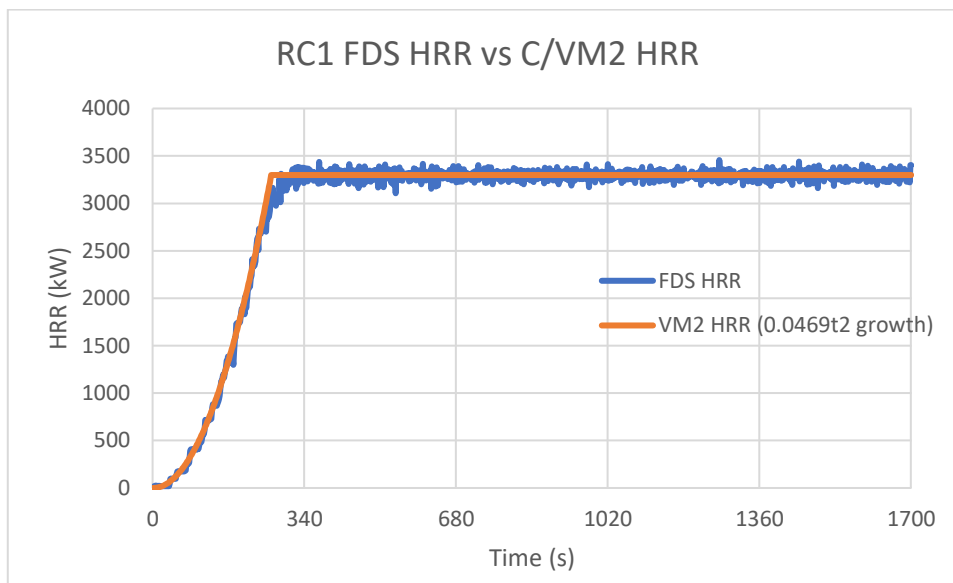


Figure 26 - RC1 FDS HRR v.s. VM2 HRR

#### C.4.1 RC1 ASET Summary

Tenability was assessed by FEDco slice files located 2m above each floor. The table below showed the tenability for each floor. As agreed in the Zone 1 FEB, only FEDco will be assessed.

Table 24 - RC1 ASET

Floor Level	Location	Time @ FED <sub>co</sub> = 0.3 (s)	ASET (s)
GF	Retail	>1700	>1700
	SW Entry to Mall	>1700	
	Main Entry (Esk St)	>1700	
	SE Exit to Tay St	>1700	
L1	Retail	1610	1610
	Entry to Carpark	1644	1644
	Entry to Stair 3	1686	1686

Floor Level	Location	Time @ FED <sub>co</sub> = 0.3 (s)	ASET (s)
	Entry to Stair 4	1615	1615

The images below showed FDS Smokeview FEDco slice file at 2 metres above each level.

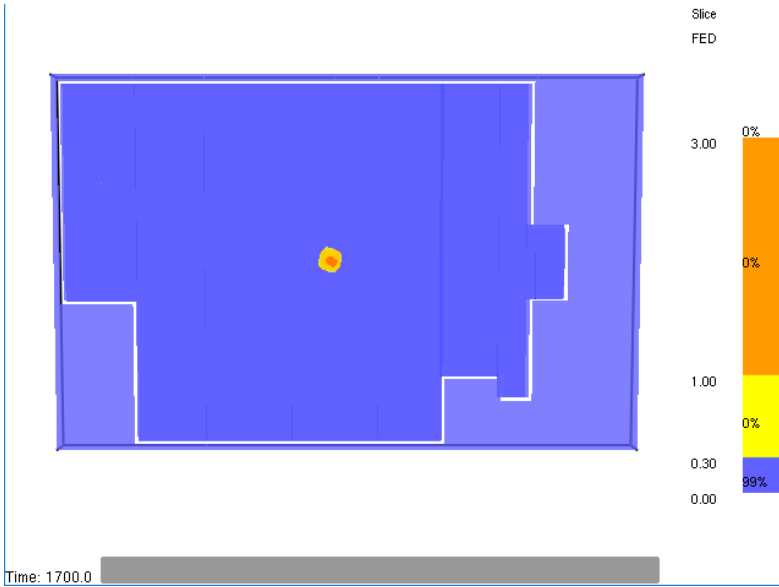


Figure 27 - RC1 FEDco slice file at 2.0 m above Ground Floor Anchor at 1700 s

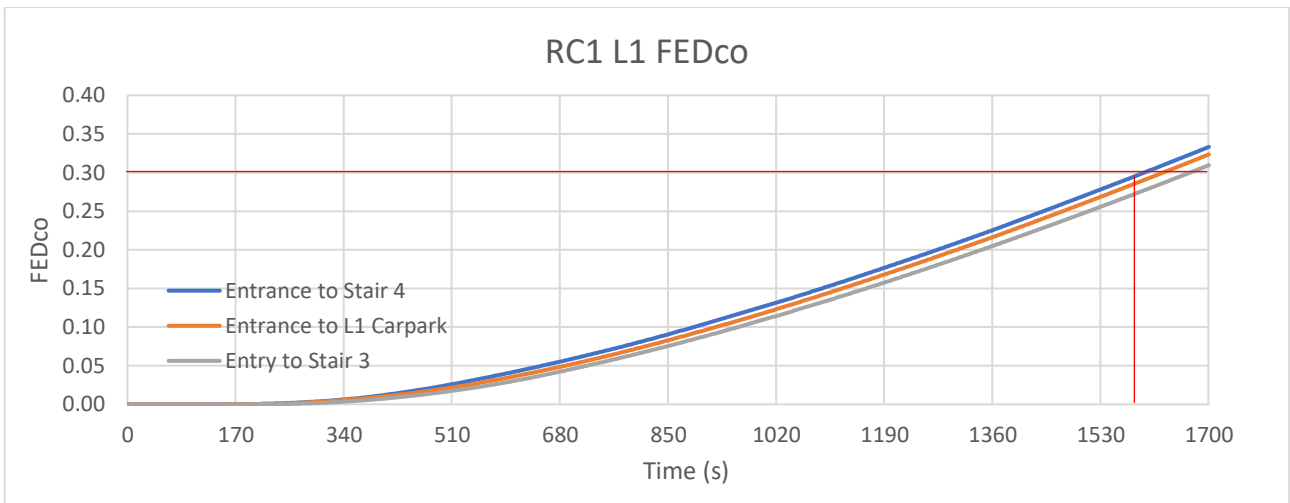


Figure 28 - RC1 FEDco measured at 2.0 m above Level 1 floor at main exits

### C.4.2 RC1 ASET vs RSET Assessment

Table 25 - RC1 ASET vs RSET Summary

Floor Level	Location <sup>1</sup>	ASET (s)	RSET <sup>1</sup> (s)		ASET > RSET
			Base Case	Non-Base Case	
GF	GF Anchor	>1700	212	202	Yes
	N Circulation <sup>2</sup>	>1700	-	534	Yes
L1	L1 Anchor	1610	285	351	Yes
	Entry to Carpark	1644	285	287	Yes
	L1 Stair 3 Landing <sup>3</sup>	1686	281	273	Yes
	L1 Anchor-S BoH <sup>4</sup>	1615	285	243	Yes
	L0 Stair 3 Landing <sup>5</sup>	1610	298	290	Yes
	L0 Stair 4 Landing <sup>6</sup>	1644	270	276	Yes
	Corridor <sup>7</sup>	>1700	-	1540	Yes
L2	Childcare Centre	>1700	786		Yes

Explanatory Notes:

- 1) Location is the space represented as nodes in EvacuationNZ.
- 2) 'N Circulation' is the node that corresponds to the space precede the final exit from the Zone 2 ground floor mall space and is taken as the node where the last person leaves GF Anchor.
- 3) 'L1 Stair 3 Landing' is the node that corresponds to the lobby space before entering into Stair 3 which indicates the queuing clear time preceding stair 3.
- 4) 'L1 Anchor-S BoH' is the node that corresponds to the lobby space before entering into Stair 4 which indicate the queuing clear time preceding stair 4.
- 5) 'L0 Stair3 Landing' is the node that corresponds to the space precede the final exit from Stair 3 (i.e. time to clear L1 Anchor north stairwell) which is shared by the occupants from L2 Childcare space.
- 6) 'L0 Stair4 Landing' is the node that corresponds to the space precede the final exit from Stair 4 (i.e. time to clear L1 Anchor south stairwell).
- 7) 'Corridor' is the node that corresponds to the space precede the final exit from Zone 3 Carpark building.

As shown above in Table 25, ASET is greater than RSET for all locations.

## Appendix D Smoke Barrier (Upper Layer Temperature) Assessment

The following details the assessment of the smoke barrier located between the Anchor building and the adjacent mall/carpark building.

The worst-case scenario is Challenging Fire 2 where the fire is located near the mall opening on the ground floor. The temperature is monitored near the Zone 1 Anchor west elevation.

Table 26 - CF1, CF2 and RC1 Upper Layer Temperature

Challenging Fire	Floor Level	Upper Layer Temperature (°C)
CF1	GF (between Anchor and Mall)	<50
	L1 (between Anchor and Carpark)	<50
CF2	GF (between Anchor and Mall)	<117
	L1 (between Anchor and Carpark)	<30
RC1	GF (between Anchor and Mall)	<40
	L1 (between Anchor and Carpark)	<80

The slice files below in Figure 29, Figure 30 and Figure 31 showed the upper layer temperature against time for CF1, CF2 and RC1.

As shown in Table 26 above and the figures below, the temperature between the ground floor anchor and mall smoke barrier are less than 200°C for the duration of the model run (1700 seconds) for all three scenarios. Thus, it is reasonable to assume the smoke barrier between anchor and mall would remain in place for the duration of the RSET. The temperature between the level 1 anchor and level 1 carpark are also less than 200°C for the duration of the model run for all three scenarios and is reasonable to assume the smoke barrier between level 1 anchor and carpark would remain in place for the duration of the RSET.

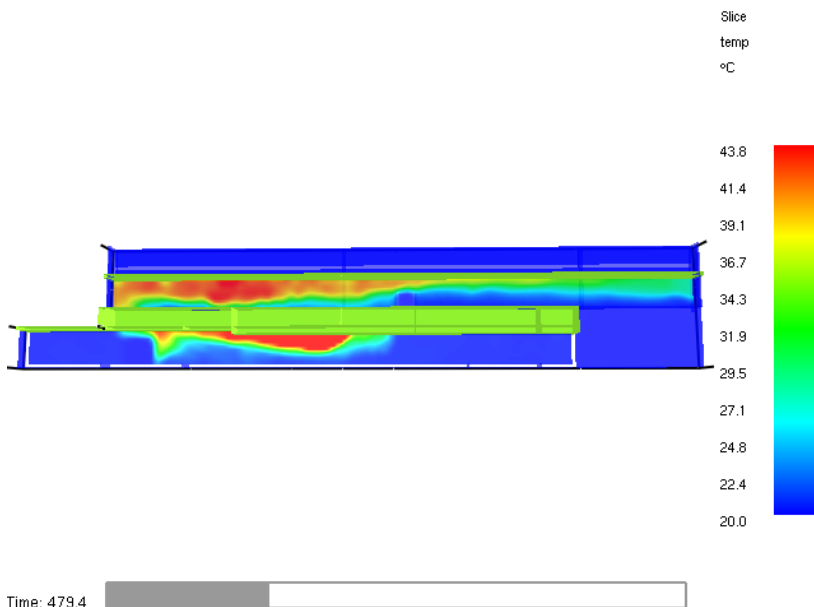


Figure 29 - CF1 Temperature slice file adjacent the west wall at 479 s (worst case)

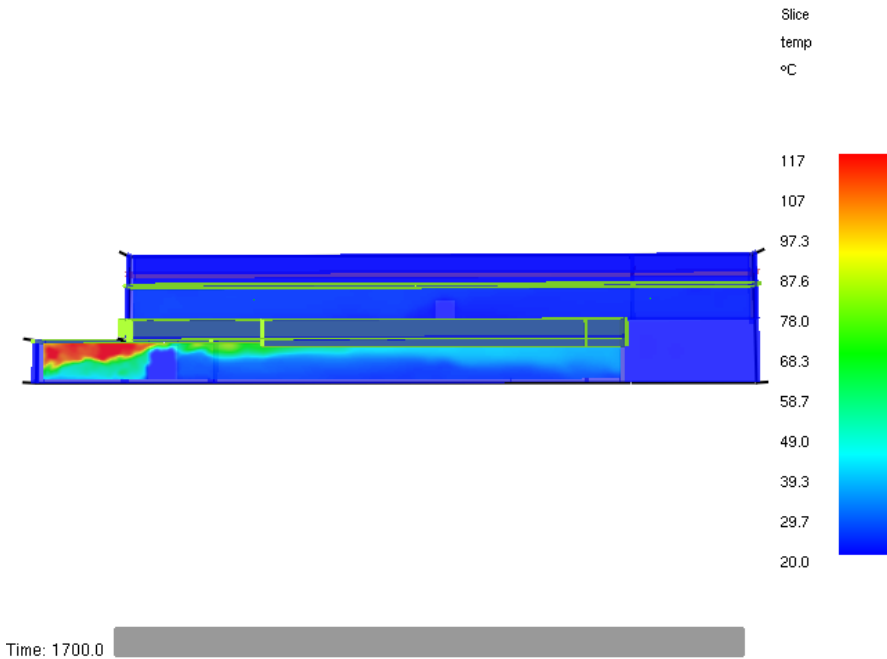


Figure 30 - CF2 Temperature slice file adjacent the west wall at 1700 sec

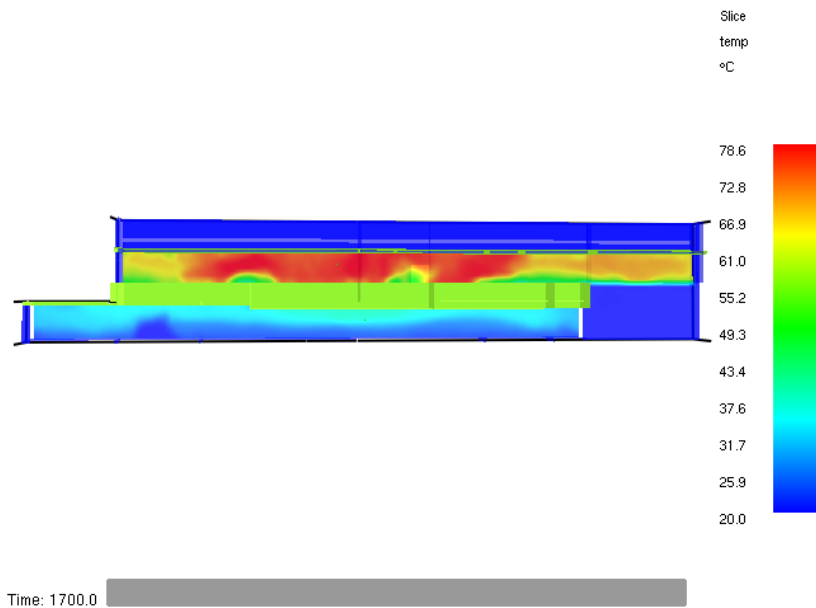


Figure 31 - RC1 Temperature slice file adjacent the west wall at 1700 sec

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## Appendix E Correspondence

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HWCP Zone 3 FEB Fire Peer Review Queries Response

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HolmesFire Q&A LOG

<b>Project:</b>	HWCP Invercargill CBD Development	<b>Design Stage:</b>	FEB Peer Review
<b>Document:</b>	<b>Zone 1 (Anchor) Fire Engineering Brief</b>		<b>Rev A dated 24 June 2019</b>
<b>Company:</b>		<b>Reviewer (s):</b>	MacDonald Barnett / Michael Dunn

No.	Item	Review Comments Date: 26/06/2019	Response Comments Date: 04/07/2019
1)	BOH Areas Anchor tenant	<ul style="list-style-type: none"> <li>The fire design is based on a Class A sprinkler water supply and on this basis there is no requirement for HS fire spread to neighbouring property to be considered. Under C/VM2 this imposes a storage height limit of 3 metres.</li> <li>How is storage to be managed in the BOH areas of the anchor tenant, or is a fire separation between BOH and retail areas to be provided?</li> </ul>	<p>The design for the BOH areas is still under discussion with the proposed tenant. If the storage height exceeds the 3 m limit, fire separation will be provided between the BOH and retail areas. Any such firewall will be 60 min rated.</p> <p><b>Date 1-8-2019 MacDonald Barnett</b> Peer review FEB query closed out</p>
2)	Fire Resistance	<ul style="list-style-type: none"> <li>Confirm that Clause 2.5 will be addressed in respect to evaluating fire resistance of the enclosed egress stairs and fire separation between the childcare centre and the remainder of the development.</li> </ul>	<p>The fire resistance rating for the anchor stairwells will be assessed either by using burnout calculation or 3 times the RSET as per Clause 2.5.</p> <p><b>Date 1-8-2019 MacDonald Barnett</b> Peer review FEB query closed out</p>



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No.	Item	Review Comments Date: 26/06/2019	Response Comments Date: 04/07/2019
3)	Challenging Fire 3	<ul style="list-style-type: none"> <li>We consider that the zone model with fire modelled in the kitchen should have the adjacent area being modelled as an equivalent area of the adjoining corridor / linkway and not half the entire floor area. Given the building is sprinkler protected it is reasonable to assume that the partitions will remain in place.</li> <li>Under C/VM2 we believe it is reasonable to model adjacent room /s with the doors open as per C/VM2 2.2.1e.</li> </ul>	<p>Noted. The zone model for the childcare will include the kitchen (room of fire origin), central corridor and potentially one more room with tenability measured in the central corridor. Doors connecting these rooms will be modelled as open.</p> <p>We do not fundamentally agree this is necessary under C/VM2 as they will be unrated barriers and therefore no criteria apply to their performance. We are modelling as requested simply to enable us to progress.</p> <p><b>Date 1-8-2019 MacDonald Barnett</b>          Peer review FEB query closed out</p>

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HWCP Zone 3 FEB Fire Peer Review Queries Response

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HolmesFire Q&A LOG

END OF REVIEW COMMENTS

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**FIRE**

**EMERGENCY**

NEW ZEALAND

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Paul Richards  
Fire and Emergency New Zealand  
Phone: 03 372 8613  
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BUILDING CONSENT NUMBER

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Amy Chao  
Holmes Fire LP  
By Email

23 July 2019

Dear Amy,

**Re: Fire Engineering Brief for HWCP Invercargill CBD Development (Our Reference: FEB 13041- Rev 1)**

**Status: Ongoing**

Thank you for the additional information provided on the above project. Fire and Emergency understands that the project involves the redevelopment of a whole city block bounded by Tay Street, Dee Street, Kelvin Street and Esk Street.

The complex will consist of two levels of retail and dining tenancies, a multi-level carpark building and an office tower which may form a separate stage. The existing Kelvin hotel on this block is not part of this development, however the existing Readings cinema complex will be connected to the development. With regards to development staging, the complex has been subdivided into multiple zones, namely:

- Zone 1            The anchor tenancy space and the rooftop childcare center
- Zone 2            The ground and first floor mall area
- Zone 3            The carparking building

The complex is intended to operate on an all-out evacuation scheme however smoke detection may operate on a double knock arrangement before alarm activation.

The master FEB is unusual in that it covers only those aspects that are intended to apply to the entire complex. It is effectively a master document and additional FEB documentation is intended to be issued as the project develops.

The Zone 3 FEB covers design aspects (such as design fire locations) that are applicable to the carpark building. The Zone 1 FEB covers design aspects of the anchor tenancy. These documents are intended to be read in conjunction with the Zone 0 FEB.

The FEB report proposes to use C/VM2 to demonstrate that the fire design for the building will meet the performance requirements of the New Zealand Building Code. This letter outlines the Fire and Emergency position as a stakeholder in the building design process.

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Referenced Information

Item	Title	Date	Revision
Emails	Preliminary meeting and email discussion on fire fighting facilities and requirements for complex	19 October 2018 to 8 May 2019	-
FEB	HWCP Invercargill CBD Development Master Fire Engineering Brief	19 May 2019	A
Meetings and meeting minutes	Two weekly meetings on design progress	Commenced 23 May 2019	-
Peer review correspondence	Fire Peer Review of FEB – HWCP Invercargill CBD Development, Edendale	30 May 2019	-
FEB response	HWCP Invercargill CBD Development Master Fire Engineering Brief response	13 June 2019	-
FEB	HWCP Invercargill CBD Development Zone 3 (Carpark) Fire Engineering Brief	14 June 2019	A
FEB	HWCP Invercargill CBD Development Zone 1 (Anchor tenancy) Fire Engineering Brief	24 June 2019	A
FEB response	HWCP Invercargill CBD Development Master Fire Engineering Brief response	4 July 2019	-

The comments from the peer reviewer are noted and concurred with. Fire and Emergency has reviewed the FEB documentation identified above and offers additional comments in the attached list:

To avoid unnecessary iterations of the FEB process, Fire and Emergency welcomes discussion on any of the above items, however a written response is required for our records. While we recommend that the final revision of the FEB includes all stakeholder comments, the impact of the items identified above are not considered sufficient to warrant a revision of the FEB documentation on their own. However, should additional items be identified by other stakeholders then it is recommended that the FEB be revised to address all issues.

Our review of the information provided has focused on the requirements of C/VM2 and is intended to provide guidance to reduce the consent risks associated with undertaking verification method design. No assessment against the requirements of the acceptable solutions has been undertaken. Also, please note that this advice does not imply a technical verification of the information provided.

If you have any questions related to the above, please do not hesitate to contact me.

Sincerely,



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Paul Richards  
Fire Engineering Unit

cc:  
Steve McCarthy  
Fire and Emergency Engineering Unit  
Mike Dunn  
Murray Milne-Maresca

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Attached: FEB comments register

FEB Comments Register – FENZ ref: FEB 13041

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Designers Reference: 136249

Item	Fire and Emergency NZ Comment	Designers Response	Close Out Date
<b>Building Code Items</b>			
The following items have been identified as they directly relate to compliance with the Building Code			
<b>Master FEB Comments</b>			
1.1	<p><b>4 June 2019 – Project staging</b></p> <p>While we acknowledge and support the proposed approach of this FEB we note that some subtleties of the design may only become apparent once more information is available. While the following comments have been made on the basis of the information provided, please note that in specific instances these decisions may have to be revised once greater detail is available.</p> <p>One example of this is the proposal for a medium fire in the carpark zone. While this may be appropriate for the carpark use, it may not be appropriate for the proposed community use of the top floor.</p>	<p><i>Note only</i></p>	4 June 2019
1.2	<p><b>4 June 2019 – Double knock smoke detection</b></p> <p>For those areas with smoke detection, please clarify how the proposed double knock detection will be incorporated into the modelling.</p> <p>In addition please clarify how this will work in the event of rooms small enough to have only a single detector.</p>	<p><b>13.06.2019</b></p> <p>Double knock detection is yet to be confirmed.</p> <p>If double knock system is proposed, the configuration of detectors, noting only one may be present in a space, will be presented in a sketch format in detailed zone FEB for mutual understanding before we proceed.</p>	21 June 2019
1.3	<p><b>4 June 2019 – FLED</b></p> <p>The FLED drawings indicate that back of house storage areas are to have a FLED of either 400 or 800MJ/m2. Please justify why the storage&lt;3m FLED of 1200MJ/m2 given in C/V/M2 Table 2.2 is not proposed to be used.</p>	<p><b>13.06.2019</b></p> <p>We will address the storage&lt;3m FLED of 1200 MJ/m<sup>2</sup> in the detailed zone FEB. At this stage we believe this is limited to major anchor tenancies only. A Time equivalence sensitivity of retail areas having 10% 1200MJ/m<sup>2</sup> will also be considered.</p>	21 June 2019
1.4	<p><b>4 June 2019 – Proposed k<sub>b</sub> factor</b></p> <p>As discussed in the meeting, please justify the value of 0.065 for the spaces immediately below the carpark given that this floor slab will be insulated for thermal reasons.</p>	<p><b>13.06.2019</b></p> <p>For the space below the carpark (mall area), we are proposing to do a weighted average FLED and K<sub>b</sub> factor. The void between ground floor mall area and the intermediate floor will be considered as a horizontal vent for the purpose of calculation time equivalence for the ground floor space only.</p> <p>Details will be included in the appropriate detailed Zone FEB.</p>	21 June 2019
1.5	<p><b>4 June 2019 – Use of B-risk</b></p> <p>The proposal to use Q* and shape factor to assess the suitability of B-Risk is noted and concurred with. However be aware that other guidance such as aspect ratio and the 'rules' over the configuration of virtual rooms may also impact on the model set-up and therefore suitability of this tool.</p>	<p><b>13.06.2019</b></p> <p>If and when B-Risk is proposed, this will be detailed in the zone FEB in sketch format taking into consideration of other guidance not mentioned in the master FEB such as aspect ratio and virtual rooms configuration.</p>	21 June 2019

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FEB Comments Register – FENZ ref: FEB 13041

Designers Reference: 136249

Item	Fire and Emergency NZ Comment	Designers Response	Close Out Date
1.6	<p><b>4 June 2019 – FDS grid resolution</b></p> <p>Proposed grid resolution (0.25m near field to 1m far field) noted. Recommended that details to be provided in subsequent zone FEB documents once these developed. Given that D* has not been supported by NIST since November 2015 reference to D* should no longer be relied on to justify an appropriate resolution.</p> <p>A review of the FDS user guide suggests that either a grid resolution study or the use new parameters such as MTR or Wavelet Error Measure (WEM) may be more appropriate.</p>	<p><b>13.06.2019</b></p> <p>Noted. We are proposing to do grid resolution study to one scenario. Detailed of the grid resolution study will be included in each zone FEB.</p>	21 June 2019
1.7	<p><b>4 June 2019 – Factors influencing challenging fire locations</b></p> <p>In other mall projects around the country we have observed a number of parameters that impact on the choice of design fire locations. We recommend consideration of these when determining the challenging fire locations particularly for the zone 2 mall FEB.</p> <ul style="list-style-type: none"> <li>a. Ceiling height within the mall and retail shops</li> <li>b. Width and number of openings into the mall (particularly applicable for corner tenancies).</li> <li>c. Controls or restrictions on the downstand (if any) between the tenancy and the mall concourse.</li> <li>d. The potential of openings between floors within tenancies.</li> <li>e. Proximity to voids connecting to the upper level of retail/dining spaces.</li> </ul> <p>While the details of these is unlikely to be available at this time the intention is to highlight the concern and support the future challenging fire locations.</p> <p>We also recommend that the details of these assumptions be clearly documented so that future retail fit-outs may be compared against these design assumptions. This will help confirm if a proposed fit-out lies within the original building assumptions or if additional modelling is required to support that fit-out.</p>	<p><b>13.06.2019</b></p> <p>Noted. Details of assumptions will be documented in each zone FEB.</p>	21 June 2019
1.8	<p><b>4 June 2019 - Modelling of doors</b></p> <p>The FEB currently proposes to model external doors as 50% open for the duration of the simulation. While this is appropriate during occupant egress, please justify in accordance with C/VM2 2.2.1(d). Are these doors designed to open for makeup air purposes?</p>	<p><b>13.06.2019</b></p> <p>Noted. Details of external doors will be clarified in each zone FEB. In general, if the doors are designed to auto open, it applies only to those doors.</p>	21 June 2019
1.9	<p><b>4 June 2019 – Smoke control initiation</b></p> <p>The FEB currently proposes to model mechanical smoke control with a delay time of 0 seconds and a ramp up time of 30 seconds. We note that the 30 second verification time in C/VM2 is based on the alarm verification and equipment response time requirements of NZS 4512 clauses 204.6 and 204.7. Please discuss the suitability of the times proposed.</p>	<p><b>13.06.2019</b></p> <p>If the double knock system is proposed, a delay time of 0 seconds is considered reasonable. If a double knock system is not proposed within the building, we will be considering a delay time of 15 seconds.</p> <p>In respect to exhaust fan ramp up times, this is to be detailed in the zone FEB for the appropriate buildings (Zone 1 - Anchor and Zone 2-mall).</p>	21 June 2019

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FEB Comments Register – FENZ ref: FEB 13041

Designers Reference: 136249

Item	Fire and Emergency NZ Comment	Designers Response	Close Out Date
<b>Zone 3 (Carpark) FEB</b>			
1.10	<p><b>3 July 2019 - HS scenario</b></p> <p>The zone 3 FEB is ambiguous in that Table 1 indicates that two water supplies for the sprinkler system is being provided whereas section 4.1 indicates that the secondary water supply is no certain.</p> <p>We note that the master FEB was more certain on the two water supplies. Is this a design change? As this impacts on the HS scenario, please clarify.</p>	<p><b>04.07.2019</b></p> <p>At this stage, dual water supplies is still the proposed design. If the design changes, we will update the assessment on HS scenario.</p>	15 July 2019
1.11	<p><b>3 July 2019 - Future retail</b></p> <p>We note no consideration of this space at this time. Is this being considered or is this intended to be considered should this occur in the future? Given the floor area of the carpark we recommend consideration of the occupant loads using the stairs and the potential for the occupant load to exceed 1000 people within this zone.</p>	<p><b>04.07.2019</b></p> <p>Future retail will be considered in the future when this is confirmed.</p> <p>Comments regarding the stairwell noted. We will address this point when the design has confirmed. It is proposed to address the occupant load within the stairwell on a case by case basis as the occupant load within any stairwell is dependant on the location of the fire and the alternative available egress provided to the occupant load. If a challenging fire arise where it forces the occupant load within a certain stairwell to exceed 1000 people, we will assess tenability within the stairwell.</p>	15 July 2019
1.12	<p><b>3 July 2019 - Occupant load from other zones</b></p> <p>While it is not expected to have a large impact on the results please confirm that for CF2 and CF3, the egress of occupants from zone 1 will be considered., particularly as they will essentially all use the same stair.</p>	<p><b>04.07.2019</b></p> <p>Yes, the egress of occupants from zone 1 will be considered as per Section 9 of the FEB where we talk about non-base case RSET which includes occupants from Zone 1 and Zone 2. Please also refer to Appendix A updated sketches on egress distributions (page 24-29).</p>	15 July 2019
<b>Zone 1 (Anchor Tenant) FEB</b>			
1.13	<p><b>3 July 2019 – Level 1 offices</b></p> <p>Does the current layout of the level 1 offices trigger the requirement for a challenging fire scenario in this space? Particularly with regards to the 25m dead end limitation. Please discuss.</p>	<p><b>04.07.2019</b></p> <p>The office layer is still under design. If the final design reaches the 25 m dead end limitation, challenging fire scenarios will be looked into for the office.</p>	15 July 2019
1.14	<p><b>3 July 2019 – Stair fire rating</b></p> <p>We note that the stairs in the anchor tenant are provided with different fire ratings. Please clarify the logic of this.</p>	<p><b>04.07.2019</b></p> <p>The design has changed since the issue of the FEB. We will update the stair fire rating in accordance to the burnout calculation in the fire engineering verification document.</p>	15 July 2019
1.15	<p><b>3 July 2019 – CF3</b></p> <p>While we take the point that the internal partitions within the childcare centre is unrated, Fire and Emergency questions the appropriateness of modelling the 'supplementary compartment' as a single room.</p> <p>We recommend consideration of three rooms, the kitchen (room of fire origin), one representing the central corridor and the other representing the balance of the smoke reservoir. If tenability is measured in the central corridor, this would provide a reasonable representation of this portion of the building.</p>	<p><b>04.07.2019</b></p> <p>Noted. The zone model for the childcare will include the kitchen (room of fire origin), central corridor and potentially one more room with tenability measured in the central corridor. Doors connecting these rooms will be modelled as open. We do not fundamentally agree this is necessary under C/VM2 as they will be unrated barriers and therefore no criteria apply to their performance. We are modelling as requested simply to enable us to progress.</p>	15 July 2019



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FEB Comments Register – FENZ ref: FEB 13041			
Fire and Emergency NZ Comment		Designers Reference: 136249	
Item	Fire and Emergency NZ Comment	Designers Response	Close Out Date
<b>Building Consent Items</b>			
The following items are considered to be detailed design elements that are considered to be required as part of the consent stage documentation. They have been identified at this stage to avoid delays during consenting.			
2.1	<b>4 June 2019 – Cause and Effect Matrix</b>  Given the expected building complexity, we recommend that a cause and effect matrix be included in the consent documentation to ensure that the system operates as intended (e.g. smoke extract fans – particularly if zoned and make-up air supplied).	<b>13.06.2019</b>  A cause and effect matrix will be included in the consent documentation for the appropriate zone.	21 June 2019
2.2			
<b>Compliance with Other Relevant Legislation</b>			
The following items have been identified to address issues with legislation other than the Building Code.			
3.1			
<b>Other Issues</b>			
The following recommendations have been made solely as advice for good risk management and are intended for discussion only. They are not required to be addressed to demonstrate compliance with the Building Code or other applicable legislation.			
4.1			

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# **Zone 1 – D.S. ANCHOR & Childcare Centre HWCP Invercargill CBD Development**

HWCP Management Ltd

**Fire Engineering Strategy**

### Issue Authorisation

Project: Zone 1 – D.S. ANCHOR & Childcare Centre, HWCP Invercargill CBD Development

Project No. 136249

Version	Date	Status	Prepared	Reviewed
A	03 May 2019	Preliminary Issue	ACC	DXM
B	23 September 2019	For Approval	ACC/DXM	DXM

Version	Extent of Revision

This report caters specifically for the requirements for this project and this client. No warranty is intended or implied for use by any third party and no responsibility is undertaken to any third party for any material contained herein. This report is produced and signed solely on behalf of Holmes Fire and no liability whatsoever accrues to the authors.

The building owner must be aware that the Fire Engineering Strategy described in this report may be alternative solutions to those given by the MBIE Acceptable Solutions or Verification Methods.

New Zealand Building Regulations do not impose specific requirements on a building owner to protect their own property. Consideration of protection of the building owner's property is not included in this design beyond the extent which arises from compliance with the Building Code, unless this has been specifically requested. Accordingly, in the event of a fire, it is possible that the property loss could be significant.

It is assumed that the details of these documents are read and understood. Holmes Fire should be contacted if there are any queries regarding interpretation or meaning of the content. Holmes Fire takes no responsibility for the misinterpretation by others.

Submission of this Fire Engineering Strategy document for Building Consent Authority approval implies full understanding and acceptance of the above.

Written By:



Amy Chao

Written/Reviewed by:



Darin Millar

17 Dec 2019

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## INTRODUCTION

The purpose of this report is to determine the minimum fire safety precautions required within the proposed D.S. Anchor & Childcare Centre in HWCP Invercargill CBD Development to demonstrate compliance with Section 17 of the New Zealand Building Act 2004 with respect to the fire regulations.

This is a legal requirement whereby it must be shown that after the completion of works, the objectives of clauses of the New Zealand Building Code relating to means of escape from fire, protection of other property, and structural and fire rating behaviour are satisfied.

This Fire Engineering Strategy report includes a performance based Scope of Works advising of fire safety issues affecting architecture, building services and structure in accordance with the requirements of the New Zealand Building Code. This Fire Engineering Strategy must be read in conjunction with the accompanying fire safety sketches which are marked up on drawings prepared by other consultants.

This is not a 'For Construction' document, but a performance document that is intended to be used by the Architect and other consultants in implementing their detailed designs and preparing their working drawings and specifications. The consultants whose documentation is required to incorporate the requirements of this Fire Engineering Strategy are expected to have read this report, understood the implications as it affects their scope of work, and incorporated the relevant fire requirements into their drawings, specifications, and other construction documents.

## SUPPORTING DOCUMENTS

This Fire Engineering Strategy document is one of a suite of documents prepared by the fire engineer:

- Fire Engineering Brief (FEB)
- Fire Engineering Verification (FEV)
- Fire Engineering Strategy (FES) - this document
- Fire Engineering Sketches (ref latest version of FSK sketches).
- Document transmittal

The Fire Engineering Brief outlines what the design intends to achieve, the factors that affect the design solution, and the design methodology and acceptance criteria that are used to verify that the design objectives are met. The FEB does not detail the final design solution.

The Fire Engineering Verification document contains the calculations and engineering background to the fire safety design - the verification showing how the design solution meets the acceptance criteria.

The Fire Engineering Strategy document outlines the fire safety solution for the proposed works and describes the design solution and specific fire safety requirements necessary to achieve the design objectives.

The Fire Engineering sketches (prepared by Holmes Fire) are to be read in conjunction with the Fire Engineering Strategy.

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## EXTENT OF WORK

This Fire Engineering Strategy covered in this C/VM2 design is the construction of the Zone 1 of HWCP Invercargill CBD development, Invercargill.

The overall development comprises of numerous zones to achieve the completed development. In broad terms the zones are:

- Zone 0 = Overall development consideration.
- Zone 1 = D.S Anchor and Childcare Centre
- Zone 2 = Mall
- Zone 3 = Carpark

Zone 1 is a three-storey structure consisting of a large anchor tenancy occupying the majority of the ground and level 1 space. In the centre of the ground floor are two escalators that lead from the ground floor to level one which creates an open void. Level one is therefore considered as an intermediate floor rather than fully fire separated first floor. Small retail tenancies unrelated to the Anchor, are accessed directly from Esk St.

Level two is proposed to be a childcare centre that is accessed via the adjacent Zone 3 Carpark.

This Fire Engineering Strategy is for the base building design to the extent of proposed works as identified by the Architectural plans used as backgrounds to the Fire Strategy drawings. As a result, all the interactions with Zone 2 and 3 are not part of this fire engineering strategy. For greater understanding of the interaction of the Zones and how we demonstrate compliance with NZBC, refer to the Compliance Design Features Report (CDFR). In broad principles, the following is being asked for Building Consent for Zone 1:

- Ground floor and Level one design except for ceilings in the Anchor tenancy area. Without the ceilings, which have been considered in the Fire Engineering analysis, then the specified systems will not be installed to the ceilings but transferred to the separate application for the tenancy fitout.
- Level 2 design except for the outdoor space sun shades, kitchen fitout or associated extract, floor or window coverings. These works are not transferred as their presence and compliance can be addressed independently via a separate building consent application once the works originate.

To augment the ability for Zone 1 to be granted a Building Consent, the CDFR clearly identifies that the intended occupancy at the completion of the Zone 1 Building Consent works is zero occupants, During the analytical fire design (the Verification) for Zone 1 it has been demonstrated that once additional works as identified in current Zones 3 and future Zone 2 are undertaken, that the Zone 1 can be occupied.

## WORK BY OTHERS

### Access Routes

Escape route widths specified in this fire engineering strategy are the minimum widths for fire safety only, and may not specifically address requirements for access for people with disabilities. Other escape routes features that are not related to fire safety - and hence not specified in this Fire Engineering Strategy - may be required for compliance with Clauses D1 of the New Zealand Building Code.

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### Visibility in Escape Routes

The design of systems to achieve compliance with F6 of the NZBC is outside the scope of this report. Any comments in the Fire Engineering documentation for visibility in escape routes are for purposes of assisting the designers responsible for F6 compliance.

The design of systems to provide artificial lighting to escape routes (both internal and external parts) in compliance with G8 of the NZBC is outside the scope of this report. To assist, the fire strategy identifies the intended escape routes.

### Wayfinding/Signage

The design of exit signage for compliance with F8.3.3 a) of the NZBC is outside the scope of this report. Any comments in the Fire Engineering documentation for exit signage positioning are for purposes of assisting the designers responsible for F8.3.3 a) compliance.

### Structure

Defining the period of fire resistance and fire severity in consideration of C6.2 b, c, and d of the NZBC is addressed by this fire strategy. Identification of the structural systems and its need for structural stability to achieve the performance requirements is to be provided by others. The methodology to achieve the performance is to be provided by others.

Any load bearing walls identified by the structural engineers for the purposes of compliance with C6 have not been annotated onto the fire strategy sketches.

### HSNO

This Fire Engineering Strategy does not specifically consider requirements for Hazardous Substances and New Organisms (HSNO). Therefore, clause C5.7 c) of the NZBC is not addressed by this report.

### Other

Details and approval of the Evacuation Scheme, are to be provided by others.

## DESIGN APPROACH

### Parameters

The following key parameters form the basis of this design. These parameters have been verified by the appropriate parties:

1. No unit title or similar other boundary arrangements exist or are proposed [Client].
2. There are no Memorandum of Encumbrances or similar that exist or proposed which relate to fire. [Client]
3. The Building Importance Level is not IL4 or IL5.
4. The fire design is based around a building wide evacuation strategy. The philosophy is further explained in the FES Zone 0 Discussion.
5. There will be immediate evacuation upon detector activation – no double knock or pre-investigation period is considered.
6. No storage in excess of 3m height is to occur. [Anchor tenant]
7. There are no air ducts which include combustibile materials, passing through exitways.
8. The activities (including potential storage and associated Fire Load Energy Density as appropriate) for the various areas of the building are as follows:

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- Ground Floor – 800MJ/m<sup>2</sup>
- Level one – 800 MJ/m<sup>2</sup>
- Level two (Early childhood centre) – 800 MJ/m<sup>2</sup>

9. There is no solid fuel, gas burning, and oil fired appliances and open fires, proposed in the works.
10. There are no specific spaces for which the sprinkler system is not permitted to be installed as defined by other disciplines.
11. No upper/subfloor concealed spaces shall be used as an air-handling plenum.
12. At this stage there is no ventilation system that services multiple firecells and therefore in duct detection is not required.

### Philosophy

To demonstrate compliance with the relevant fire safety clauses of the Building Code, the following Compliance Documents have been adopted as the design basis:

- C/VM2 – Verification Method: Framework for Fire Safety Design, Amendment 5, 24 November 2017.

### FIRE AND EMERGENCY NEW ZEALAND (FENZ)

In accordance with section 46(1) of the Building Act 2004 some kinds of applications for Building Consent must be provided to Fire and Emergency New Zealand for review.

The proposed fire engineering design solution contained herein;

- establishes compliance in accordance with the provisions of an applicable compliance document to the extent required by the Building Act, and

Therefore, under the Gazette we believe this application need not to be forwarded to Fire and Emergency New Zealand for review. HOWEVER – as this project includes a unique CDFR, we encourage this application to be sent to FENZ for consideration. FENZ have been intimately involved in this development and therefore the process should be relatively straight forward.



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## SCOPE OF WORKS

We believe that the proposed work will be in compliance with the objectives of the New Zealand Building Code clauses C1 to C6 Protection from Fire, to the extent required by the Building Act, based on implementation of the following Scope of Works. This is required to be read in conjunction with the Fire Safety sketches.

The Scope of Works below lists the fire safety precautions needed for compliance with the fire safety requirements of the Building Code.

### 1 FIRE DETECTION, WARNING AND SUPPRESSION SYSTEMS

#### 1.1 Alarm / Detection Systems Requirements

- 1.1.1 A new supplementary smoke detection alarm system is required to be installed to the full area (including detectors for Electromagnetic Hold Open Devices) as indicated on the Fire Strategy sketches, in accordance with NZS 4512:2010.

*To be addressed in other applications shall be:*

- The ground floor and level one smoke detectors, when the ceilings are installed.
- The ground floor and level one manual call points once the fitout of the space is designed.
- The positions of the Fire Control Room (FCR), Sprinkler Valve Room (SVR), all associated infrastructure to make the alarm/detection system functional - being the fire alarm and indicator panels (FAP & FIP)

- 1.1.2 In order to provide signal for the release of electromagnetic hold open devices, the relevant detectors shall be within 1.5 m in plan, on both sides of the door.

- 1.1.3 At the request of the Anchor tenant, a communication cable is to be installed linking the FAP to the tenants security panel in their security office. This is not a specific NZBC item but a request by the tenant.

#### 1.2 Electromagnetic Hold Open Devices

- 1.2.1 Automatic Hold Open Devices including associated detection devices shall be provided at locations as identified in the fire strategy sketches. They are to be installed to BS 7273.4:2007, or EN 1155:1997.

#### 1.3 Sprinkler System Requirements

- 1.3.1 A new Type 6 automatic fire sprinkler system is required to be installed throughout the Zone 1 (including external transformer area) in accordance with NZS 4541:2013 with the amendments outlined in Appendix B of C/AS1 to C/AS/6.

*To be addressed in other applications shall be:*

- The ground floor and Level one sprinkler system where ceilings are installed (retail space).
- The positions of the Fire Control Room (FCR), Sprinkler Valve Room (SVR), all associated FENZ inlets (FSI & FHI)

- *The class A water supply infrastructure (tank and pumps)*

Specifics that are ancillary to NZBC requirements, for information only:

- The sprinkler system for the Zone will have a single isolation valve for all three levels.
- The extent of recessed concealed heads, with white caps is part of a tenant requirement.
- The sprinkler system design will need to cater for the intended use/storage of the tenants.
- There may be no coverage to the Esk street canopy as no external combustible content is expected.
- The rear loading dock canopy shall be provided with sprinklers with a hazard classification equating to the higher of either the sprinkler standard or the largest design density inside the tenancy.
- The expectation of final ceilings extent is important, otherwise the sprinkler head type in a ceiling void could be more than that actually required.

1.3.2 The sprinklers are to have the following operational characteristics in the designated locations:

- Unless noted below all sprinklers are to be quick response ( $RTI \leq 50$ ), with an activation temperature ( $T_{act}$ ) of  $68\text{ }^{\circ}\text{C}$ . Any concealed heads must also meet these parameters.
- External sprinklers to cover areas such as the transformer and loading canopies provide sprinklers with standard response and  $T_{act}$  being  $68\text{ }^{\circ}\text{C}$ .
- Higher rated heads as dictated by the standard due to the ambient environment.

*To be addressed in other applications shall be:*

- *The ground floor and Level one sprinkler system where ceilings are installed (retail space) with the characteristics noted above.*

#### 1.4 Alerting Requirements - Alarm Sounder

1.4.1 A new fire alarm sounder system shall be installed throughout Zone 1 in accordance with NZS 4512:2010.

*To be addressed in other applications shall be:*

- *The ground floor and level one sounders, when the ceilings are installed.*
- *All associated infrastructure to make the alarm/detection system functional - being the fire alarm panel (FAP)*

1.4.2 Provide a Remote Display Unit, or similar, to the Level 3 Childcare facility. The objective of the unit is to easily identify the area of fire original so that the Evacuation Managers of the Childcare facility are more informed than they would be from purely an evacuation alarm. The details of the information is to be developed as part of the Evacuation Scheme design for the tenancy, which will be by others. This feature is considered for facilitating an Evacuation Scheme, it is not considered critical for the NZBC compliance.

*To be addressed in other applications shall be:*

- *All associated infrastructure to make the RDU functional - being the fire alarm panels (FAP)*

- 1.4.3 The functional alerting operation associated with the fire alarm system shall be as identified on the fire strategy sketch Z0 FS 100.

*To be addressed in other applications shall be:*

- All associated infrastructure to make the interfaces functional - being the fire alarm panel (FAP)

## 1.5 Fire Alarm System Interface Requirements

- 1.5.1 Functional interface expectations associated with the fire alarm system shall be as identified on the fire strategy sketch Z0 FS 100.

*To be addressed in other applications shall be:*

- All associated infrastructure to make the interfaces functional - being the fire alarm panel (FAP)

## 1.6 Hydrants

- 1.6.1 A new internal charged fire hydrant riser is required to be installed as identified on the Fire Safety Strategy drawings in accordance with NZS 4510:2008.

*To be addressed in other applications shall be:*

- The positions of the Fire Control Room (FCR), Sprinkler Valve Room (SVR), all associated FENZ inlets (FSI & FHI)

## 1.7 Hand Operated Firefighting Equipment

- 1.7.1 Portable hand operated extinguishers to NZS 4503:2005, are to be provided in the Zone 1 Anchor tenancy to the extent agreed with the Anchor tenant, but not in excess of the requirements of the standard. These items are not a functional requirement of the New Zealand Building Code.

*To be addressed in other applications shall be:*

- The positions of the extinguishers and their type/size .

## 2 FIRE AND SMOKE CONTROL SYSTEMS

### 2.1 Mechanical Smoke Exhaust System

- 2.1.1 Mechanical smoke extract is required as indicated in the fire strategy sketches to achieve 40m<sup>3</sup>/s of smoke extract from the space. The system components and controls are to be designed and installed in accordance with AS/NZS 1668.1:2015 and AS 1670.1:2015.

- 2.1.2 Make up air is to be provided as shown on the fire strategy sketches. The system components and controls are to be designed and installed in accordance with AS/NZS 1668.1:2015 and AS 1670.1:2015.

To be addressed in other applications shall be:

- The associated inlet air continuation from the ground floor once the Zone 2 works are imposed. Technically compliance is currently achieved as the neighbouring space is the Zone 3 ground floor area which is open, has no perimeter enclosures.

- 2.1.3 A fire fans control panel is required to be design and installed in accordance with AS 1670.1:2015. The FFCP shall be located in the Fire Control room.

To be addressed in other applications shall be:

- The positions of the Fire Control Room (FCR) and therefore the resulting FFCP.

- 2.1.4 Functional interface expectations associated with the fire alarm system shall be as identified on the fire strategy sketch Z0 FS 100.

To be addressed in other applications shall be:

- All associated infrastructure to make the interfaces functional - being the fire alarm panel (FAP)

### 3 ESCAPE ROUTE REQUIREMENTS

#### 3.1 Dimensions

- 3.1.1 Horizontal escape routes are to have minimum clear widths not less than those outlined in the following table, unless specifically identified otherwise in the fire safety sketches:

Table 1: Horizontal escape route widths

Location	Min. Clear Width <sup>1</sup> [mm]	Min. Clear Door Width Into/Within [mm]
Horizontal egress routes in open path travel with less than 50 people - not an accessible route	700	600
Horizontal egress routes in open path travel with greater than 50 people - not an accessible route	850	760
Horizontal egress routes in open path travel - accessible route	1200	760
Horizontal egress route within an Exitway	1000	875
All entrance doors into an exitway stair	N/A	1600

1. Allowable minor obstructions to the widths noted are as defined by D1/AS1.

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To be addressed in other applications shall be:

- All means of escape continuation through the Zone 2 area.

3.1.2 Vertical escape routes are to have minimum clear widths not less than those outlined in the following table, unless specifically identified otherwise in the fire safety sketches:

Table 2: Vertical escape route width

Location	Min. Clear Width <sup>1</sup> [mm]	Min. Clear Door Width Into/Within [mm]
Vertical egress routes in open path travel with less than 50 people - not an Exitway or an accessible route	850	600
Vertical egress routes in open path travel with greater than 50 people - not an Exitway or an accessible route	1000	760
Vertical egress routes in open path travel - accessible routes.	1100	760
Vertical egress routes within an Exitway	1800	1600

1. Allowable minor obstructions to the widths noted are as defined by D1/AS1.

3.1.3 The clear height of escape routes shall be no less than 2100 mm across the full width (except for isolated ceiling fittings less than 200 mm in diameter, which may project downwards to reduce this clearance by no more than 100 mm).

3.1.4 All doors on escape routes shall have a clear height of no less than 1955 mm for the required width of the opening, open onto a level floor area on both sides of the door, and where side hinged shall open no less than 90° and the door swing shall not reduce the width of any escape route.

3.1.5 Clear widths of doors shall be measured taking into account the door frame and the width of the door. Door hardware is not permitted to intrude into this minimum clear width of a doorway. Measurement method for escape route width and clear door width shall be as indicated in the figure below.

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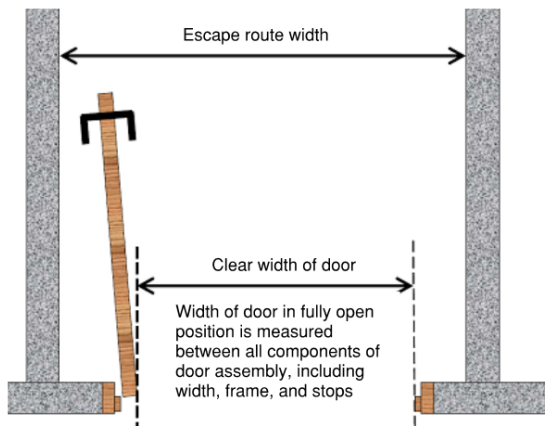


Figure 1 Method of door opening measurements

### 3.2 General

- 3.2.1 Vision panels are to be provided to the doors as noted on the fire strategy sketches.
- 3.2.2 For means of escape provisions, all manually operated doors on escape routes shall have door handles complying with D1/AS1 and door opening forces that do not exceed 67 N to release the latch, 133 N to set the door in motion, and 67 N to open the door to the minimum required width.
- 3.2.3 Automatic sliding doors on escape routes required on malfunction or power failure to automatically slide open and remain open in an emergency. Integration with this related to the smoke control system and the various hours of trade is identified in the fire alarm interface matrix.
- 3.2.4 Painting on floors keep clear adopting yellow hatching in accordance with AS 1319:1994 Table A1 to the areas as indicated on the Fire Strategy sketches.

*To be addressed in other applications shall be:*

- *Paving surfaces so that the application of the painting can be done.*

### 3.3 Locking Devices/Security

- 3.3.1 All locking devices on doors on escape routes until reaching the defined place of safety shall be clearly visible, located where such a device would normally be expected, designed to be easily operated without a key or other implement and allow the door to open in a normal manner.
- 3.3.2 All electronic locking devices on doors on escape routes shall either act under free handle or be fitted with a push button or switch that is fail safe (i.e. independent of any BMS or Security System). The operation must be such that it releases the lock and allows the door to be opened.
- 3.3.3 Crash bars (Panic Bar Door Hardware - PBDH) are required to doors on escape routes as identified in the fire strategy sketches. The following is proposed for some doors which are noted as having PBDH:

- The doors only have push plates – no lever action or PBDH units.
- The doors will be interfaced with the fire alarm system such that if fire alarm is activated during operating hours the doors release any latching.
- In out of hours operations, the doors will not auto release on fire alarm.
- The doors will be fitted with a break glass door release function (addresses any out of hours functionality).
- All doors will be fitted with a manual call point adjacent the break glass alarm – so for what ever reason if occupants are choosing to evacuate and no fire alarm has initiated, then they can release the doors via either manual call point of the door break glass.

3.3.4 If the above is not adopted, then for the PBDH, the associated actuating portion shall consist of a horizontal bar that is not less than half the width of the escape route door leaf and be located between 800 mm and 1200 mm above the floor. The horizontal force is not to exceed 67 N and the door lock is to release allowing the door to swing freely. Doors identified as requiring PBDH but which are auto doors, are deemed to meet this provision.

#### 4 LIGHTING AND SIGNAGE

4.1.1 A new emergency lighting system is required to be installed throughout Zone 1 including associated external escape routes to a safe place, to the extent and in accordance with F6.

*To be addressed in other applications shall be:*

- The ground floor and level one coverage, when the ceilings are installed.
- Coverage in the neighbouring Zone 2 space.

4.1.2 A new emergency exit signage system is required to be installed throughout Zone 1 and associated external escape routes to a safe place, in accordance with F8.

*To be addressed in other applications shall be:*

- The complete ground floor and level one coverage, when the ceilings are installed.
- Coverage in the neighbouring Zone 2 space.

4.1.3 A specific “Clever evac” exit sign system is to be adopted for the Level two Childcare centre such that “no exit” is identified as per the fire alarm interface matrix.

4.1.4 Signage for the fire related safety features is required to be installed throughout the Zone 1 in accordance with F8.

4.1.5 Wherever deemed practical, it is recommended that fire rated or smoke rated wall separations are to be marked within ceiling voids, where no ceilings and aesthetically deemed acceptable in non ceiling areas, with a visible annotation stating “Fire wall {xx}/xx/xx sm, all penetrations to be fire stopped.” Where xx is the period of fire or smoke rated from the fire strategy sketches. This is over and above the NZBC requirements.

## 5 CONTROL OF INTERNAL HAZARDS INCLUDING SURFACE FINISH REQUIREMENTS

5.1.1 Throughout the Zone 1 internal surface finishes shall meet the following early fire hazard indices limitations (when tested to ISO 9705:1993 as per C/VM2 Clause A1.2, or ISO 5660:2002 as per C/VM2 Clause A1.3). Refer to Clause 5.1.2 for exceptions.

Table 3: Group Number Limitations

Building Elements	Location	Maximum Material Group
Ceilings and walls	Exitways (stairwells)	2
Ceilings	Crowd spaces	2
Walls	Crowd spaces	3
Ceilings and walls	All other occupied spaces (offices/store)	3
HVAC ducts	Internal surfaces	2
	External surfaces	3
Acoustic treatment and pipe insulation	Within air handling plenum	3

5.1.2 Note surface finish controls do not apply to:

- Small areas of non-conforming product within a space with a total aggregate surface area not more than 5.0 m<sup>2</sup>.
- Electrical switches, outlets, cover plates and similar small discontinuous areas.
- Pipes and cables used to distribute power or services.
- Handrails and general decorative trim of any material such as architraves, skirtings and window components including reveals, provided these do not exceed 5% of the surface area of the wall or ceiling to which it is attached.
- Damp-proof courses, seals, caulking, flashings, thermal breaks and ground moisture barriers.
- Timber joinery and structural timber building elements constructed from solid wood, glulam or laminated veneer lumber. This includes heavy timber columns, beams, portals and shear walls not more than 3.0 m wide, but does not include exposed timber panels or permanent formwork on the underside of floor/ceiling systems.
- Individual doorsets.
- Continuous areas of permanently installed openable wall partitions not more than 3.0 m high and having a surface area of not more than 25% of the divided room floor area or 5.0 m<sup>2</sup>, whichever is less.

*To be addressed in other applications shall be:*

- *The ground floor and part level one compliance because a stahlton floor system if exposed in the public area would not achieve GN2, but once the ceiling installed compliance achieved.*

5.1.3 The correlation of wall and ceiling surface finishes derived from Australian or European classifications to the Group Number requirements of NZBC Clause 3.4(a) can, without the need for further testing, be taken as described in the following.



Table 4: Australian or European correlations

Group Number to NZBC Clause C3.4(a) using ISO 9705:2003	Australian Group Number to NCC Specification C1.10 Clause 4 using AS ISO 9705:2003	European Classification to EN 13501-1:2007+A1:2009
1S	Group 1, and a smoke growth rate index not more than 100	Class A1, A2 or B and smoke production rating s1 or s2
1	Group 1	Class A1, A2 or B
2S	Group 2, and a smoke growth rate index not more than 100	Class C and smoke production rating s1 or s2
2	Group 2	Class C
3	Group 3	Class D

5.1.4 Any foamed plastic building materials or exposed combustible insulating materials forming part of a wall, ceiling or roof system are required to have a completed system (foamed plastic and/or foamed plastic plus a surface lining) meeting the above maximum material group number as applicable for the location of this building material. In addition, the foamed plastic is to meet the flame propagation criteria as specified in latest versions of AS 1366. It is strongly recommended that foamed plastic materials are not used wherever practical.

5.1.5 Throughout the Zone 1, flooring shall meet the following critical radiant flux limitations (when tested to ISO 9239-1:2010).

Table 5: Critical flux limitations for flooring.

Area of Building	Minimum Critical Radiant Flux [kW/m <sup>2</sup> ]
Exitways (stairwells)	2.2
All other spaces	1.2

5.1.6 Throughout the Zone 1, any suspended flexible fabrics shall have a Flammability Index of no greater than 12 (when tested to AS 1530.2).

5.1.7 Throughout the Zone 1, any flexible fabrics used as underlay to roofing or exterior cladding that is exposed to view, shall have a flammability index of no greater than 5 (when tested to NZS/AS 1530.2:1993).

5.1.8 Throughout the Zone 1, downlights are required to be designed and installed to C/AS1 to C/AS6 Part 7 and the manufacturer's requirements or alternatively, downlights can be considered to have achieved compliance with C2.2 if compliance is demonstrated using the Electrical (Safety) Regulations and subject to a condition of consent.

5.1.9 At the completion of the installation of the lighting, in particular downlights, shall be achieved by a Declaration of Conformity by a Registered Electrician.

## 6 FIRE AND SMOKE SEPARATIONS

### 6.1 Internal Passive Fire and Smoke Separations

6.1.1 Throughout the Zone 1, bounding construction (walls and floors) shall achieve a fire resistance rating as noted on the fire strategy plans.

6.1.2 The nominated internal and external fire ratings need not have the insulation rating applied.

6.1.3 Firecells are as indicated in the fire strategy sketches. The firecells are generally described as:

- Childcare Centre on the second floor;
- Each of the exitway stairs;
- Lift shafts as noted
- Remainder of the Zone 1

The ground and Level 1 including their interaction with Zone2 and Zone 3 is essentially one firecell except as noted above. Openings at floor slabs in Zone 1 for the reticulation is to be kept to a minimum, effectively treated as a smoke barrier around the service.

6.1.1 The vertical risers being the stairs and lift shaft as indicated on the fire strategy drawings, are required to be enclosed with two-way fire rated constructions that achieve a FRR of no less than that identified in the fire strategy sketches as a vertical shaft.

6.1.2 Vertical fire separations are required to be continuous from the ground or floor slab below, to either:

- the underside of the fire rated floor slab above, or
- the fire rated ceiling above, or
- underside of the roofing material.

6.1.3 The horizontal fire separations which separate firecells, are required to extend to the inside face of the external cladding.

6.1.4 The fire separations for the purposes of floors which do not divide firecells shall have a structural stability rating of 30min . Openings between floors for the escalators are expected – other openings are to be addressed as per above even though Ground and Level one is one firecell. As an example, large openings around service penetrations may be filled with intubatt/rockwool material to act as a suitable barrier.

6.1.5 Assemblies of construction to achieve the fire resistance rating performance must be tested in accordance with AS 1530.4:2005, or NZS/BS 476:1987 Parts 21 and 22, or EN 1363 Part 1:1999.

6.1.6 The fire rated glazing required is limited to those associated with the fire doors.

6.1.7 Throughout the Zone 1, smoke separation as indicated in the fire strategy sketches shall achieve the performance with the construction/materials meeting the following:

1. Be a smoke barrier complying with BS EN 12101 Part 1:2005, or
2. Consist of rigid building elements capable of resisting without collapse:
  - a. a horizontal pressure of 0.1 kPa applied from either side, and
  - b. self-weight plus the intended vertically applied live loads; and

3. Form an imperforate barrier to the spread of smoke, and
4. Be constructed of non-combustible materials or achieve a fire resistance rating of (10)/10/- sm, except that non-fire resisting glazing may be used if it is toughened or laminated safety glass.
5. It is acknowledged that duct openings may be present in a smoke barrier – in these circumstances they are to be considered as a fire barrier to achieve a -/10/- rating.
6. As an example, large openings around service penetrations may be filled with intubatt/rockwool material to act as a suitable barrier.

## 6.2 Fire/Smoke Doors, Panels and Hatches

- 6.2.1 All doors within fire separations (excluding lift landing doors) are required to be certified fire rated door-sets complying with NZS 4520:2010 that achieve a FRR of no less than -/xx/-, where xx is the fire resistance rating of the separation the door is to be installed within.

Fire doors are to include self-closers and smoke seals to the top and both side edges of the door leaf or the door frame (and in the latter option, where the door is multi-leave smoke seals are also to be provided at the meeting stile).

- 6.2.2 The fire doors may have vision panels of no greater than 65,000 mm<sup>2</sup> using non-insulated glass.
- 6.2.3 Lift landing doors within fire separations are required to achieve an FRR of no less than -/XX/- or as noted on the fire strategy sketches with the explicit note that they need only achieve integrity rating. The doors shall be certified as a one-way fire rating from the landing side to the shaft.
- 6.2.4 Any access panels or hatches within fire separations are required to be certified to AS 1530.4:2005 to achieve an FRR of no less than -/xx/xx.
- 6.2.5 All doors (except lift doors) within fire separations are required to be fitted with door closers and smoke seals to the top and vertical edges.
- 6.2.6 All doors in smoke separations as indicated in the fire strategy sketches shall meet the required performance with the construction/materials meeting the following:
1. Be constructed of non-combustible materials or achieve a fire resistance rating of (10)/10/- sm, except that non-fire resisting glazing may be used if it is toughened or laminated safety glass.
  2. Provided with smoke seals which are in continuous contact with the mating element, and located to minimise interruption of hardware.
  3. Have frames constructed of non-combustible materials such as aluminium or steel.
  4. Have maximum average clearances (excluding pre-easing) of 3 mm between leaf to frame, 5 mm leaf to leaf, and 10 mm leaf to top of any floor covering.
  5. Be fitted with door closers.
  6. If vision panels present, then the cutout no closer than 150 mm from the leaf edges.

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### 6.3 Closures and Penetrations in Fire and/or Smoke Separations

- 6.3.1 All penetrations through fire separations (created by wires, cables, pipes, flush boxes, etc.) or any gaps, or control joints, are required to be fire stopped with systems (collars, wraps, sleeves, mastics, etc.) that are approved for the proposed use (e.g. rating, orientation, penetration type, construction type) in accordance with AS 1530.4 2005 and AS 4072.1:2005. Where fire stopping systems to AS 4072.1:2005 are not able to be provided, it is acceptable to incorporate systems tested to BS EN 1366.3:2009, or UL 1479. Fire stopping systems are required to be installed strictly in accordance with the manufacturer's instructions.
- 6.3.2 Specifically note that the Level one floor is not a firecell separation and therefore sealing of penetrations is not required. However – to mitigate the paths for smoke migration any opening that is not within a riser, must be “smoke sealed” with a non combustible product.
- 6.3.3 Penetrations shall be supported to resist movement or collapse during fire. Supports shall not prevent normal expansion and contraction of the penetration.
- 6.3.4 Throughout the building, fire dampers are required to be installed where HVAC ductwork penetrates through fire separations (and smoke barriers as noted above). Dampers are to be installed in accordance with AS 1682.2:1990 and the manufacturer's instructions.
- 6.3.5 Each relevant services contractor will be required to submit details of the proposed fire stopping systems for review, prior to installation on site. Care should be taken to select and submit details that have been tested in the relevant wall/floor construction.

The details need to:

- identify the substrate, service and associated fully detailed solution
- solution system manufacturer/supplier
- demonstration of the certification of fire resistance rating for the complete system in accordance with a relevant standard
- test data may be required to verify performance of these systems

### 6.4 Structural Considerations

- 6.4.1 The Structural Engineer is required to identify the *primary elements* that provide support to the fire rated construction. The primary elements shall either:
1. Inherently achieve the structural adequacy, integrity, and insulation component of the fire rating as appropriate, or
  2. Have applied treatment or fire protection to achieve the adequacy component of the fire rating as appropriate.
- 6.4.2 Primary elements are required to achieve a fire resistance rating for structural adequacy of not less than the fire rated construction elements they support. The separation elements are identified in the fire strategy sketches and in the body of the fire strategy.
- 6.4.3 Fire rated construction that are for protection of fire spread to other properties (i.e. external walls, internal building elements separating different titles) shall achieve structural stability during and post fire.

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## 7 FIRE AND EMERGENCY NEW ZEALAND (FENZ)

### 7.1 Access

7.1.1 FENZ vehicle appliance access is required to the FENZ attendance point within the site boundary (as distinct from a location on a street frontage). The associated pavements for vehicle access situated on the property which provide vehicular access by fire appliances shall:

- The positions shall provide access to within 20 m of the firefighter access into the building and any associated inlets.
- Be able to withstand a laden weight of up to 25 tonnes with an axle load of 8 tonnes or, have a load bearing capacity of no less than the public roadway serving the property, whichever is the lower, and
- Be trafficable in all weathers, and
- Have a minimum width of 4.0 m, and
- Provide a clear passageway of no less than 3.5 m in width and 4.0 m in height at site entrances, internal entrances and between buildings.

*To be addressed in future applications shall be:*

- *The positions of the Fire Control Room (FCR), Sprinkler Valve Room (SVR), all associated FENZ inlets (FSI & FHI)*
- *The positions of the Fire Control Room (FCR), Sprinkler Valve Room (SVR), all associated infrastructure to make the alarm/detection system functional - being the fire alarm and indicator panels (FAP & FIP)*



# **Zone 1 – D.S. ANCHOR & Childcare Centre HWCP Invercargill CBD Development**

HWCP Management Ltd

**Design solutions for Passive Fire Rated Systems for services**

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### Issue Authorisation

Project: Zone 1 D.S Anchor and Childcare Centre, HWCP Invercargill CBD Development

Project No. 136249

Version	Date	Status	Prepared	Reviewed
A	21 October 2019	For Approval	DXM/TM	DXM
B	22 October 2019	For Approval	DXM/TM	DXM

Version	Extent of Revision
B	Minor adjustments in solutions

This document caters specifically for the requirements for this project and this client. No warranty is intended or implied for use by any third party and no responsibility is undertaken to any third party for any material contained herein. This specification is produced and signed solely on behalf of Holmes Fire and no liability whatsoever accrues to the authors.

New Zealand Building Regulations do not impose specific requirements on a building owner to protect their own property. Consideration of protection of the building owner's property is not included in this design beyond the extent which arises from compliance with the Building Code, unless this has been specifically requested. Accordingly, in the event of a fire, it is possible that the property loss within unsprinklered buildings could be significant.

It is assumed that the details of these fire safety documents are read and understood. Holmes Fire should be contacted if there are any queries regarding interpretation or meaning of the content. Holmes Fire takes no responsibility for the misinterpretation by others. Submission of this Passive Fire Protection Specification document for Building Consent implies full understanding and acceptance of the above.

This document is intended for the use of a Specialist fire stopping contractor that has been engaged by either the client or the Main contractor. If this is not the case and the passive fire protection is being attempted by the individual sub trades or the Main contractor, then thought must be given to the extra costs associated with the higher level of Engineer engagement through construction monitoring and design advice that this type of approach inevitably requires.

Regardless of whether a specialist is engaged or not (highly recommended), it is IMPORTANT that this document is read during a round table discussion with the Engineer, Main contractor and all the Sub trades prior to first fix of building services.

It is expected that the dissemination of this document to the relevant sub trades is done by the Main contractor (or client) in a timely manner, as improper sequencing can significantly affect the delivery of compliant fire stop systems.

This document is meant to be read in conjunction with the Holmes Fire report

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## GENERAL REQUIREMENTS & CLARIFICATIONS

### GENERAL

- A1.1 The solutions presented herein are derived from manufacturer's literature, consisting of Technical Datasheets, and/or Test Reports, and/or Appraisals by Certified Bodies. They are to form the basis of Tender and Construction as applicable.
- A1.2 The solutions presented are by no means exhaustive and are not to be construed as meaning only the presented solutions should be considered compliant. However, the solutions specified in this document have been carefully chosen by looking at several criteria, and more than just price or adherence to a standard.
- A1.3 Substitution of a specified solution is allowable only if site conditions make that specified system unachievable. The Sub-contractor is to state why the substitution is necessary, what solution is being proposed instead and if required provide that solutions manufacturer's literature. This includes Technical Datasheets, Fire Test Certificates and where possible Fire Test Reports. Alternatively, the Fire Protection Associations product register can be used as a source of compliant solutions. The Engineer will review the potential alternative and notify acceptance upon agreement, with the substitution triggering a revision update to this document.
- A1.4 Penetrations shall be supported to resist movement or collapse during fire. Supports shall not prevent normal expansion and contraction of the penetration.
- A1.5 Notwithstanding the above, care should be taken to select and submit details that have been tested in the relevant wall/floor construction.

The details need to:

- identify the substrate, service and associated fully detailed solution
  - solution system manufacturer/supplier
  - demonstration of the certification of fire resistance rating for the complete system in accordance with a relevant standard
  - test data may be required to verify performance of these systems
- A1.6 If no off the shelf tested solution is available for a passive fire stop issue and an Engineering Judgement (EJ) is required then the Sub-contractor is to organise, in conjunction with a reputable manufacturer, an alternative solution. This alternative solution should come with the documents outlined in A1.3 that show that in a similar or close to situation compliance was reached. The Engineer will review the potential alternative and notify acceptance upon agreement, with the EJ triggering a revision update to this document.

### CARE TO BE TAKEN

- A2.1 The Sub-contractors shall take all due care to ensure that no consequential damage occurs as a result of the works being carried out in the premises. Where necessary, protective covers shall be used to protect finishes, fittings and plant equipment.
- A2.2 All work areas are to be thoroughly cleaned before the application of firestop solutions. This is particularly important for sealants, as they MUST bind to the substrate that are applied to.



## INSPECTIONS, ACCEPTANCE AND FINAL COMPLETION

- A3.1 The works shall be made available for inspection by the Engineer or their representative at appropriate times during the construction, to enable the Engineer or their representative to undertake a level of construction monitoring of the fire stopping systems, conducive to ascertaining whether completion of the works has been achieved and whether a PS4 Producer Statement for Construction can be issued. The construction review will entail visual inspection of fire stopping and associated quality control systems and documentation, and destructive testing of random samples of typical firestop installations. Making good following destructive testing will be done at the cost of the installer.
- A3.2 Any works that have not been made available for inspection by the Engineer or do not meet the requirements of the Specification, appropriate Standards and/or legislation shall be made accessible and/or made good at no cost to the Principal.
- A3.3 Upon completion the Sub-contractor shall provide a Producer Statement (Construction) stating they have installed all fire stopping in accordance with this Specification and manufacturers' instruction.
- A3.4 The Producer Statement shall be issued by persons competent to attest that the fire stopping systems meet Standards and Statutory requirements and that understand the liabilities of non-conformance. They should be able to be on the local council's Producer Statement Authors list.
- A3.5 In order to obtain Practical Completion the Sub-contractor shall obtain a PS4- Producer Statement (Construction) from The Engineer, who is to observe the fire stopping installations in accordance with the Standards and Statutory requirements.
- A3.6 The Sub-Contractor is required to keep a record of the installation of fire stop systems. This information needs to be presented as a "Schedule of Works" as per the relevant standards guidance (AS4072.1). **Additionally, this schedule of works is to accompany a marked-up plan indicating where the firestop installations are located.** At completion of fire stopping the service the Sub-contractor is to make allowance to place an identification label adjacent to the penetration. The locating of these signs and their style is to be agreed by The Engineer prior to undertaking the works.
- A3.7 Every penetration is to be photographed, and if it is a through penetration both sides of the penetration are to be photographed. These photos are to form part of the Schedule of Works. These photos are to be taken AFTER an installation label has been attached as per the requirement outlined in A3.6.
- A3.8 Supply of the above certificates shall be part of the Contract requirements and final payments shall/may not be considered until ALL necessary certificates have been supplied.

## SUB-CONTRACTOR RESPONSIBILITIES

- A4.1 The Sub-Contractor shall coordinate with the Main contractor and other trades to ensure that their systems do not interfere with each other's fire stop solutions, particularly in areas where differing trade services are in close proximity to each other such as riser shafts or firewalls. Care needs to be taken in riser shafts and wall penetrations shared by different trade services. Minimum space constraints between services must be considered at this time.
- A4.2 The Sub-contractor shall take particular care to avoid placing their services too close together or too close to another trades, so that a tested fire rated fire stopping solution may be applied.

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- A4.3 The Main contractor needs to be informed of all the penetration types and is required to allocate the areas where each trade may make their penetration(s). Any services placed without the approval of the Main contractor is to be removed and relocated at no expense to the Principal. Any remedial costs will also be borne by the trade making the penetration without prior approval. Alternatively, it may be determined the fire separation can be modified to account for the service being placed in an untimely manner, however associated costs of the Engineers time, and the additional costs of the fire stopping method will be passed to the contractor at fault to pay.
- A4.4 The Sub-contractor is responsible for placing their services in a manner that it can be fire stopped. For example, cable bundles, pipes and conduits must be brought through the fire separation perpendicular to the fire separation. Cable bunches must be kept less than 100 mm in diameter and at least 150mm apart. Any services run at an angle through a fire separation are to be removed and reinstated in a compliant manner and the fire separation made good at the contractor's expense.
- A4.5 The Sub-contractor is not to run their service before being instructed to by the Main contractor. Any service run prior to suitable wall framing and/or linings being provided may need to be removed and reinstated once the linings and/or openings are in place at no cost to the Principal. The Engineer may determine an alternative method of fire stopping can be applied, in which case the Engineers time and any additional or associated costs of the alternative fire stopping method are required to be met by the Sub-contractor and may be retained from the contract amount for this purpose.
- A4.6 Separate trades are to avoid sharing penetrations, unless prior approval is given by the Main contractor. In no instance shall any other service be run in the same opening allowed for fire dampers and sprinkler pipes. It is with note, that fire stopping solutions for penetrations containing multiple penetrations may incur greater costs (and greater penetration opening sizes) and these additional costs will be passed to the contractors concerned.
- A4.7 The Sub-contractor is responsible for supporting their services on both sides of a fire separation (whether it be a floor or a wall) from the building structure. Supports shall be consistent with the relevant design standard for the services being installed (e.g. AS/NZS 3500.2 for plumbing pipes, AS/NZS 3000 for wiring, NZS 4541 for sprinkler pipes) but, with the first support either side of the penetration being within the limits stated on the fire stopping solution drawings. Wiring is required to be supported by a catenary system or cable tray system. Catenary systems (wires) are not to penetrate through a fire separation. They must terminate at the face of the separations.

## DISCLAIMERS

### A5.1 Acoustic Requirements

- A5.1 The solutions contained herein make no reference to acoustic performance. Should walls and/or floors require a certain acoustic performance as specified on Architectural Plans and/or Specifications or by the Principal, the contractor is to notify the Engineer where this occurs along with the proposed fire stopping solution(s) to be adopted, so that acoustic performance can be investigated, and a suitable instruction issued.

### A5.2 Environment

- A5.2.1 The solutions contained herein are for internal environments only that are typically maintained at temperatures between -5 °C and + 70°C and with no exposure to rain and no exposure to UV.

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A5.2.2 Furthermore, Hilti CFS-C P fire collars and CFS-SL speed sleeve solutions are restricted to internal environments that do not include high humidity (e.g. not humidity class 5 in accordance with EN ISO 13788) and are not to be used where temperatures may be expected to fall below 0°C.

A5.2.3 Where systems include fire mastic, the manufacturer's instructions are to be followed with regard to temperatures to be maintained during the curing period. Typically, temperatures are to be maintained at above 8°C and full curing typically takes 1 day for every mm depth of mastic.

A5.2.4 Should fire stopping of services be in areas outside the above restrictions, the contractor is to notify the Engineer so that a suitable detail may be sourced, and a suitable instruction issued.

### **A5.3 Seismic**

A5.3.1 The fire stopping solutions detailed herein are for low movement scenarios and do not include consideration to required clearances around services with regards to requirements of structural/services standards such as NZS 4219. It is assumed required clearances around services will be detailed within the Services Specification and/or plans. Where a solution contained herein is not able to be used for the required clearances between the services and the floor or wall, the contractor is to contact the Engineer so that a suitable detail may be issued.

### **A5.4 Floor Slab junctions to external walls**

A5.4.1 Fire stopping solutions at the interface of floor slabs and exterior cladding and/or curtain walls are outside the scope of this Specification. Such systems are expected to have been co-ordinated between Consultants and detailed within the Architectural Specifications and/or drawings. If required, we can be engaged to undertake a review of these gaps and advise accordingly.

### **A5.5 Fire Dampers**

A5.5.1 The nomination of a manufacturer and the installation of fire dampers is outside the scope of this Specification. However, fire separations must be viewed by Holmes as have being correctly prepared for the damper installation. New fire dampers are to be installed by the Mechanical Services contractor in accordance with AS 1682 and the manufacturer's instructions.

### **A5.6 Electrical flushboxes**

A5.6.1 Appropriate treatment via intumescent pads or similar to the manufacturers detail shall be dealt with by the appropriate installation trade.

### **A5.7 Fire separation junctions**

A5.6.1 Fire stopping solutions at the interface of fire separations with other elements of construction are outside the scope of this Specification. Such systems are expected to have been co-ordinated between Consultants and detailed within the Architectural Specifications and/or drawings. If required, we can be engaged to undertake a review of these gaps and advise accordingly.

## FIRE STOPPING SOLUTIONS

### B1.1 Light Weight Fire Separation Walls

- B1.1.1 The majority of fire stopping solutions developed and tested for use in plasterboard lined walls (timber or steel framed) are for countries that include higher fire rating requirements than New Zealand and as such incorporate wall types that achieve a 120 minute FRR and thus have 2 x 13 mm (or 2 x 12.5 mm) or 1 x 19 mm plasterboard linings on both sides of the wall.
- B1.1.2 The sub-contractor is required to provide marked-up plan to the Main contractor, identifying the location they wish to penetrate the fire separation wall, and what the service is and the proposed method of fire stopping if they are responsible for it.
- B1.1.3 The Main contractor, upon review of the sub-contractors marked up plans is to provide the necessary framing and linings in the areas to be penetrated.
- B1.1.4 In most above ceiling instances, the Main contractor is required to provide designated areas where services are to be run. These designated areas are required to include additional framing to cut down the wall cavity area around the services. Single lined walls may require an additional layer of wall lining on the single line side (referred to as the "localised patch") to bring the wall lining thickness up to no less than 26 mm both sides of the wall. These localised patches can either be external or internal.
- B1.1.5 All sheet edges of the specified wall linings must fall on framing. The localised patch must span from stud to stud and be fixed into the framing. This means any slots or cuts made in plasterboard to accommodate service penetrations must have wall framing behind them for the plasterboard to be adequately fixed, and so that the wall maintains its fire performance. Any back blocking needs to be mechanically fixed to the framing. Under no circumstances is the weight of any back blocking or framing to be carried by the plasterboard.
- B1.1.6 It is preferred that any fire wall linings and localised patches are installed in the vicinity of the service penetration prior to the service being run. This requires thought around sequencing, and if it is not possible then services installed prior to the wall framing or lining must be framed around as per B1.1.5.
- B1.1.7 Openings made in plasterboard walls for hydraulic and electrical/data services must be made with the appropriately sized hole saw that allows for any annular gap requirements that a fire stop system may have.
- B1.1.8 For fire stopping solutions that require an opening through the wall that is framed and lined through the wall cavity, the Main contractor is required to provide the framing and the linings through the wall cavity, as well as providing the localised linings of the fire separation wall (as described above). The openings are to be fully framed and lined with the same plasterboard (as described above). The openings are to be fully framed and lined with the same plasterboard as the wall (e.g. wall is 13mm the opening must be 13mm, if the wall is 2 x 13mm then the opening must be trimmed with 2 x 13mm).
- Ideally, services are not permitted to be run prior to the wall linings and/or trimmed opening being installed.
- B1.1.9 No services are to penetrate seismic joints or deflection head joints. Service penetrations on walls with deflection heads are to be far enough away from the head to ensure that the firestop system used is in no way impacted by the action of the deflection head.

B1.1.10 Localised patches are to be applied as follows:

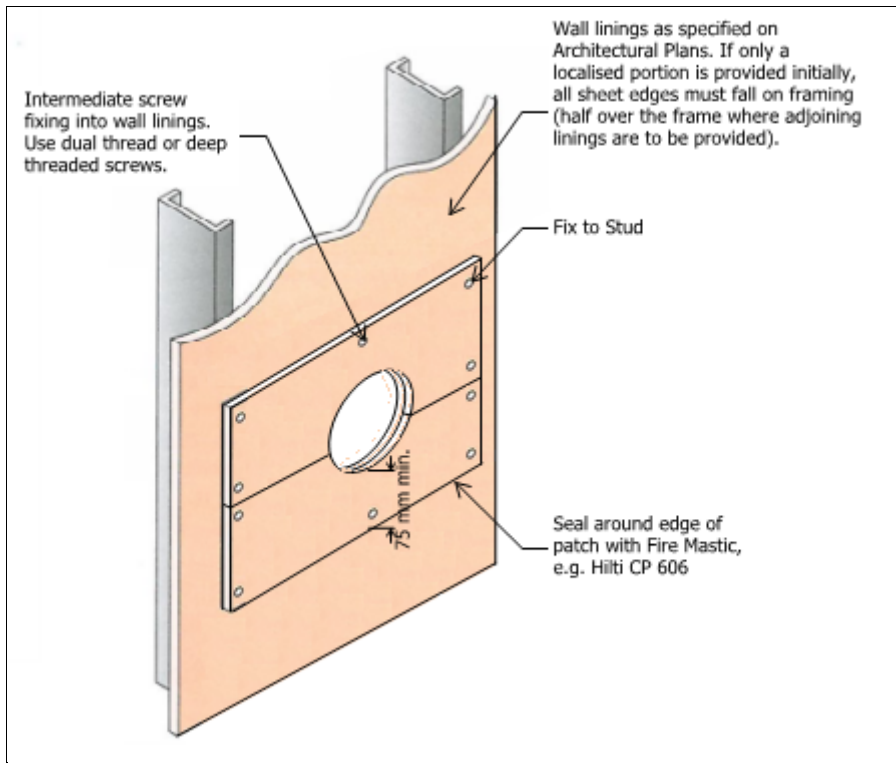


Figure 1: Patching the Services Opening.

B1.1.11 Where localised patching is to occur in areas below ceiling and open to view, the patch is required to be provided behind the finished wall layer. Additional framing is required to be fixed to the wall framing for the patch to be fixed to, as indicated in the figure below.

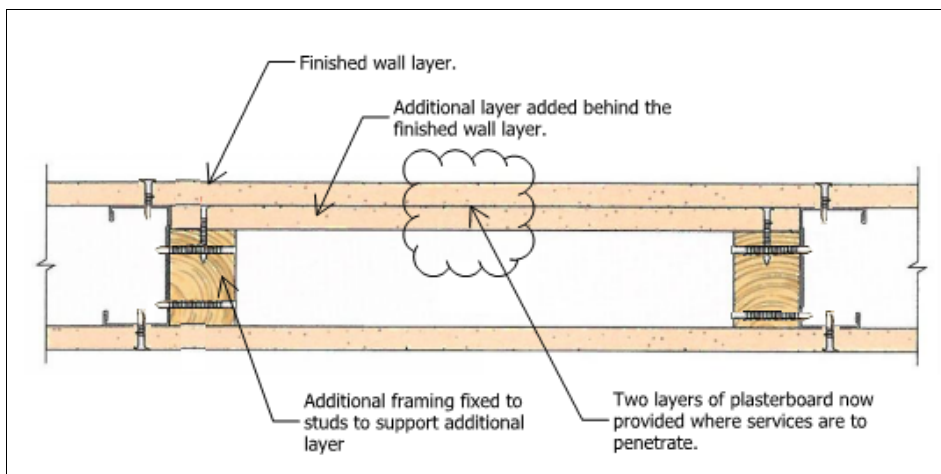


Figure 2: Provision of Additional Lining Thickness behind Finished Wall Layer.

B1.1.12 Where Fibre cement (RAB, PACBLD etc) is to be used, any penetrations must be run through solid timber framing, or they must be framed out in order to except a plasterboard patch. Where possible the fibre cement board is to be replaced with a suitable plasterboard system.

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B1.1.13 All penetration through walls must have protection fitted to both sides unless specifically stipulated. Any item that cannot be treated with a system specified below, requires approval from the fire engineer prior to install.

## **B1.2 Light Weight Fire Separation Floor Assemblies**

B1.2.1 No lightweight floors have been specified for this project.

## **B1.3 Concrete Floors**

B1.3.1 For hydraulic penetrations trade it is expected for the Main contractor will inform of the approach that will be adopted for the site, being either the provision of Cast-In Collars or the provision of Retro-Fit collars and/or pipe wraps.

B1.3.2 Where Retro-Fit solutions are specified the Sub-contractor is to tender the supply and install of the appropriately sized retro-fit collar and/or pipe wrap. Wraps are not permitted to be provided to the shower or floor waste gullies. These are to fire stopped with fire collars only. Wraps may be used on basin and toilet wastes.

B1.3.3 With retro-fit solutions, it is the responsibility of the Sub-contractor to provide the correct sized core hole in the slab for the collar or wrap (wrap for toilet and basin wastes only). The sub-contractor is also to select the appropriate method accounting for the proximity of any structural element such as ribs or columns.

B1.3.4 Where collars are proposed to be used by the Sub-contractor for a penetration type that could have been protected with a pipe wrap and there is a clash with the ribs, preventing the application of a collar, the additional cost of the required bulkhead and any additional collars is to be borne by the sub-contractor.

B1.3.5 It is the responsibility of the applicable Sub-contractors to provide the correct sized core hole, or where applicable the correct sized conduit through the wall, taking note of the size of the services and the requirements of the fire stopping solution that is to be adopted. Typically, services are to occupy no greater than 60% of the opening. If conduit is cast into the wall this conduit counts to the percentage loading of the services.

## **B1.4 Concrete Walls**

B1.4.1 It is the responsibility of the Sub-contractors to provide the correct sized core hole, or where applicable the correct sized conduit through the wall, taking note of the size of the services and the requirements of the fire stopping solution that is to be adopted. Typically, services are to occupy no greater than 60% of the opening. If conduit is cast into the wall this conduit counts to the percentage loading of the services.

B1.4.2 Where the wrong sized core hole or conduit is placed, the cost of additional required core holes and any rework of services is to be borne by the contractor at fault.

B1.4.3 All sub-contractors are to price for penetrating concrete walls and the required fire stopping. Should during works different sub-contractors negotiate between themselves to share a core hole, provided it can readily still be fire stopped to the methods contained herein, the savings are to be passed onto the Principal.

B1.4.4 No cables or plastic pipes are to be run through openings formed for sprinkler pipes or fire dampers.

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B1.4.5 Any penetration through walls must have protection fitted to both sides unless specifically stipulated. Any item that cannot be treated with a system specified below, requires approval from the fire engineer prior to install.

### **B1.5 Stahlton Floor**

B1.6.1 Where plastic pipes penetrate through floors, All Proof drop in fire collars are preferred. Where retro-fit options are specified the sub-contractor is to tender the supply and install of the appropriately sized retro-fit collar and under packing if required (i.e Intubatt, steel plate and rockwool etc). For shower or floor waste gullies only the All Proof system can be used.

B1.6.2 It is the responsibility of the sub-contractor to provide the correct sized core drilled hole in the slab for the service. The Sub-contractor is also to select a method appropriate for accounting for the proximity of any structural element such as ribs or columns.

B1.6.3 It is the responsibility of the applicable sub-contractor to provide the correct sized core drilled hole, or where applicable the correct sized conduit through the floor, taking note of the size of the services and the requirements of the fire stopping solution that is to be adopted. Typically services are to occupy no greater than 60% of the opening. If conduit is cast into the floor this conduit counts to the percentage loading of the services. If in doubt about loading percentages being met, then core another hole.

B1.6.4 If any cable tray/large cable group is to penetrate the slab, specific form work may be required in the floor system to create a specific opening which can be appropriately fire stopped (the slab may be required to be a full section 150mm thick).

B1.6.5 Suitable spacing between penetrations must be provided to allow fire stop devices/systems to be installed as per manufacturers specifications. If services are installed without the correct spacing then this would be treated as an alternative solution, and any costs associated with providing more information or an engineering judgement would be undertaken at the expense of the sub-contractor.

## SPECIFIC FIRE RATING SOLUTIONS

### Overview

The following scope of services penetrating through fire separations that divide firecells are provided as identification that a solution is available to address the service and maintain compliance with the performance requirement of the fire separation.

Based on the services supplied information, the following represents product solutions for the individual service penetrations that have been identified

Service	Substrate	Material	Indicative sizes	Solution	Doc
Cables for fire alarm	Concrete wall	Cable	4<math>\phi</math><math><15\text{mm}</math>	Hilti CFS-IS (CP611A)	CWE01
Metal pipe sprinkler and hydrant	Concrete wall	Steel	40<math>\phi</math><math><165\text{mm}</math>	Hilti CFS-S ACR (CP606)  Or  Firetherm Intumastic	CWP01
Electrical cable trays (120min wall)	Plasterboard wall	Galvanised Steel with XLPE/PVC cabling attached	600mm width horizontally	Hilti CFS-F FX (CP660 – 150mm min. thickness)	Hilti approval document or Ryanfire V32



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Service	Substrate	Material	Indicative sizes	Solution	Doc
Electrical cable duct (vertical duct riser from transformer to Childcare DB – Grid 1.C-1.D/1.6-1.7)	Concrete Inter floor structure	High impact uPVC conduit c/w XLPE/PVC cabling	Ø 100mm	HiltiCP660 Or Hilti CFS-B and CFS-P BA Or RyanFire Intusleeve , intumastic and Mineral Fibre Backing 64kg 100mm thick	Hilti approval document Or RyanFire V40
Electrical Cable trays (horizontal)	Level 1 reserve / stair lobby smoke separated area	Galvanised Steel with XLPE/PVC cabling attached	200 – 600mm	Not through fire/smoke separation no fire stopping req.	
Mechanical & Electrical services cables (cables serving electrical services within stairs)	Concrete wall	TPS cable	1.5mm <sup>2</sup> <Ø<25mm <sup>2</sup>	Hilti CFS-IS (CP611A)	CWE01
Security and Telecommunications cables (cables serving electrical services within stairs)	Concrete wall	PVC multicore and/or LSZH optical fibre	Ø<1.5mm <sup>2</sup>	Hilti CFS-IS (CP611A)	CWE01

Service	Substrate	Material	Indicative sizes	Solution	Doc
Mechanical & Electrical services cables - Cable conduit	Concrete inter floor structure?	High impact uPVC conduit c/w TPS cable?	16mm <sup>2</sup> <math>\phi</math><math><150\text{mm}</math> 2	Hilti CFS-IS (CP611A) (upto 32mm)  Hilti Collar  For >32mm  All Proof Drop In Collar Or Firetherm Intubatt with Ryan Fire SL Collar sealed with Intumastic or Intusleeve	CFP04  CFP05/06  Or  Allproof  or V22.3 or V22.5  Or  V63.1
Electrical flush boxes  (not part of this scope)	Fixed to fire/smoke separation walls	Metal flush boxes		Firetherm Putty Pads  Or  RyanFire V37.2 (acoustic tested)  (not part of this scope)	V37  V37.2  (not part of this scope)

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Service	Substrate	Material	Indicative sizes	Solution	Doc
Surface mounted electrical outlets	Conduit through floor as per above.	High impact uPVC conduit c/w TPS cable Proprietary PVC mounting hardware		Hilti CFS-IS (CP611A) upto 32mm  All Proof Drop In Collar Or Firetherm Intubatt with double Intustrap sealed with Intumastic or Intusleeve	CFP04
Vent pipes Foul drainage & stormwater	Concrete Floor Concrete Floor	uPVC Raupiano acoustic pipe	Ø65 - 80mm Ø 65 - 100mm	All Proof Drop In Collar Or Firetherm Intubatt with double Intustrap sealed with Intumastic or Intusleeve	Allproof manual
Water Services Pipes	Concrete floor & walls	Polyethylene	Ø32 - 40mm	All Proof Drop In Collar Or Firetherm Intubatt with Ryan Fire SL collar with Intumastic or Intusleeve	Allproof Or V22.3 or V22.5 Or V63.1

17 Dec 2019

Building Division

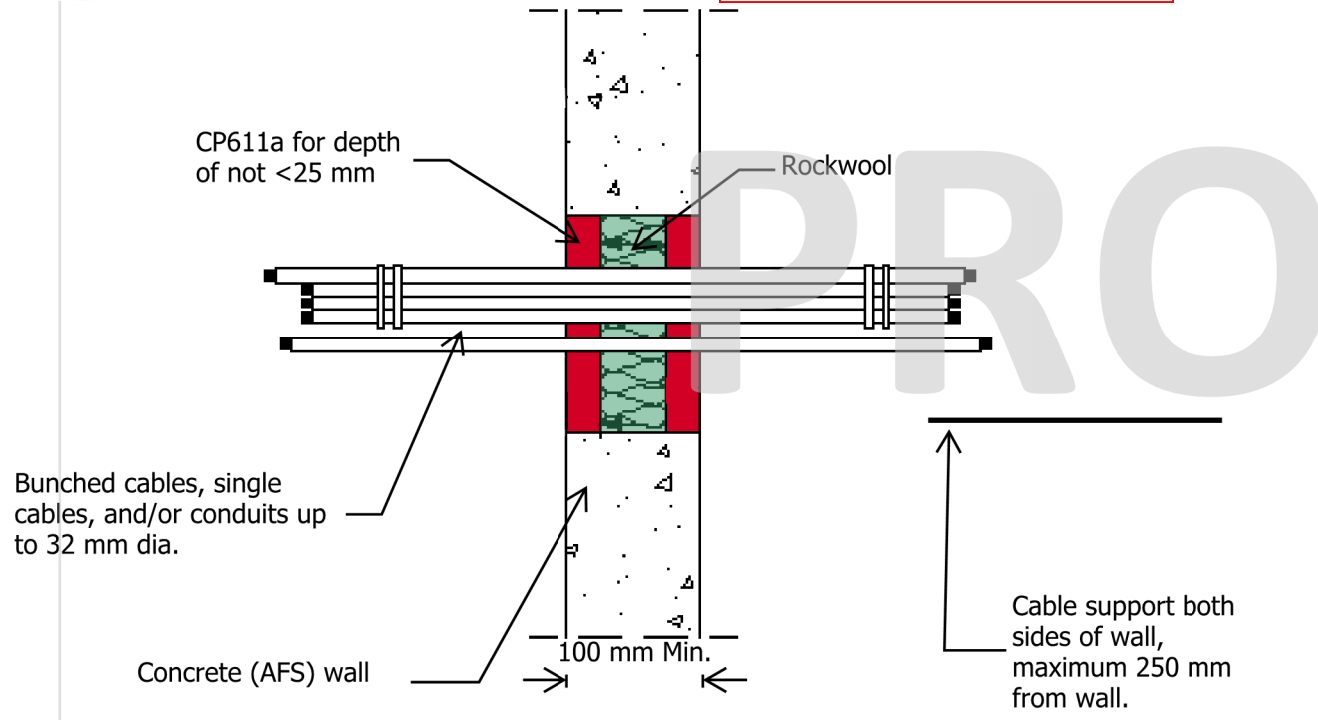
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**2019/1381**

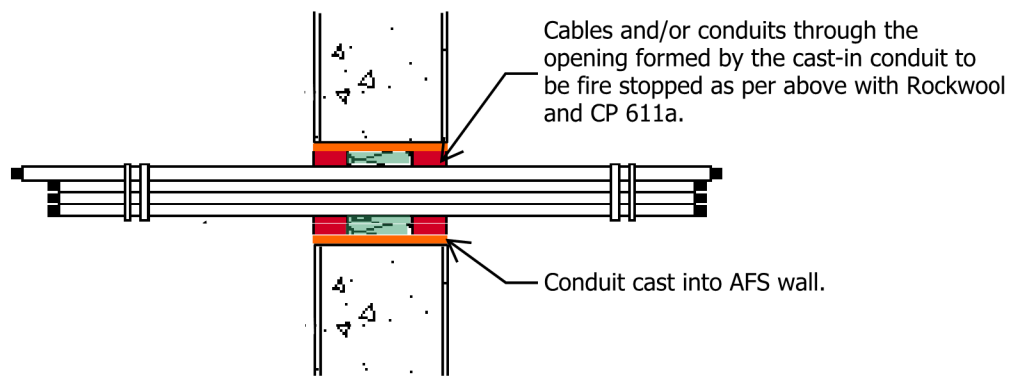
Service	Substrate	Material	Indicative sizes	Solution	Doc
Mech condensate pipes	-	-	-	Assume none	
Mechanical refrigeration pipes	-	-	-	Assume none	
Mechanical ductwork (not part of this scope)	Gib lined stud walls	Galvanised steel	600 x 600 & 800 x 600	Holyoake fire/ smoke damper  Kilargo Fire/ Smoke dampers  Model dependant on size and cross sectional area...	Refer to manufacturer specifications dependant on damper type  (not part of this scope)



Section

Note:

It is acceptable for a piece of oversized Conduit to be cast into the wall. The conduit is to be trimmed flush with the AFS surface and cables run through the opening. The inside of the conduit is then to be treated as above. Noting however the 60% services limitation is to account for the plastic of the cast in conduit.



Restrictions/Notes

Solution is from EWFA Report No. RIR 27912900.1

Maximum opening size  $w = 150$  mm and  $h = 150$  mm, or 170 mm diameter.

Separation of services, as per the figure below.

**Services are not to fill more than 60% of the opening size.**

Max cable bundle size is 100 mm dia.

Max conduit size is 32 mm dia.

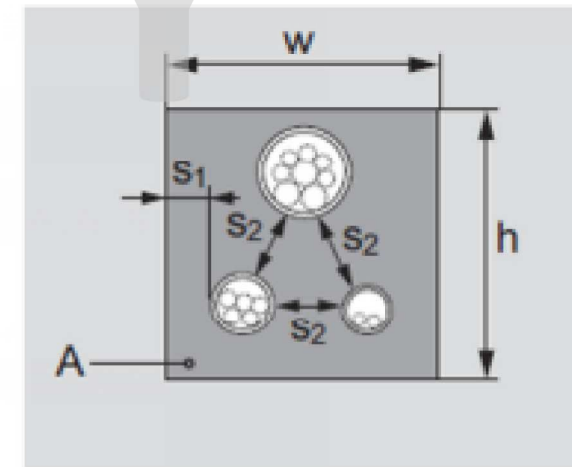
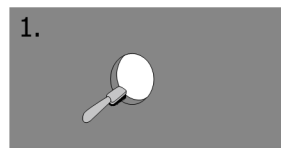


Figure 1 – Distance Requirements of Penetrations

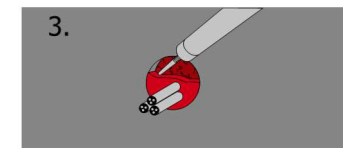
Distance valid for installations of services in wall and floor	Minimum distance in mm
Cables to edge of seal	$s1 = 0$
Cable to other cables/services	$s2 = 40$
Tied Cable bundle to seal edge	$s1 = 10$
Tied cable bundle to other services	$s2 = 40$
Small conduits/tubes to edge of seal	$s1 = 10$
Small conduits/tubes to other services	$s2 = 40$
Conduits $\varnothing > 16$ mm, distance between conduits to edge of seal	$s1 = 10$
Conduits $\varnothing > 16$ mm, distance between conduits and other services	$s2 = 40$



1. Clean opening. Surfaces to be dry and free of loose debris, dirt, oil, wax or grease.



2. Insert mineral wool backfilling, leave sufficient depth for application of sealant.



3. Fill around services with CP611a for required depth.



4. Where exposed to view, smooth before skin forms using water (permissible to use diluted liquid soap) and spatula. Leave completed seal undisturbed for 48 hrs.

Installation Instructions

This sketch does not constitute a complete fire engineering design or detail. Detailed construction drawings are provided by others. Best viewed in colour. Not all fire separations around ducts and shafts are shown.

Legend



Holmes Fire LP  
holmesfire.com

Project Title

HWCP

Sketch Title

Cable and Conduit Penetrations through Concrete Walls  
Hilti CP611a Solution

Drawn: DXM

Date: 22 / 10 / 2019

Project No.

136249

Sheet No.

CW-E-01

Rev

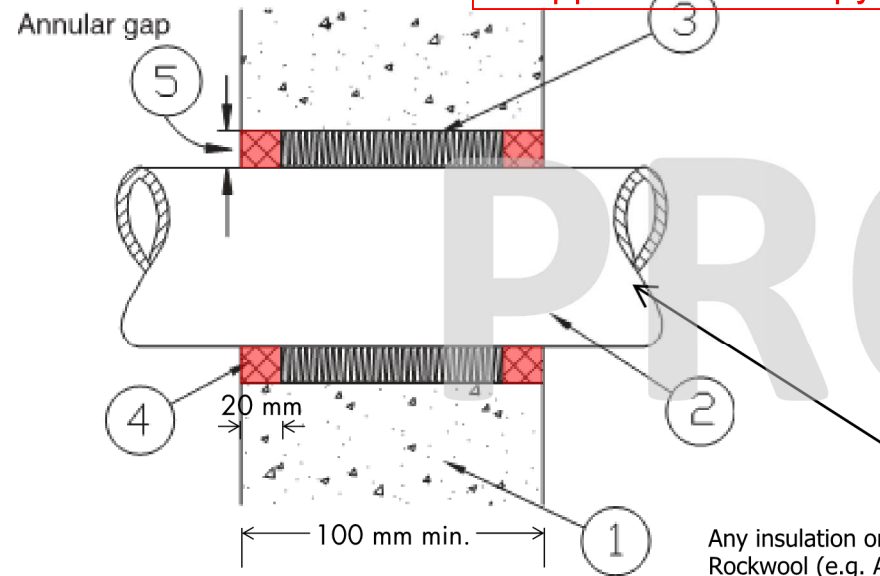
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Any insulation on pipe that is not Rockwool (e.g. Armaflex) is required to be cutout so only the pipe penetrates the wall. If insulation cannot be cut out, refer to different fire stopping solution.

- 1 = Concrete Wall (AFS Wall)
- 2 = Metal Pipe up to 200 mm dia.
- 3 = Rockwool backfilling
- 4 = Hilti CP606 Sealant. Minimum Depth 20 mm.
- 5 = Annular Gap, 10 mm to 40 mm max.

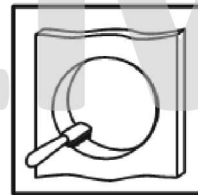
Section

Notes:

Solution and restrictions based on Hilti ETA No. 10/0292 Report and also Hilti Australia Opinion FCO-2038.

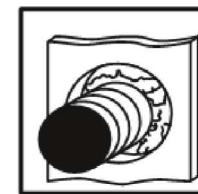
If an insulation rating is required of the fire rated system, the metal pipe will need to be lagged with Rockwool on both sides of the penetration. Contact the Engineer for details.

1.



Clean opening. Surfaces to be dry and free of loose debris, dirt, oil, wax or grease.

2.



Insert pipe and provide Rockwool backfilling, leave sufficient depth for application of sealant.

3.



Fill around services with CP 606 for the required depth.

4.



For penetrations exposed to view, smooth before skin forms using water (permissible to use diluted liquid soap) and spatula. Leave completed seal undisturbed for 48 hrs.

Installation Instructions

This sketch does not constitute a complete fire engineering design or detail. Detailed construction drawings are provided by others. Best viewed in colour. Not all fire separations around ducts and shafts are shown.

Legend



Holmes Fire LP  
holmesfire.com

Project Title

HWCP

Sketch Title

Metal Pipe through  
Concrete Walls, Annular  
Gap up to 40 mm Integrity  
Only. Hilti CP606 Solution

Drawn: DXM

Date: 21 / 10 / 2019

Project No.

136249

Sheet No.

CW-P-01

Rev

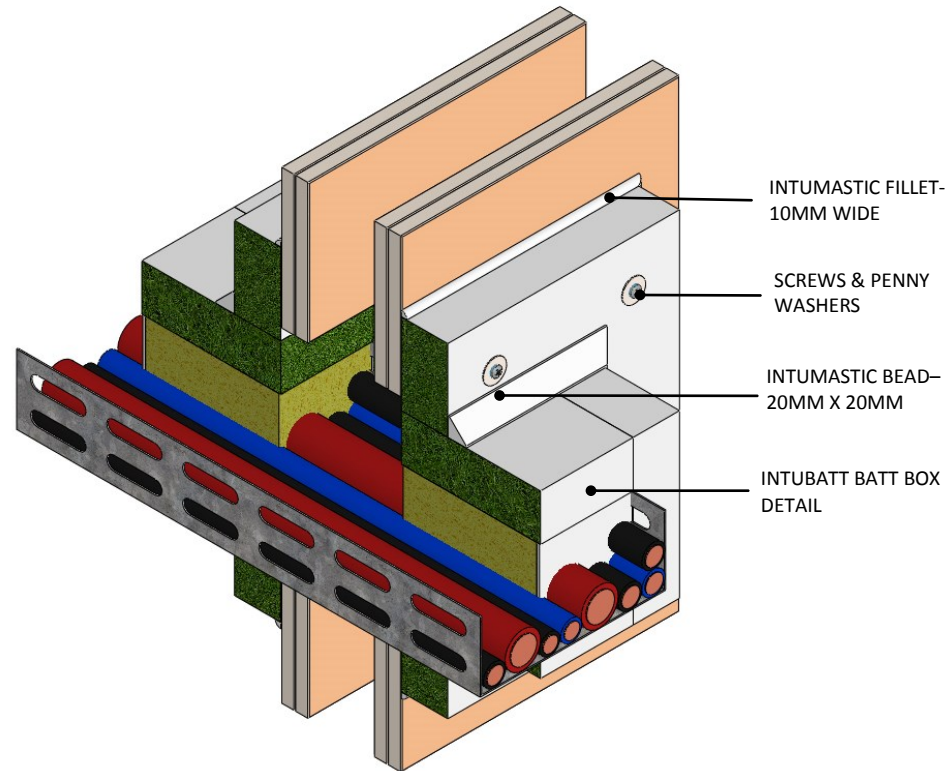
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1. ENSURE THE APERTURE IS CLEAN AND FREE OF DEBRIS AND LOOSE CEMENT. REMOVE DUST FROM SURFACES REQUIRING INSTALLATION.
2. CUT THE INTUBATT TO FORM THE BATT BOX DETAIL AROUND THE CABLE TRAY, AS PER THE BATT BOX DETAIL DRAWING V44.
3. POSITION THE BATT BOX AROUND THE PENETRATION AND POSITION THE BACK EDGE OF THE BATT BOX IN LINE WITH THE BACK SIDE OF THE PROPOSED INTUBATT FIRE SEAL.
4. CUT THE INTUBATT TO THE REQUIRED SIZE AND SHAPE, ENSURING THE INTUBATT WILL OVERLAP THE PLASTERBOARD 100MM AROUND THE OPENING..
5. CUT THE INTUBATT TO TIGHTLY FIT AROUND THE BATT BOX DETAIL.
6. CUT THE INTUBATT ACROSS THE SHORTEST DIMENSION INCORPORATING THE MIDPOINT OF THE PENETRATION, TO ENABLE THE INTUBATT TO BE FITTED ON TO THE PLASTERBOARD/MASONRY.
7. APPLY INTUMASTIC TO THE PLASTERBOARD/ MASONRY WHERE THE INTUBATT IS TO BE FITTED.
8. APPLY INTUMASTIC BRUSH GRADE TO ALL EDGES OF THE INTUBATT, ENSURING THAT AN EVEN COVERAGE IS ACHIEVED OVER THE ENTIRE EXPOSED THICKNESS OF THE INTUBATT. THIS SHOULD INCLUDE THE OUTER EDGES OF THE INTUBATT AND THE CUT ACROSS TO ALLOW INSTALLATION IN TO THE APERTURE.
9. OFFER INTUBATT UP TO PLASTERBOARD WALL AROUND THE INSTALLED BATT BOX.
10. FIX THE INTUBATT TO THE PLASTERBOARD/MASONRY USING MINIMUM 75MM LONG STEEL SCREWS AND 25MM DIAMETER STEEL WASHERS. FIXINGS SHOULD NOT EXCEED 50MM FROM ANY EDGE AND NOT EXCEED 200MM CENTRES.
11. APPLY AN INTUMASTIC FILLET APPROXIMATELY 10MM WIDE TO THE PERIMETER OF THE INTUBATT WHERE IT MEETS THE PLASTERBOARD, AND 20MM X 20MM BEAD AROUND THE BATT BOX DETAIL. ENSURE THAT ALL GAPS BETWEEN THE INTUBATT AND THE SURROUNDING EDGES ARE FULLY FILLED USING INTUMASTIC.
12. REPAIR ANY DAMAGES TO THE COATING WHICH MAY HAVE OCCURRED DURING INSTALLATION USING BRUSH OR SPRAYING APPLICATION OF INTUMASTIC.
13. REPEAT THE ABOVE TO THE OPPOSITE SIDE OF THE WALL.



**Notes**

**Products:** INTUBATT BATT BOX DETAIL AS 1530.4/AS 4072.1

**Approval:** 1

**BK:** 35084000

**Ref:**

**ID:** 35

**Scenario:** Penetration seal to cable tray.

**Construction:** Fire rated gypsum wall.

**Fire Integrity:** 120 minutes.

**Insulation:** 120 minutes.

**Services:** Cable Tray up to 500mm wide  
Standard cable configuration  
BSEN 1366.

Web based drawings are for example only, fire performance of any system is dependant on, but not limited to size of opening, substrate, if penetrations are passing through, type, size and number. Please refer to Ryanfire technical department for detailed and specific fire performance information.



Client

Job Title

Drawing Title  
**Batt Box detail to Cable Tray in Gypsum Fire Wall**

Scale <b>NTS</b>	Date <b>July 2019</b>
Sheet Size <b>A3</b>	Drawn By
Drawing Number <b>V32</b>	Rev <b>2.0</b>

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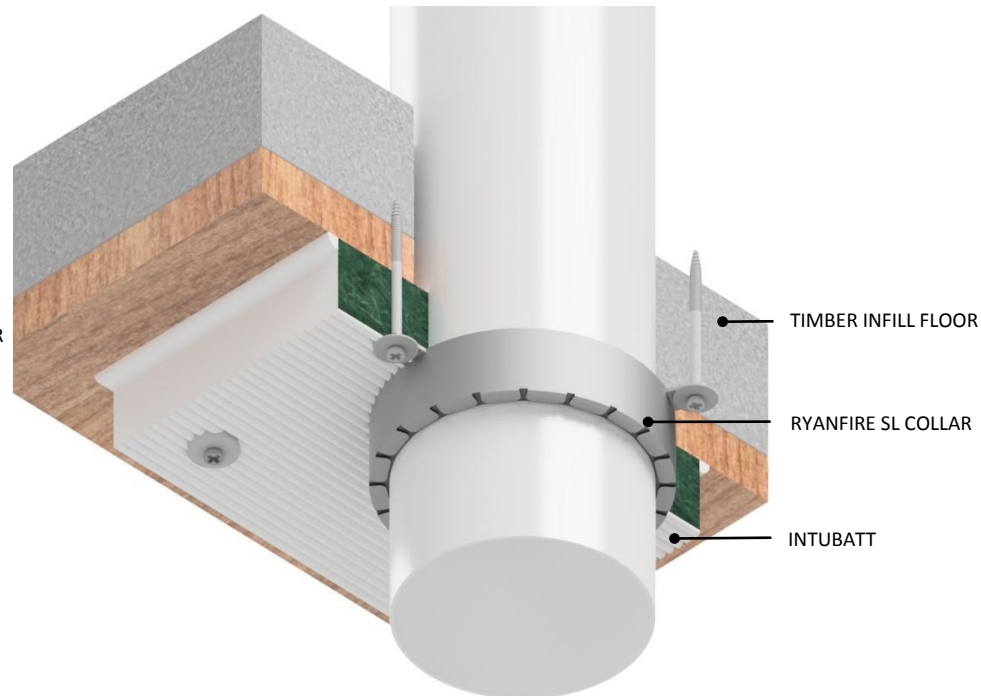
**2019/1381**

RYANFIRE SL COLLAR  
 AS 1530.4/AS 4072.1

**Products:**  
**Approvals:** 49 / 50  
**BK:** 51892400 / 51892200  
**Ref:** Service C / B  
**ID:**  
**Scenario:** Penetration seal to combustible pipe  
**Construction:** Timber infill floor (75mm concrete 25mm timber sarking).  
**Fire Rating:**  
**PVC pipe -** Integrity 60 minutes. Insulation: 60 minutes.  
**HDPE pipe-** Integrity 30 minutes. Insulation 15 minutes.  
**Services:** Up to 160mm dia. PVC pipe. Up to 160mm dia. HDPE pipe.

**INSTALLATION INSTRUCTIONS**

1. ENSURE THE APERTURE IS CLEAN, FREE OF DEBRIS, LOOSE CEMENT AND DUST.
2. CUT THE INTUBATT TO THE CORRECT SIZE TO FIT TIGHTLY AROUND THE SERVICE PENETRATION AND OVERLAP THE TIMBER SARKING AROUND THE APERTURE BY 100MM.
3. APPLY INTUMASTIC (WHITE) TO THE BACK SIDE OF THE INTUBATT AND PRESS FIRMLY INTO POSITION AROUND THE PIPE.
4. SECURE THE INTUBATT TO THE UNDERSIDE OF THE TIMBER INFILL FLOOR USING 100MM LONG MILD STEEL SCREWS & 25MM WASHERS POSITIONED 50MM FROM THE EDGE OF THE INTUBATT AND NOT EXCEEDING 200MM CENTRES.
5. SELECT THE CORRECT DIAMETER RYANFIRE SL COLLAR FOR THE COMBUSTIBLE PIPE.
6. APPLY INTUMASTIC (WHITE) AROUND THE PIPE TO SMOKE SEAL THE OPENING.
7. POSITION THE RYANFIRE SL COLLAR AROUND THE PENETRATION AND FASTEN AROUND THE PIPE.
8. SLIDE THE COLLAR ALONG THE PIPE UNTIL IT IS HARD UP AGAINST THE UNDERSIDE OF THE INTUBATT.
9. FIX THE COLLAR IN PLACE USING 100MM LONG MILD STEEL SCREWS & WASHERS. ENSURE ALL FIXING POINTS ARE USED AND THE SCREWS EMBED THE SOLID CONCRETE SUBSTRATE BY MIN. 25MM.
10. APPLY INTUMASTIC BRUSH GRADE TO ALL EXPOSED INTUBATT EDGES. REPAIR ANY DAMAGE TO THE COATING THAT MAY HAVE OCCURRED DURING INSTALLATION USING BRUSH OR SPRAY APPLICATION OF INTUMASTIC.



Web based drawings are for example only, fire performance of any system is dependant on, but not limited to size of opening, substrate, if penetrations are passing through, type, size and number. Please refer to Ryanfire technical department for detailed and specific fire performance information.



Client  
 Job Title

Drawing Title  
**Ryanfire SL Collar - Combustible Pipe through Timber Infill Floor**

Scale <b>NTS</b>	Date <b>July 2019</b>
Sheet Size <b>A3</b>	Drawn By
Drawing Number <b>V22.3</b>	Rev <b>2.0</b>

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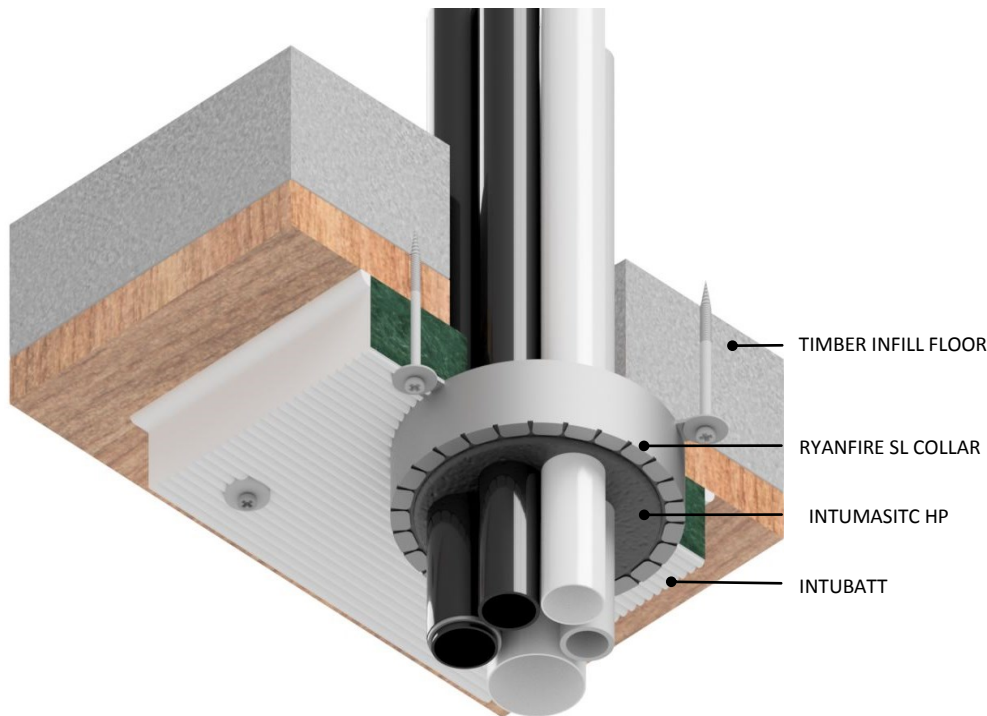
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**INSTALLATION INSTRUCTIONS**

1. ENSURE THE APERTURE IS CLEAN, FREE OF DEBRIS, LOOSE CEMENT AND DUST.
2. CUT THE INTUBATT TO THE CORRECT SIZE TO FIT TIGHTLY AROUND THE SERVICE PENETRATIONS AND OVERLAP THE TIMBER SARKING AROUND THE APERTURE BY 100MM.
3. APPLY INTUMASTIC (WHITE) TO THE BACK SIDE OF THE INTUBATT AND PRESS FIRMLY INTO POSITION AROUND THE SERVICES.
4. SECURE INTUBATT TO THE UNDERSIDE OF THE TIMBER INFILL FLOOR USING 100MM LONG MILD STEEL SCREWS & 25MM WASHERS POSITIONED 50MM FROM THE EDGE OF THE INTUBATT AND NOT EXCEEDING 200MM CENTRES.
5. SELECT THE CORRECT DIAMETER RYANFIRE SL COLLAR FOR SERVICE PENETRATIONS UP TO 160MM DIA SL COLLAR.
6. POSITION THE RYANFIRE SL COLLAR AROUND THE PENETRATION AND FASTEN INTO POSITION .
7. SLIDE THE COLLAR ALONG UP TO THE UNDERSIDE OF THE INTUBATT SEAL.
8. FIX THE COLLAR IN PLACE USING 100MM LONG MILD STEEL SCREWS & WASHERS. ENSURE ALL FIXING POINTS ARE USED AND THE SCREWS EMBED THE SOLID CONCRETE SUBSTRATE BY MIN. 25MM.
9. APPLY INTUMASTIC HP TO FILL THE ANNULAR GAP TO THE FULL DEPTH OF THE RYANFIRE SL COLLAR.
10. APPLY INTUMASTIC BRUSH GRADE TO ALL EXPOSED INTUBATT EDGES. REPAIR ANY DAMAGE TO THE COATING THAT MAY HAVE OCCURRED DURING INSTALLATION USING BRUSH OR SPRAY APPLICATION OF INTUMASTIC.



**Products:** RYANFIRE SL COLLAR  
INTUMASTIC HP  
AS 1530.4/AS 4072.1

**Approvals:** 50

**BK:** 51892200

**Ref:** 51892200

**ID:** Service D

**Scenario:** Penetration seal to multiple combustible pipes.

**Construction:** Timber infill floor (75mm concrete 25mm timber sarking).

**Aperture:** 150mm dia.

**Fire Integrity:** 60 minutes.

**Services:** Up to 25mm dia conduit, 22mm dia. buteline pipe, 32mm rehaul rautitan pipe, 32mm rehaul PEX - AL pipe, 50mm PVC pipe.

Web based drawings are for example only, fire performance of any system is dependant on, but not limited too - size of opening, substrate, if penetrations are passing through, type, size and number. Please refer to Ryanfire technical department for detailed and specific fire performance information.



Client

Job Title

Drawing Title

**Multi Combustible Service Penetration Through Timber Infill**

Scale	Date
<b>NTS</b>	<b>July 2019</b>

Sheet Size	Drawn By
<b>A3</b>	

Drawing Number	Rev
<b>V22.5</b>	<b>2.0</b>

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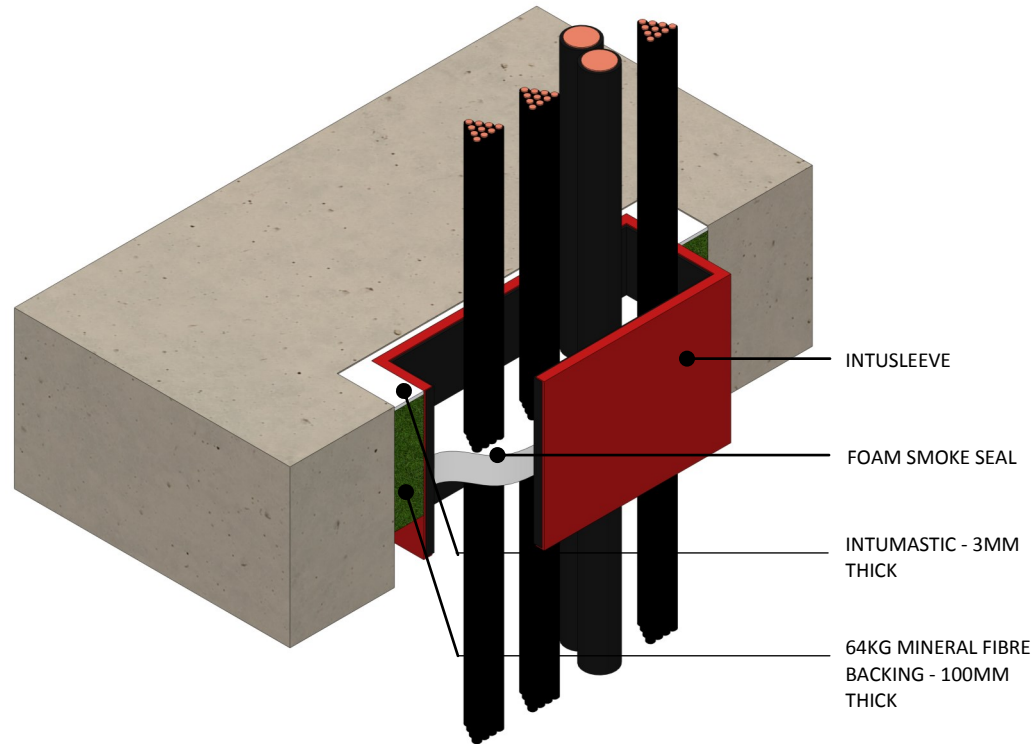
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**BUILDING CONSENT NUMBER**  
**2019/1381**  
 CABLE TRANSIT & INTUMASTIC

**INSTALLATION INSTRUCTIONS**

1. ENSURE THE APERTURE IS CLEAN AND FREE OF DEBRIS AND LOOSE CEMENT. REMOVE ALL DUST FROM SURFACES REQUIRING INSTALLATION.
2. SELECT THE CORRECT SIZE INTUSLEEVE.
3. FIT AROUND THE CABLES AND SECURE BY COMPRESSION FITTING THE 25MM THICK SMOKE SEAL (FOAM) TIGHTLY WITHIN THE INTUSLEEVE AND AROUND THE CABLES.
4. FIT 100MM DEPTH OF 64KG MINERAL FIBRE BETWEEN THE INTUSLEEVE AND CONCRETE FLOOR OPENING, FORMING A 3MM RECESS FROM THE TOP OF THE CONCRETE FLOOR.
5. APPLY 3MM THICKNESS OF INTUMASTIC TO THE RECESS AROUND THE INTUSLEEVE.
6. CLEAN EXCESS INTUMASTIC USING A DAMP CLOTH.



**Products:**  
**Approvals:** AS 1530.4/AS 4072.1  
**BK:** 1  
**Ref:** 35084000  
**ID:** 38  
**Scenario:** Floor seal to various cables passing through intusleeve cable management sleeve.  
**Penetrations:** **Cables**  
 2no type E  
 10no type A1  
 10no type A2  
 14no 3 core, twin and earth  
**Construction:** Nominal 150mm concrete floor.  
**Fire Integrity:** 120 minutes.  
**Insulation:** 30 minutes.

Web based drawings are for example only, fire performance of any system is dependant on, but not limited to size of opening, substrate, if penetrations are passing through, type, size and number. Please refer to Ryanfire technical department for detailed and specific fire performance information.



Client

Job Title

Drawing Title  
**Intusleeve, Cable Management Floor Seal.**

Scale <b>NTS</b>	Date <b>July 2019</b>
Sheet Size <b>A3</b>	Drawn By
Drawing Number <b>V40</b>	Rev <b>2.0</b>

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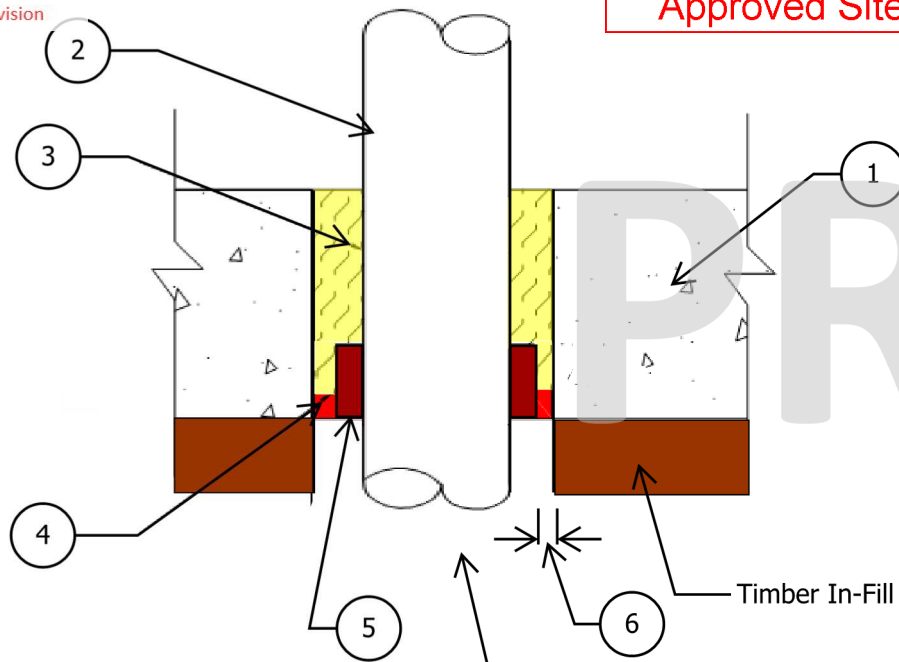
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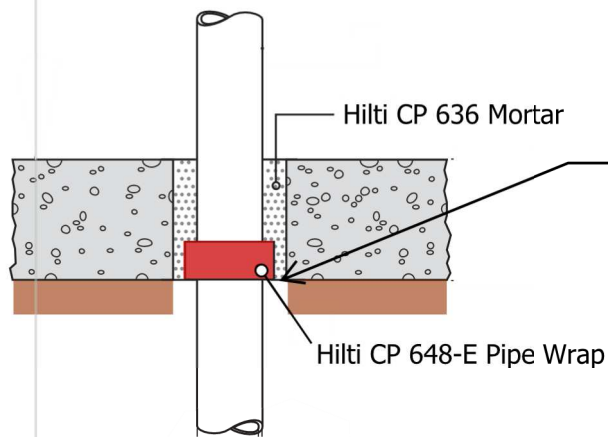


Section

- 1 = Concrete Floor
- 2 = Plastic Pipe uPVC and PE 150 mm dia max.
- 3 = Rockwool backfilling.
- 4 = Hilti CP606 Sealant. Minimum Depth 15 mm.
- 5 = Hilti CP 648-E Pipe Wrap (number of layers dependent on pipe dia. - refer Notes)
- 6 = Annular Gap, 10 mm max for sealing with CP 606. Refer also Below.

Pipe supported both sides  
maximum 300 mm from  
floor.

Alternative Back-Fill (for oversized Core Holes)



Install wrap, provide temporary shuttering to underside of the hole and pour 636 Mortar from above. Remove shuttering once cured. Pipe Wrap must be visible from below and be flush with the underside of the concrete slab/mortar backfill.

Restrictions/Notes:

System is from Hilti Australia Technical Datasheet for CP648-E which is based on Hilti Australia FCO-23013909. This document refers only to uPVC pipes up to 150 mm through floors. The Hilti European Technical Datasheet ETA-10/0405 documents the same system for uPVC and PE pipes up to 160 mm dia. It is therefore considered the system detailed opposite can be suitably used for PE pipes up to 150 mm dia.

Number of Layers of 648-E

Pipes up to and including 65 mm dia. only require 1 layer of CP 648.

Pipes >65 mm and to 100 mm dia. require two layers of wrap.

Pipes >100 mm and to 150 mm dia. require three layers of wrap.

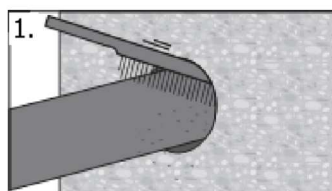
The wrap is 5 mm thick.

Core holes are to be sized appropriately, e.g:

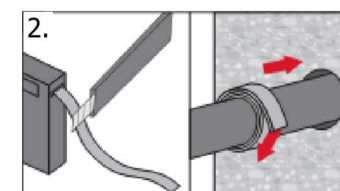
For pipes up to 65 mm dia. the core hole is to be = pipe outer dia. + 10 mm (1 layer of pipe wrap) + maximum 20 mm (CP 606 seal).

For pipes >65 mm to 100 mm dia. the core hole is to be = pipe outer dia. + 20 mm (2 layers of pipe wrap) + a maximum 20 mm (CP 606 seal).

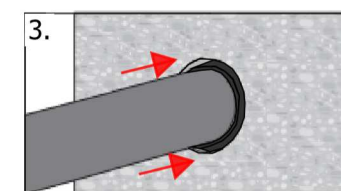
For pipes >100 mm to 150 mm dia. the core hole is to be = pipe outer dia. + 30 mm (3 layers of pipe wrap) + a maximum 20 mm (CP 606 seal).



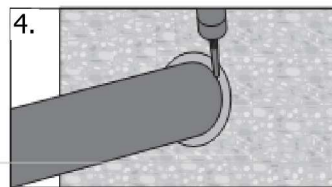
Clean opening and the pipe where the wrap is to be placed. Surfaces to be dry and free of loose debris, dirt, oil, wax or grease.



Cut the wrap to length according to outer diameter of pipe and accounting for required number of layers. Wrap the wrap around the pipe the required number of times and secure with adhesive tape.



Push wrap into opening until the outer edge is flush with the bottom of the concrete of the flooring system.



Fill remainder of annular space between the wrap and the opening edge with CP606. Do Not cover the bottom of the wrap with mastic.

NOTE:  
Multiple layers to be concentric (i.e. overlap each other) and layers need to be finished flush with the underside of the concrete.

Installation Instructions

This sketch does not constitute a complete fire engineering design or detail. Detailed construction drawings are provided by others. Best viewed in colour. Not all fire separations around ducts and shafts are shown.

Legend



Holmes Fire LP  
holmesfire.com

Project Title

HWCP

Sketch Title

Plastic Pipe (uPVC, PE) up to 150 mm Dia Penetration through Concrete Floors Hilti CP648-E Solution

Drawn: DXM

Date: 22 / 10 / 2019

Project No.

136249

Sheet No.

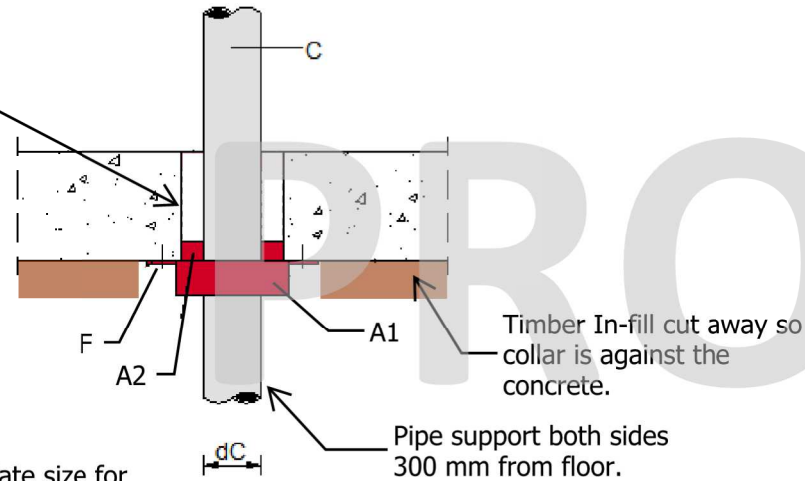
CF-P-04

Rev

A

Plastic Pipe Penetrations Through  
Concrete Floors

Core drill hole in concrete,  
diameter to be less than  
the outside diameter of the  
required collar for the pipe  
size.



dC = Pipe Diameter. Refer Notes.

C = Pipe type. Refer Notes.

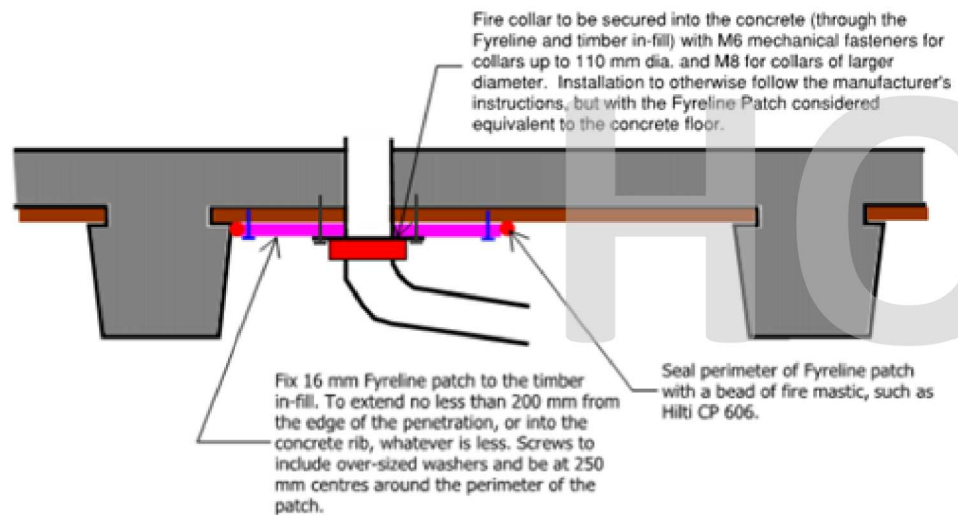
A1 = Hilti CP644 Fire Collar, of appropriate size for  
the pipe size fitted to underside of floor.

A2 = Hilti CP606 Fire Mastic, for depth of 10 mm min.

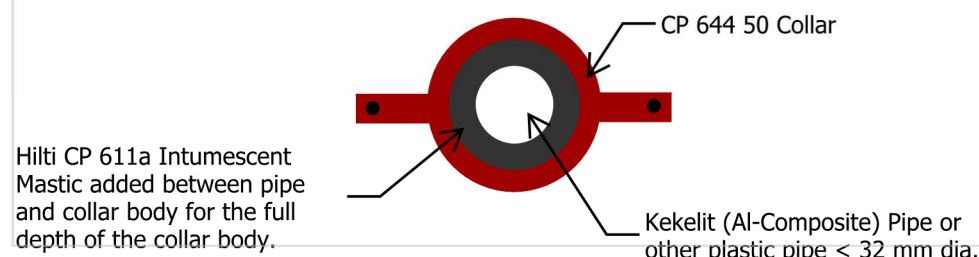
F = Fastening Hook and Anchor. Refer Installation Instructions and Notes.

Section

**Alternatively -**  
Follow Specification and  
Protect the Timber with  
Fyreline and Mount Collar to  
Underside of Fyreline.



Treatment of Kekelit pipes  
(and other plastics) < 32 mm diameter.



Notes:

Solution is based on Hilti Australia CP 644 Technical Data Sheet referencing Report No. EWFA 27006-01. The Aluminium Composite (e.g. Kekelit Kelox) solution is based on Technical Approval ETA No. 10/0404.

Solution is applicable for:

- Raupiano Plus pipes up to 110 mm dia.,
- uPVC pipes up to 150 mm dia.,
- PE pipes up to 125 mm dia.
- PPR pipes up to 125 mm dia.
- Al - Composite up to 63 mm dia.

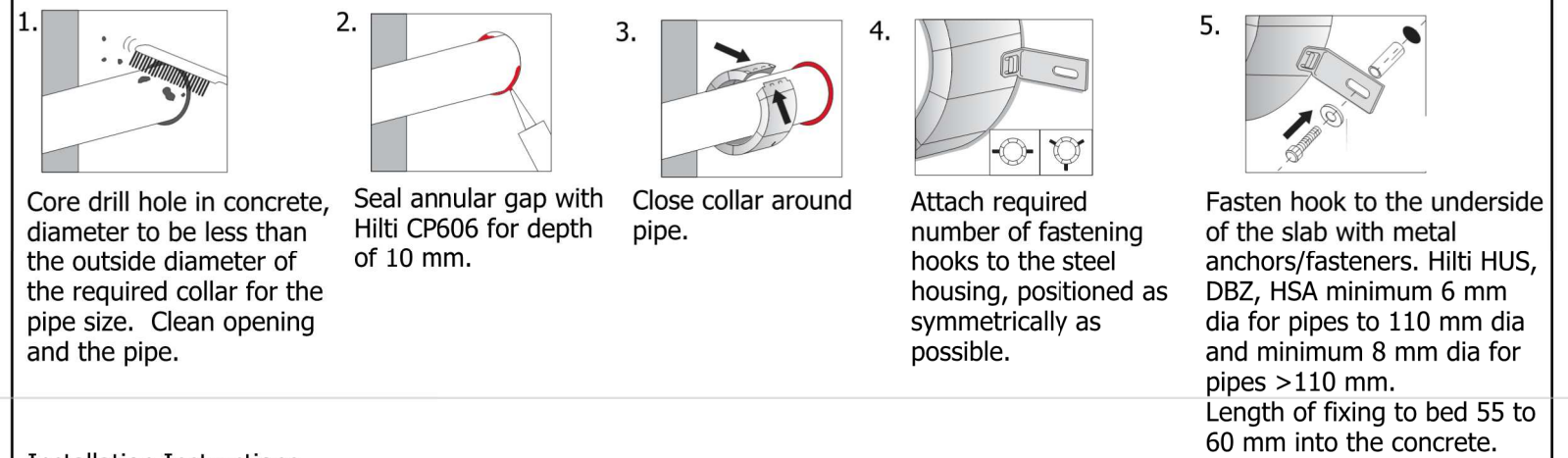
For plastic pipes less than 32 mm in diameter of the types noted above with the exception of Al-Composite, and for conduits (with or without cables) refer to the Hilti CP 611a solution. Alternatively use same detail as that opposite for Kekelit Pipes.

Collar Size Selector:

	Pipe diameter - range	Collar outside diameter	Height
CP 644 50/1.5"	32 - 51 mm	66.7 mm	22.4 mm
CP 644 63/2"	52 - 64 mm	81.7 mm	32.4 mm
CP 644 75/2.5"	65-78 mm	101.7 mm	32.4 mm
CP 644 90/3.5"	75 - 91 mm	116.7 mm	42.4 mm
CP 644 110/4"	92 - 115 mm	145.7 mm	47.4 mm
CP 644 125/5"	116 - 125 mm	166.1 mm	47.8 mm
CP 644 160/6"	126 - 170 mm	235.5 mm	48.2 mm
CP 644 200/8"	200 mm	257 mm	177.5 mm

Collar sizes and number of hooks  
for suitable pipe diameters

	CP 644 50/1,5" - 2		CP 644 160/6" - 6
	CP 644 63/2" - 2		
	CP 644 75/2,5" - 3		CP 644 200/8" - 8
	CP 644 90/3" - 3		
	CP 644 110/4" - 4		
	CP 644 125/5" - 4		



Installation Instructions

This sketch does not constitute a complete fire engineering design or detail. Detailed construction drawings are provided by others. Best viewed in colour. Not all fire separations around ducts and shafts are shown.

Legend



Holmes Fire LP  
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Project Title

HWCP

Sketch Title

Plastic Pipe Penetrations  
through Concrete Floors

Hilti CP644 Solution

Drawn: DXM

Date: 22 / 10 / 2019

Project No.

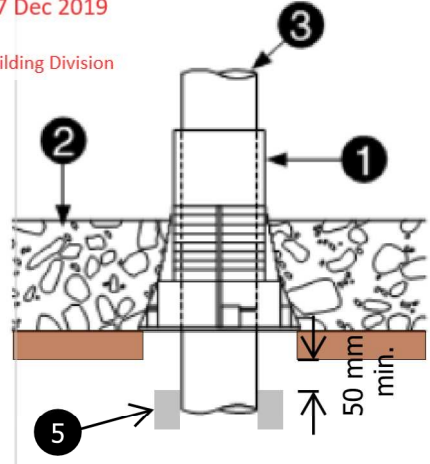
136249

Sheet No.

CF-P-05

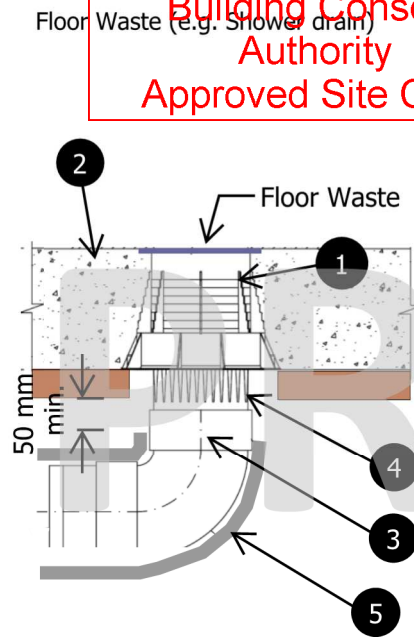
Rev

A



- 1 = Cast in CP 680-N collar. Refer Notes.
- 2 = Concrete Floor
- 3 = Plastic Pipe. Refer Notes
- 4 = RAD Device. Refer Notes
- 5 = Acoustic Insulation. To not extend closer than 50 mm to the underside of the timber in-fill.

Section



Restrictions/Notes:

Solution based on CSIRO report FCO 2285/CO3975 for installation of CP 680 in an Ultra-Floor system and CSIRO report FCO-3117 for installation of CP 680 in 100 mm thick Stanton Floor.

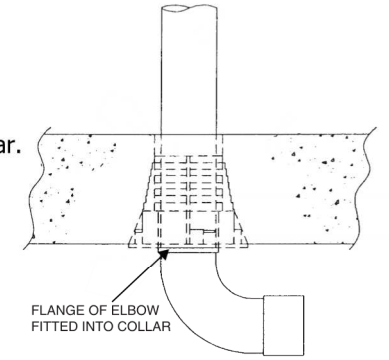
Solution is suitable for following Plastic Pipes:

- PP to 110 mm
- PP-R to 110 mm
- PE to 160 mm
- HDPE to 160 mm
- uPVC to 150 mm

Note: For Stack Pipe Configuration and uPVC pipe and pipe fittings the elbow fitting may be in the collar.

Collar Size 75/2.5" protects pipes 32 mm to 75 mm dia.  
Collar Size 110/4" protects pipes 80 mm to 110 mm dia.  
Collar Size 160/6" protects pipes 125 mm to 160 mm dia.

**RAD device** is a separate retro-fit collar to be installed from below. Make notches in the timber in-fill to accommodate the device where it is required (for floor waste applications).



1. Use the correct size collar - refer Notes.

2. The timber deck is cut away to completely expose the metal ring at the bottom of the CP 680 N collar. The cutaway section is required to be within the following dimensions:

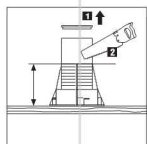
Hilti Firestop Collar Size	Minimum Hole Diameter	Maximum Hole Diameter
CP 680-75/2.5"	122	142
CP 680-110/4"	175	195
CP 680-160/6"	242	262

3. Nail the collar in place centred over the hole. Secure the top cap in place prior to concrete pour to prevent flow of concrete into the cast-in collar.

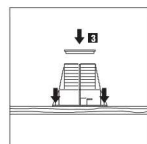
4. Pour concrete and once set remove protective cap and install pipe. Pipe may be installed from above or below.

5. Any insulation to the pipe is to be maintained 50 mm below the level of the timber in-fill

Height adjustment For Floor Wastes



1 Remove the top cap, and cut the device to the right slab thickness



2 Replace the top cap and make sure it fits correctly.

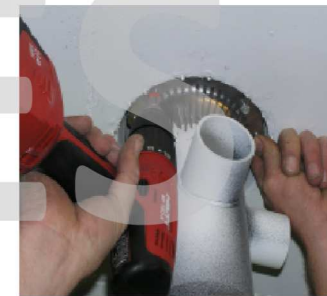
Hilti Retrofit addition CP 680 110/4" N-RAD : Installation Guidelines:



**Step 1: Place to Install:**

Place the RAD with the Red surface facing the bottom of the installed Hilti Fire Collar.

You only need 30mm clearance from the bottom of the slab to do this, and more space is even better.



**Step 4: Drill to Install:**

Screw the RAD so that it is securely fixed into the metal ring in the bottom of the Hilti Fire Collar.

Use a Hex Head socket, and a cordless screw-gun with sufficient torque to drill the screws into the metal ring.



**Step 2: Rotate to Install:**

Leverage the RAD so that the Red surface becomes visible from the bottom of the collar.

Even with only 30mm clearance from the bottom of the slab you can do this. With more space it is very easy to do this.



**Step 5: Meet to Install:**

Position the second half of the RAD so that it meets, but does not overlap, the first half of the RAD.

Then repeat steps 1 – 4 above.

RAD install time should be less than 2 minutes.



**Step 3: Push to Install:**

Push the RAD so that the Red surface becomes 100% visible from the bottom of the collar.

The RAD will fit tightly into the bottom of a Hilti Fire Collar, and hold in place for the screws to be inserted into the pre-drilled holes.

Installation Instructions

This sketch does not constitute a complete fire engineering design or detail. Detailed construction drawings are provided by others. Best viewed in colour. Not all fire separations around ducts and shafts are shown.

Legend



Holmes Fire LP  
holmesfire.com

Project Title

HWCP

Sketch Title

Plastic Pipes up to 160 mm Dia., Penetrations through Concrete Floors Cast in Hilti CP648-E Solution

Drawn: DXM

Date: 22 / 10 / 2019

Project No.

136249

Sheet No.

CF-P-06

Rev

A

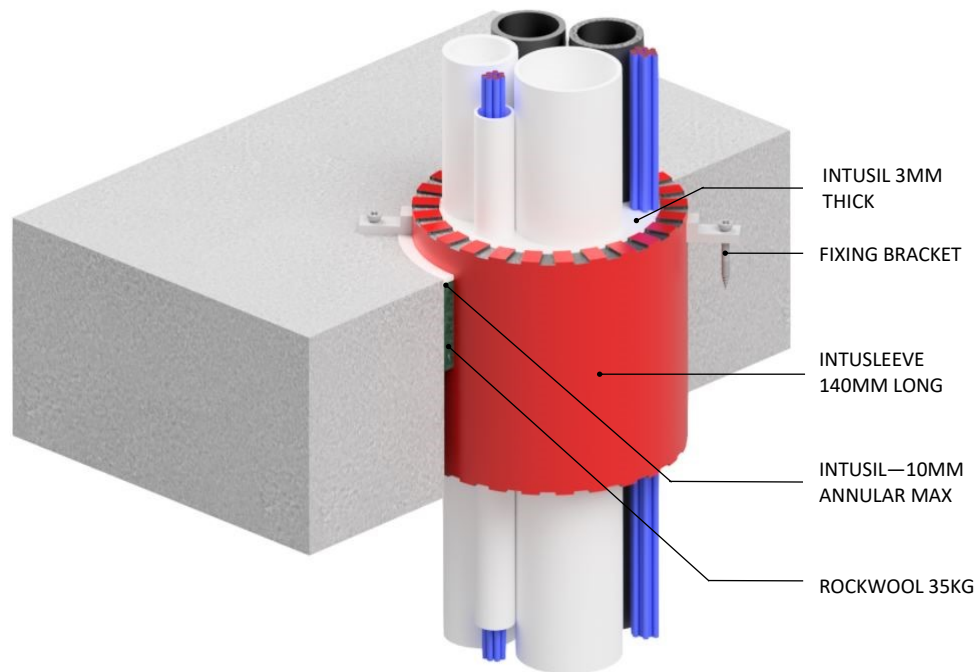
**Invercargill City Council**  
**Building Consent Authority**  
**Approved Site Copy**

**Approved For Issue**  
**27/02/2020**

**BUILDING CONSENT NUMBER**  
**2019/1381**  
 INTUSIL & INTUSLEEVE  
 AS 1530.4/AS 4072

**INSTALLATION INSTRUCTIONS**

1. ENSURE THE APERTURE IS CLEAN AND FREE OF DEBRIS AND LOOSE CEMENT. REMOVE DUST FROM SURFACES REQUIRING INSTALLATION.
2. SELECT CORRECT DIAMETER INTUSLEEVE (140MM LONG) FOR SERVICE PENETRATIONS.
3. SECURE 150X20X2MM L BRACKETS TO INTUSLEEVE USING STEEL SELF TAPPING SCREWS TO SUIT INTUSLEEVE WALL THICKNESS.
4. POSITION THE INTUSLEEVE AROUND THE SERVICE PENETRATION.
5. FIX INTUSLEEVE TO TOP OF THE CONCRETE FLOOR USING SUITABLE MILD 40MM LONG STEEL FIXINGS.
6. APPLY 60MM THICK 35KG ROCKWOOL AROUND INTUSLEEVE, CREATING A 3MM DEEP RECESS FROM THE TOP OF THE CONCRETE FLOOR.
7. FILL 3MM DEEP RECESS WITH INTUSIL.
8. APPLY 3MM INTUSIL TO ANY GAPS WITHIN INTUSLEEVE.
9. CLEAN EXCESS MATERIAL AWAY USING A DAMP CLOTH.



Notes

**Products:**  
**Approvals:**  
**BK:** 4  
**Ref:** T35319300  
**ID:** 44

**Scenario:** Penetration seal to multiple service penetrations

**Construction:** Concrete floor 150mm

**Fire Rating:** Integrity: 240 minute  
 Insulation: 60 minute

**Service Penetrations:** Fibre optic cables through PVC conduit, Fibre optic cable bundle, Twin & Earth cable bundle, PE Pipes, & PVC pipes

Web based drawings are for example only, fire performance of any system is dependant on, but not limited too - size of opening, substrate, if penetrations are passing through, type, size and number - please refer to Ryanfire technical department for detailed and specific fire performance information.



Client

Job Title

Drawing Title

**Intusleeve to Multiple Service Penetration - Concrete Floor**

Scale	NTS	Date	Oct 2017
Sheet Size	A3	Drawn By	
Drawing Number	V63.1	Rev	1.0

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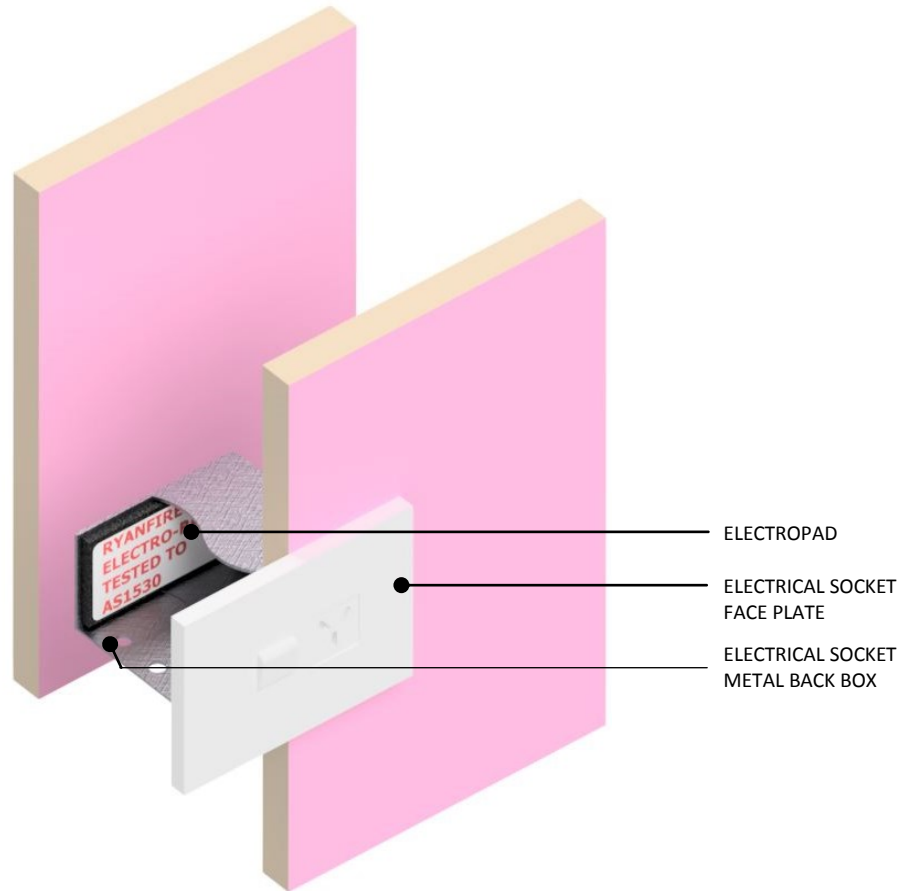
**Invercargill City Council**  
**Building Consent Authority**  
**Approved Site Copy**

**Approved For Issue**  
**27/02/2020**

**BUILDING CONSENT NUMBER**  
**2019/1381**

**INSTALLATION INSTRUCTIONS**

1. ENSURE ELECTRICAL SERVICES ARE ISOLATED PRIOR TO ANY WORKS BEING UNDERTAKEN.
2. REMOVE ELECTRICAL FACE PLATE.
3. ENSURE THE APERTURE IS CLEAN AND FREE OF DEBRIS AND LOOSE CEMENT. REMOVE ALL DUST FROM SURFACES REQUIRING INSTALLATION.
4. SELECT THE ELECTROPAD TO FIT WITHIN THE ELECTRICAL BACK BOX.
5. APPLY INTUMASTIC TO THE BACK OF THE ELECTRICAL BOX TO ENABLE THE ELECTROPAD PAD TO BE ADHERED IN PLACE. FIRMLY COMPRESS THE ELECTROPAD TO BACK OF THE ELECTRICAL BOX.
6. FILL ALL THE GAPS BETWEEN THE PLASTERBOARD OPENING AND ELECTRICAL BOX WITH INTUMASTIC.
7. REMOVE EXCESS INTUMASTIC USING A DAMP CLOTH.
8. REFIT ELECTRICAL FACE PLATE.



**Products:** ELECTROPAD  
**Approval:** AS 1530.4/AS 4072.1  
**BK:** 1  
**Ref:** 35084000  
**ID:** 29/30  
**Scenario:** Electrical socket and metal back box fitted through gypsum fire wall.  
**Penetrations:** Electrical socket metal back box.  
**Construction:** 95mm x 45mm Softwood section studwork. 13mm fire rated plasterboard fixed to both sides of studwork.  
**Fire Integrity:** 60 minutes.  
**Insulation:** 60 minutes.

Web based drawings are for example only, fire performance of any system is dependant on, but not limited to size of opening, substrate, if penetrations are passing through, type, size and number. Please refer to Ryanfire technical department for detailed and specific fire performance information.



Client

Job Title

Drawing Title  
**Electropad Gypsum Fire Wall.**

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Scale <b>NTS</b>	Date <b>July 2019</b>
Sheet Size <b>A3</b>	Drawn By
Drawing Number <b>V37</b>	Rev <b>2.0</b>

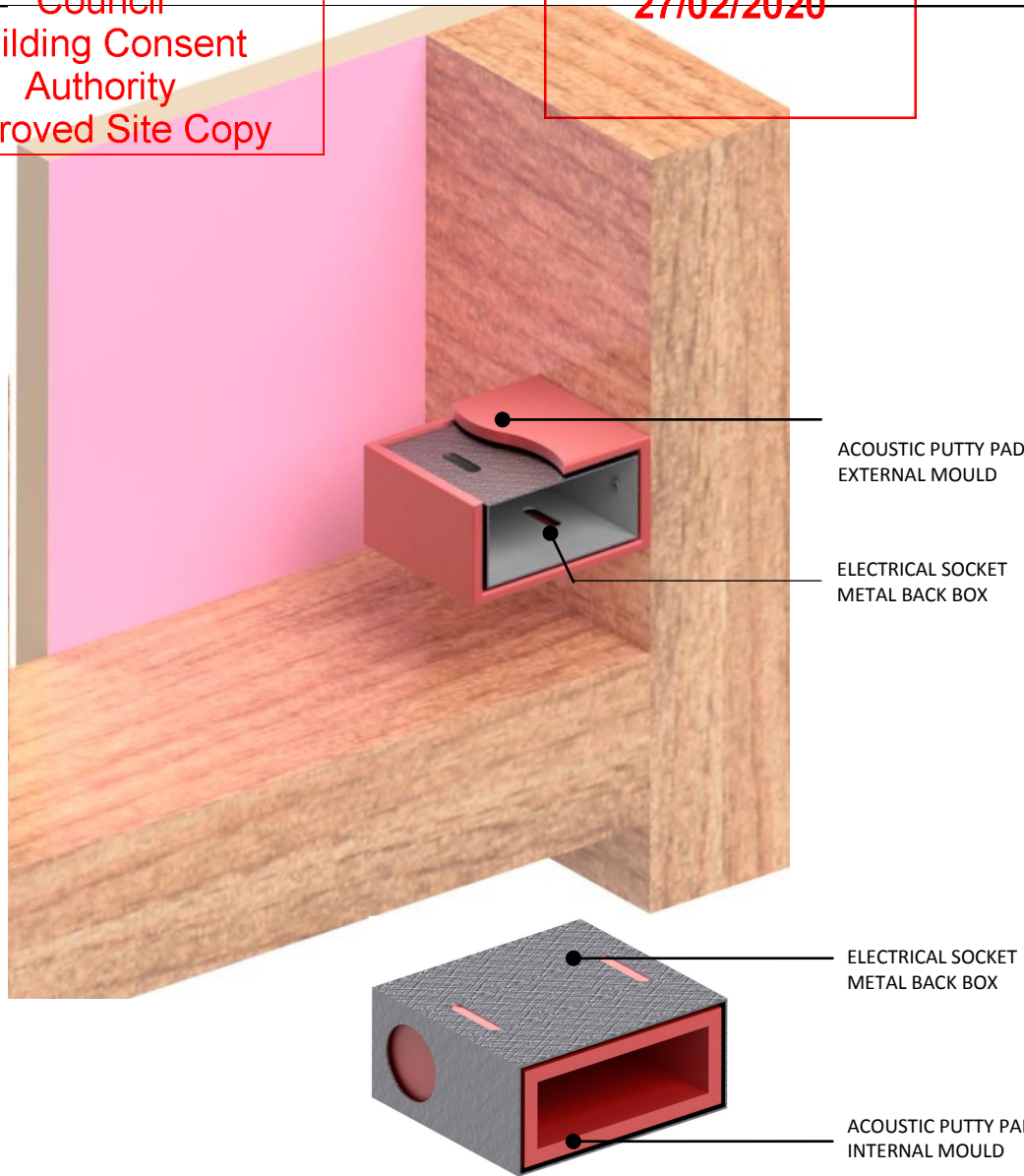
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 27/02/2020

BUILDING CONSENT NUMBER  
 2019/1381

**INSTALLATION INSTRUCTIONS**

1. ENSURE ELECTRICAL SERVICES ARE ISOLATED PRIOR TO ANY WORKS BEING UNDERTAKEN.
2. ENSURE THE APERTURE IS CLEAN AND FREE OF DEBRIS. REMOVE ALL DUST FROM SURFACES REQUIRING INSTALLATION.
3. SELECT PUTTY PADS TO FIT AROUND ELECTRICAL BACK BOX.
4. MOULD AROUND ELECTRICAL BACK BOX TO ENSURE THE ENTIRE BOX IS ENCLOSED/SURROUNDED.
5. FIX ELECTRICAL BACK BOX INTO POSITION AS PER MANUFACTURERS INSTRUCTIONS.
6. FILL ALL GAPS BETWEEN THE PLASTERBOARD OPENING AND ELECTRICAL BOX WITH INTUMASTIC.
7. FIT ELECTRICAL FACE PLATE.



**Products:** RYANFIRE  
**Approval:** AS 1530.4/AS 4072.1  
**BK:** 46 / 51 / 52  
**Ref:** 51028300 / 56662701 / 51892000  
**ID:** A, B / C / D  
**Scenario:** Electrical socket and metal back box fitted through gypsum fire wall.  
**Penetrations:** Electrical socket metal back box.  
**Construction:** 95mm x 55mm.  
 Softwood section studwork.  
 13mm fire rated plasterboard fixed to both sides of studwork.  
**Fire Integrity:** 90 minutes (External Mould)  
**Fire Insulation:** 60 minutes (External Mould)  
**Fire Integrity:** 60 minutes (Internal Mould)  
**Fire Insulation:** 60 minutes (Internal Mould)  
**Acoustic Rating:** ISO 10140.2 (STC60)

Web based drawings are for example only, fire performance of any system is dependant on, but not limited to size of opening, substrate, if penetrations are passing through, type, size and number. Please refer to Ryanfire technical department for detailed and specific fire performance information.



Client

Job Title

Drawing Title  
**Acoustic Putty Pad Gypsum Fire Wall.**

Scale <b>NTS</b>	Date <b>July 2019</b>
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Sheet Size <b>A3</b>	Drawn By
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Drawing Number <b>V37.2</b>	Rev <b>2.0</b>
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17 Dec 2019

HWCP Invercargill

Building Division Matrix 24-Sep-19

Z0 FS 100 v2

Invercargill City  
Council  
Building Consent  
Authority  
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Approved For Issue  
27/02/2020

BUILDING CONSENT NUMBER

2019/1381

Holmes

Activation Protocol	ALARM SIGNAL ORIGIN										
	Manual Call Point (Z1,Z2 Z3)	Smoke Detector (Z1 Anchor)	Smoke Detector (Z1 Childcare)	Smoke Detector (Z2 North)	Smoke Detector (Z2 all other)	Sprinkler Flow switch Zone 1	Sprinkler Flow switch Zone 2 (Ground or L1)	Sprinkler Flow switch Zone 3 (L1, L2 or L3 carpark)	Sprinkler Flow switch Zone 3 (L4 or L5 carpark)	Zone 1 FireFighters Control Panel Manual Switch	Zone 2 FireFighters Control Panel Manual Switch
FENZ Signalled	Y	Y	Y	Y	Y	Y	Y	Y	Y		
Fire Indicator Panel	Y	Y	Y	Y	Y	Y	Y	Y	Y		
Childcare RDU indicate origin	Y	Y	Y	Y	Y	Y	Y	Y	Y		
Building Wide Evacuation	Y	Y	Y	Y	Y	Y	Y	Y	Y		
Access control doors (mag clamp/security) release <sup>1</sup>	Y	Y	Y	Y	Y	Y	Y	Y	Y		
Electromechanical hold open devices	Y	Y	Y	Y	Y	Y	Y	Y	Y		
Z3 Elevators return to ground and opens	Y	Y	Y	Y	Y	Y	Y	Y	Y		
"No Exit" signage on for Childcare.				Y					Y		
Entry Traffic barrier arm stays down, Exit Traffic barrier arm open	Y	Y	Y	Y	Y	Y	Y	Y	Y		
Main Gas Solenoid	Y	Y	Y	Y	Y	Y	Y	Y	Y		
Tenancy Gas Shutoff (Foodcourt) (method of demonstrating to be considered by Cosgroves)											
HVAC shutdown (Z1 Common area Anchor)	Y	Y				Y	Y	Y	Y		
HVAC Shutdown (Z2 Common Mall Areas)	Y	Y		Y	Y	Y	Y	Y	Y		
HVAC Shutdown (Z2 Food tenancies)											
HVAC Shutdown (Z2 All tenancies)											
HVAC/Jet fan Shutdown (Z3 Carpark)	Y							Y	Y		
HVAC Shutdown (ventilation between firecells)	Y	Y	Y	Y	Y	Y	Y	Y	Y		
Z1 Anchor Smoke Extract System <sup>3</sup>		Y								Y	
Z2 Mall Smoke Extract System <sup>3</sup>				Y							Y
Z1 Auto-Doors (To Esk St & Carpark) <sup>1, 2</sup>	Y	Y		Y	Y	Y	Y	Y	Y	Y	Y
Z2 Auto-Doors (To Esk St & Tay St) <sup>1, 2</sup>	Y	Y		Y	Y	Y	Y	Y	Y	Y	Y
Separation to HWR Tower											
Separation to Reading Cinema											

Text black colour relates to works that are part of the expected works for associated building works (Z1 & Z3)

Text blue colour relates to works that are part of the future expected works (Z2)

Text red colour relates to potential future interface needs which are yet to be established.

Notes:

1. Auto-Opening of Exit Doors and Security release is only required during the hours for which either the Zone 2 or Zone 1 is in trade (e.g. when public occupancy is permitted within the building) and on activation of the manual switch at the FFCP.
2. If Smoke Extract Systems operated from the Fire Fan Control Panel (FFCP) the auto-open exit door functionality is to be interfaced with the FFCP also, to ensure that the smoke extract systems do not operate without the auto-doors opening to provide inlet/make-up air.
3. If Smoke Extract System has been triggered/ initiated in either Zone, and additional alarm signals activate, only the original smoke extract is to function.